Groundwater Sampling/Pumping Test Technical Memorandum

144TH FIGHTER WING CALIFORNIA AIR NATIONAL GUARD FRESNO AIR TERMINAL, FRESNO, CALIFORNIA



HAZWRAP SUPPORT CONTRACTOR OFFICE

Oak Ridge, Tennessee 37831

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Groundwater Sampling/Pumping Test Technical Memorandum For the 144th Fighter Wing California Air National Guard Fresno Air Terminal, Fresno, California

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List of Acronyms.

the Base California Air National Guard Base

BCP Base collection pond b aquifer thickness

bgs below ground surface

cl clay

DCP dichloropropane

ft²/day square feet per day

gpm gallons per minute

IT IT Corporation

K hydraulic conductivity

ml silt

msl mean sea level

μg/L micrograms per literPCE tetrachloroethenePVC polyvinyl chloride

RI remedial investigation

S storativity

SI site investigation
T transmissivity
TCE trichloroethene

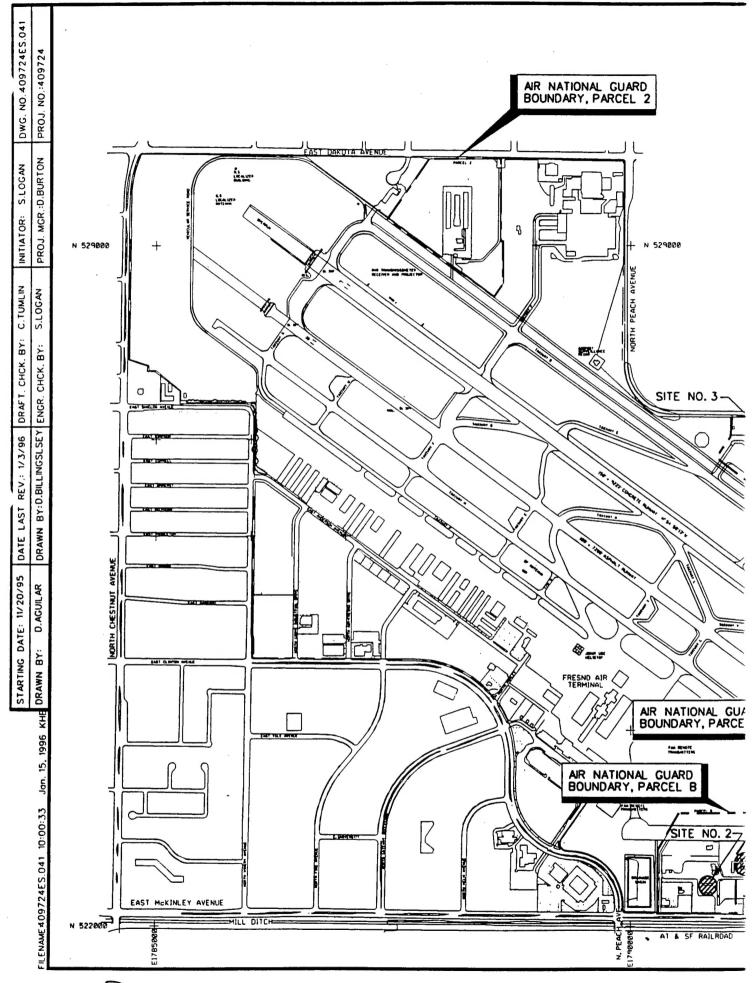
TM Technical Memorandum
VOC volatile organic compound

1.0 Introduction and Project Context

This technical memorandum summarizes the activities and findings of the continuing deep aquifer investigation at the California Air National Guard Base (the Base), located at the Fresno Air Terminal in Fresno, California (Figure 1). A brief overview of the rationale and field activities is presented, followed by laboratory results and data analysis and interpretations.

A site investigation (SI) was conducted at the Base from July 1990 to February 1991. Four sites were investigated for the presence of soil and groundwater contamination. Furthermore, groundwater was investigated Base-wide for the presence of contaminants. The results are fully discussed in the SI report (IT Corporation [IT], 1992). A potential fifth site was identified during the SI activities. As a result, a focused remedial investigation (RI) was conducted at the newly identified Site 5 (the Base collection pond [BCP]) from August to October 1992. The results are presented in the interim report of findings for the focused RI (IT, 1993a). In conjunction with the focused RI, a quarterly groundwater sampling and monthly groundwater monitoring program was conducted from June 1992 through May 1993; this program is summarized in the quarterly groundwater monitoring report, April 1993 (IT, 1993b). During the SI, focused RI, and monitoring program, the nature and lateral extent of groundwater contamination in the uppermost water-bearing zone (water table aquifer) was characterized.

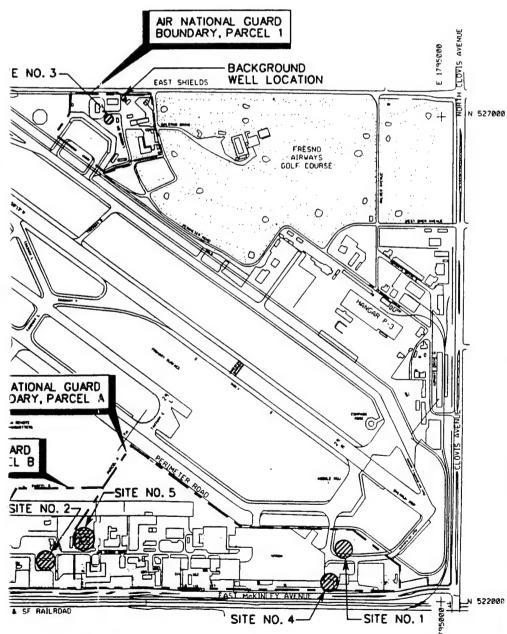
A deep aquifer investigation was performed from October through December 1993 to characterize the vertical extent of contamination in groundwater beneath the western portion of the Base. Identified groundwater contamination consisted of chlorinated volatile organic compounds (VOC), primarily trichloroethene (TCE) and tetrachloroethene (PCE). The deep aquifer investigation targeted these compounds and related VOCs for vertical characterization below the water table and the results are preliminarily discussed in the initial deep aquifer investigation technical memorandum (TM) (IT, 1994). The initial deep aquifer investigation provided good insight into the hydrogeologic regime from the water table (approximately 80 feet below ground surface [bgs]) to a depth of 250 feet bgs. However, the information gained did not define the degree of interconnection among the hydrogeologic units of interest. For this reason, pumping tests were performed to assess the communication between specific hydrogeologic zones. The 1993 investigation also determined the need for additional groundwater sampling data from the deep monitoring wells installed. Deep monitoring well groundwater sample results are presented in this TM along with results from the pumping tests.



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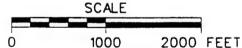


FIGURE 1
BASE MAP LOCATION OF IDENTIFIED INVESTIGATION SITE:

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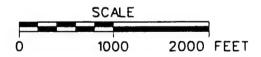


FIGURE 1
BASE MAP LOCATION OF
IDENTIFIED INVESTIGATION SITES

CALIFORNIA AIR NATIONAL GUARD FRESNO AIR TERMINAL FRESNO, CALIFORNIA





2.0 Background and Objectives

2.1 Groundwater Sampling

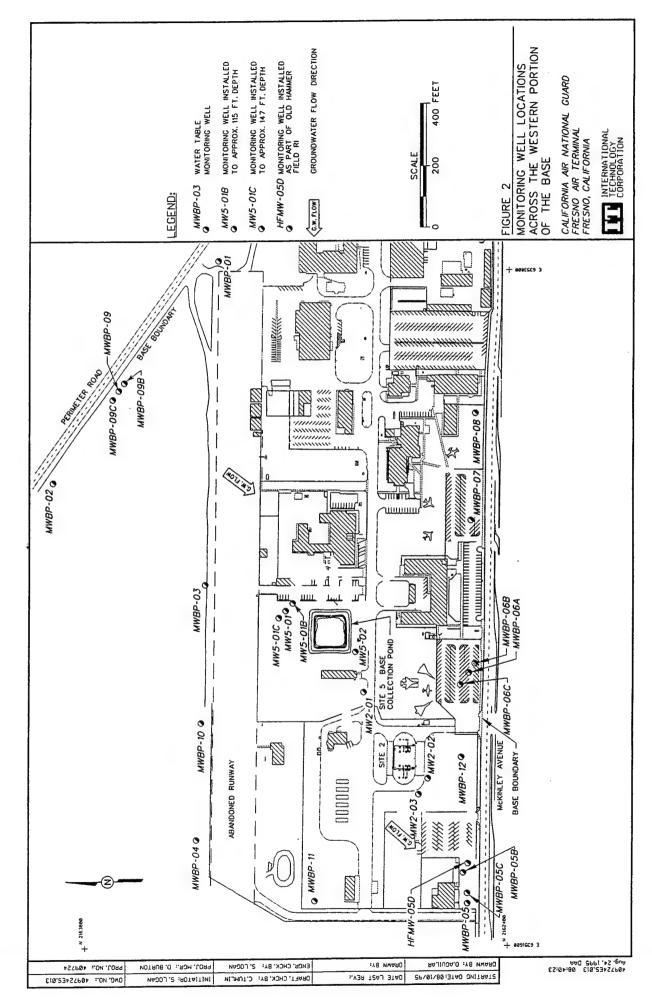
Several monitoring wells have been installed into the uppermost water-bearing unit across the western portion of the Base (Figure 2). They have been sampled on six different occasions during the SI and quarterly sampling program. During the initial deep aquifer investigation, eight deeper monitoring wells were installed and groundwater samples collected. Deep wells are those noted with a "B" or "C" suffix on Figure 2. A second round of samples from the deep monitoring wells was collected in association with the pump test activities to confirm the initial round of sampling, which occurred in 1993.

2.2 Pumping Tests

Eight wells installed during the initial deep aquifer investigation were installed into two aquifer zones below the water table. During the initial deep aquifer investigation, PCE was determined to be the contaminant of concern related to past Base disposal activities (IT, 1994) and the deep monitoring wells were installed within and below the PCE plume. The zones chosen for the monitoring wells were based on identified stratigraphic intervals and chemical screening data. However, the hydraulic communication among the stratigraphic units could not be determined by the initial investigation.

The zones into which the deep monitoring wells were installed were randomly noted as the "B" and "C" zones, with the water table wells constituting the "A" zone. From the deep aquifer investigation, it appears that the "A" and "B" zones are connected and are part of the same aquifer. Between the "B" and "C" zones, a thin aquitard was observed across much of the Base. This aquitard does not appear to be continuous, and would inhibit but not prevent the downward migration of contaminants. Therefore, the "A", "B," and "C" zones are asserted to all be part of one aquifer, within which there is a varying degree of hydraulic communication.

The current monitoring well network across the western portion of the Base is shown in Figure 2. Wells with a "B" or "C" suffix are installed into the intermediate and deep portions of the uppermost aquifer. Wells in Figure 2 with an "A" or no suffix are screened across the water table.



Considering this background information, pumping tests were performed to:

- Determine the degree of interconnection between the "A" and "B" zones.
- Supplement and refine the existing hydrogeologic data by determining aquifer parameters within the radius of influence around the pumped wells.

To satisfy these objectives, pumping tests were performed in monitoring wells screened in the "A" and "B" aquifer zones.

Contamination has not been detected in the "C" aquifer zone. If remedial actions are considered warranted for the existing contamination, these actions would focus on the depths at which contamination is present. Pumping tests performed in the "C" zone, while they would provide hydrogeologically interesting information, would not produce valuable information for the remedial effort; therefore, pumping tests were not conducted in the "C" zone.

3.0 Field Activities

The following field activities were performed in accordance with the pump/aquifer test addendum to the site investigation sampling and analysis plan (IT, 1995).

3.1 Groundwater Sampling

Eight existing deep ("B" and "C" zone) monitoring wells were sampled from February 14 through 17, 1995. A minimum of three well casing volumes of water were removed from each well with an environmental submersible pump. The pump was placed no more than 5 feet below the top of water in the casing and purge rates averaged 3.5 to 4 gallons per minute (gpm). Samples were collected with a decontaminated Teflon bailer. Analytical parameters for each sample were VOCs by methods 8010/8020.

During the sampling effort, short-term "pretests" were also conducted in three water table ("A" zone) monitoring wells in an effort to identify the most suitable well for further pump testing and piezometer installation.

3.2 Pumping Tests

Five separate phases were incorporated into the pumping test program: short-term "pretests", piezometer installation, background monitoring, step-drawdown tests, and constant rate tests. The "B" well selected for testing was MWBP-05B due to its location within a contaminated aquifer zone and its proximity to other existing monitoring wells. Short-term pretests were conducted in three shallow ("A") wells to identify the most suitable shallow well for testing around which piezometers would be installed. Wells tested were MW5-01, MW5-02 and MWBP-12 (Figure 2) based on the criteria outlined in the sampling and analysis plan addendum (IT, 1995). The environmental submersible pump used during well sampling was used to incrementally stress the shallow aquifer in the three wells for approximately 45 minutes; drawdown was manually recorded. Both MW5-02 and MWBP-12 proved suitable for more rigorous pump testing. MWBP-12 was the final selection for pump testing and piezometer installation because it is located within the water table contaminant plume.

Piezometers were installed around both wells to be tested (MWBP-12 and MWBP-05B). Water levels in two background wells were continually monitored during the pumping tests to observe ambient groundwater fluctuations. Step-drawdown tests were performed in MWBP-12 and MWBP-05B to ensure that the aquifer was adequately stressed during the constant rate tests.

3.2.1 Piezometers

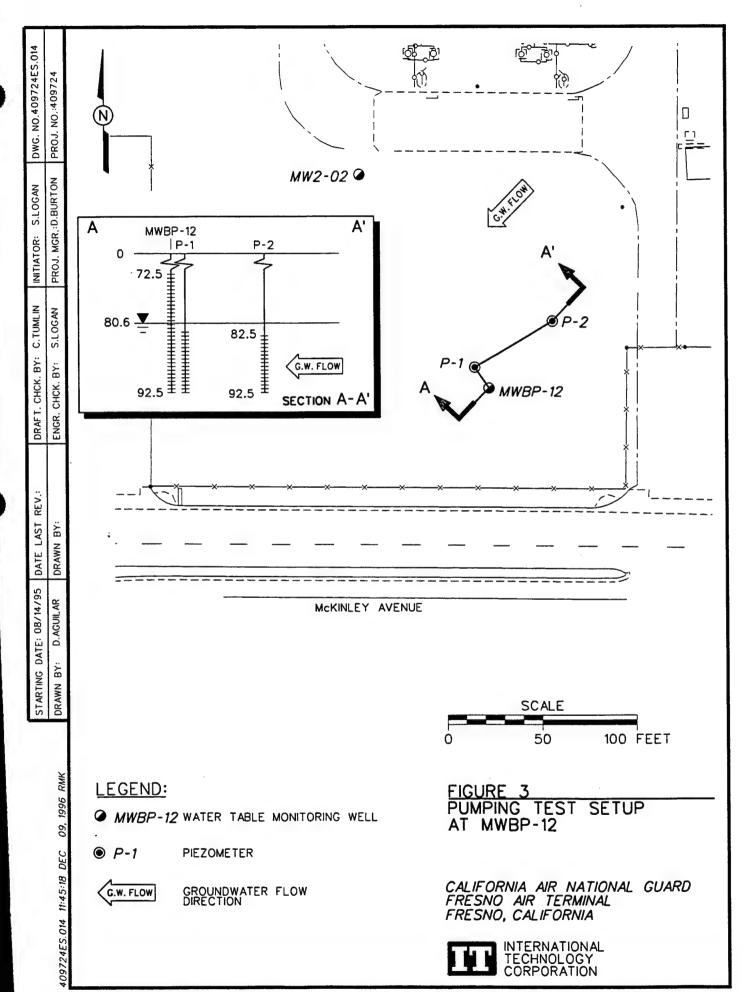
A total of five piezometers were installed in support of the pumping tests. Two (P-1 and P-2) were placed near MWBP-12 (Figure 3) and three (P-3B, P-4A, and P-5B) were installed near MWBP-05B (Figure 4). Placement of the piezometers was oriented both upgradient of and perpendicular to the prevailing flow direction. Distances of the piezometers from the pumping wells was determined based on simplistic computer modeling of aquifer stresses using preliminary hydrogeologic parameters from slug tests, well purging information, and the short-term pretests.

Drilling of the piezometer boreholes was accomplished with hollow-stem augers to the desired completion depth. Piezometers were constructed with 1.5-inch outside diameter polyvinyl chloride (PVC) screen (0.010-inch slot) and casing. Screen lengths were 10 feet. Depths of the piezometers were predetermined based on the zone to be monitored. The piezometers at MWBP-12 were installed to a depth of 92.5 feet bgs, identical to the depth of MWBP-12. Piezometers P-3B and P-5B were installed to the same depth as MWBP-05B (116 feet bgs). To provide water level data from the shallow zone near MWBP-05B, piezometer P-4A was installed approximately 10 feet below the water table (depth of 93 feet bgs). This provided shallow-zone drawdown measurements near MWBP-05B; existing shallow well MWBP-05 also provided shallow-zone measurements at a greater distance from MWBP-05B. Table 1 lists the piezometer construction and other comparative information for the wells utilized during the pumping tests.

3.2.2 Background Monitoring

The shallow and intermediate depth zones of the uppermost aquifer were selected for pump testing. To monitor ambient groundwater level fluctuations during the tests, continual water level monitoring was conducted in a water table well and the "B" well (MWBP-09 and MWBP-09B, Figure 2). Pressure transducers were installed into these two wells and measurements were recorded every 20 minutes with a data logger. Verification of fluctuations were made with periodic manual water level measurements.

Background monitoring began on March 16, 1995; the first pump tests began on March 21. A break in background monitoring was necessary due to Base activities on March 25 and 26. Ambient monitoring was reestablished before the pumping tests continued on March 27, 1995. In addition to the water level measurements, records of hourly barometric pressure data were obtained for the testing period from the National Weather Service office located immediately north of the Fresno Air Terminal.



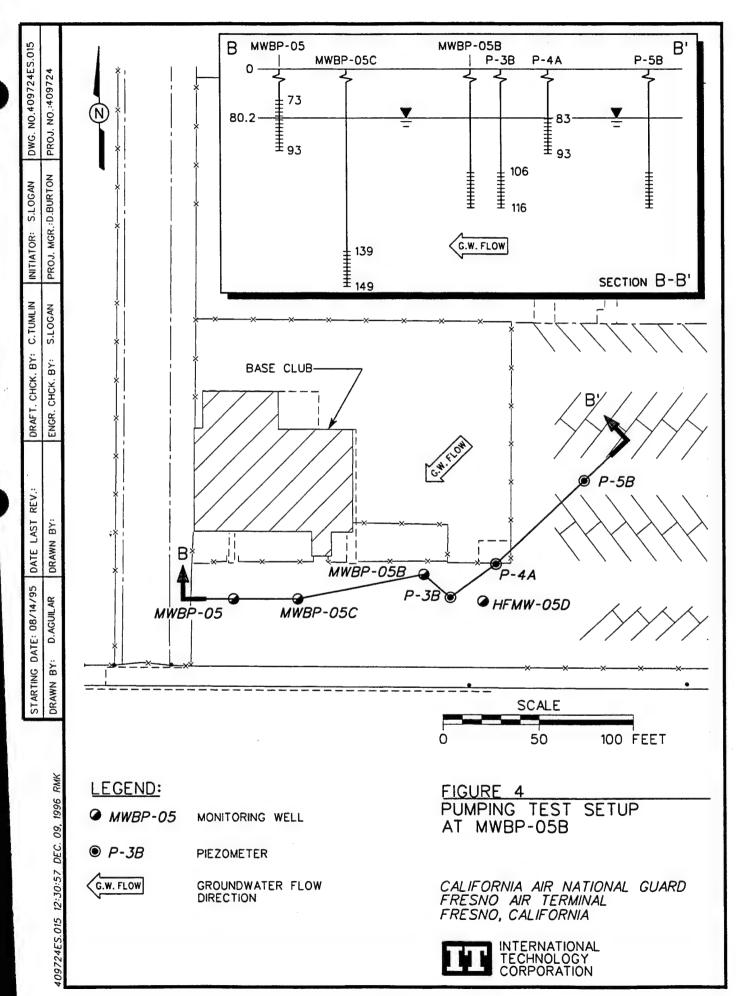


Table 1

Piezometer Construction Summary California Air National Guard, Fresno, California

Piezometer/Well ID	Installation Date	Ground Surface Elevation ^a	Screened Interval ^b	Distance from Pumping Well (feet)	Northing	Easting
MWBP-12	09-22-92	320.8	72.5 - 92.5	0	2162553.0	6352214.7
P-1	03-16-95	320.9	82.5 - 92.5	15	2162565.3	6352206.4
P-2	03-17-95	320.8	82.5 - 92.5	50	2162588.9	6352248.7
MW2-02	10-02-90	321.3	72 - 92	130	2162663.5	6352146.5
MWBP-05B	11-08-93	320.5	106 - 116	0	2162545.7	6351838.1
P-3B	03-13-95	320.7	106 - 116	20	2162533.6	6351853.7
P-4A	03-14-95	321.5	83 - 93	40	2162551.9	6351877.4
P-5B	03-15-95	321.7	106.1 - 116.1	66	2162595.6	6351923.1
MWBP-05	10-25-90	320.3	73.1 - 93.1	102	2162531.1	6351737.2
MWBP-05C	11-07-93	320.3	139.2 - 149.2	69	2162531.7	6351770.9
HFMW-05D°	03-24-94	1	335 - 345	33	2162531.8	6351870.0

^aFeet mean sea level. ^bFeet below ground surface. ^cInstalled by ERM-West as part of Old Hammer Field regional investigation.

3.2.3 Step-Drawdown Tests

Step-drawdown tests were conducted in MWBP-12 and MWBP-05B on consecutive days. Drawdown measurements were recorded in the pumping well and nearby piezometers with a pressure transducer and data logger. Table 2 lists the pumping rate steps, the step duration, and drawdown measured in the pumping well.

The wells were pumped with a 4-inch submersible pump and flow rates were measured with an in-line flow meter. Extracted groundwater was treated with a portable activated carbon treatment system and the treated water was stored at the well head in a 7,000-gallon tank for later disposal. Samples of the extracted groundwater were collected before and after treatment to assess the effectiveness of the contaminant removal.

Pumping rates were selected while the test was in progress in order to adequately stress the aquifer. The information obtained from these tests was used to provide the optimal pump rate to be used during the constant rate tests.

3.2.4 Constant Rate Tests

Constant rate tests were performed after the step-drawdown tests were conducted and evaluated in the respective pumping wells. Pressure transducers were placed into several nearby observation wells during the tests. Pump discharge rates, selected based on the results of the step-drawdown tests, were kept constant for the duration of the tests. Extracted water was again treated through the activated carbon system and the treated water was temporarily stored before it was released. Since the effectiveness of the well-head treatment system had been demonstrated during the step-drawdown tests, samples of treated groundwater were not collected prior to disposal.

Well MWBP-12 was pumped at 7.5 gpm for a period of 20 hours. Drawdown measurements were recorded automatically in the pumping well and in P-1 and P-2. Manual measurements were collected periodically from wells MW2-02 and MW2-03 (Figure 3). Due to excessive drawdown in MWBP-12, the test was stopped after 20 hours; the original intent was to conduct the test for 36 hours. From the step-drawdown test, it had appeared as though MWBP-12 could sustain a rate of 7 to 8 gpm. Unexpectedly, the aquifer was dewatered.

Well MWBP-05B was pumped at 16 gpm for 36 hours. Drawdown measurements were electronically recorded in P-3B, P-4A, P-5B, and HFMW-05D. The latter well was installed as a

Table 2 Step-Drawdown Test Summary California Air National Guard, Fresno, California

Well ID	Step Number	Step Duration (min)	Pump Rate (gpm)	Maximum Drawdown (feet)	Specific capacity (gpm/ft) ^a
MWBP-12	1	30	2.5	1.48	1.69
	2	50	5	3.24	1.54
	3	70	6.5	5.02	1.29
	4	60	7 ^b	5.63	1.24
MWBP-05B	1	45	6	3.73	1.61
	2	130	12	7.84	1.53
	3	70	18	13.13	1.37
	4	30	19 ^b	13.84	1.37

^aSpecific capacity = pump rate/drawdown. ^bMaximum pump output.

part of the more regional Old Hammer Field investigation. Manual measurements were collected periodically from MWBP-05 and MWBP-05C (Figure 4).

3.2.5 Investigation-Derived Waste

Purge water and decontamination water generated from the groundwater sampling activities was emptied into the sump at the temporary decontamination pad on Base. The water was allowed to evaporate. Water remaining at the end of the pumping test field activities was pumped through the activated carbon system and was then released to the BCP.

Water extracted during the pumping tests was immediately treated at the well head with the activated carbon system. The system consisted of two 55-gallon activated carbon units that were used in series. The first drum removed the majority of the contaminants and the second unit was used as a polishing unit. Influent and effluent samples were collected from each pumping well during the step-drawdown tests. Samples were analyzed for volatile organics on an accelerated schedule. Results of the analyses showed low levels of contaminants entering the system but not leaving the system.

Wastewater sample results demonstrated that the treatment system was working as expected and water that had been temporarily stored was released to the BCP (Figure 2) through a series of piping laid out across the Base. All of the waste water was released in this manner after it had been treated.

4.0 Results

4.1 Groundwater Sampling

Results of the VOC analyses from the eight deep monitoring wells are summarized in Table 3. Earlier sample results are shown for comparison.

TCE was detected in all eight wells, consistent with the previous sampling event. However, in each case, samples from February 1995 were lower than concentrations reported in December 1993. Concentrations in February 1995 ranged from 350 micrograms per liter (μ g/L) in well MWBP-09B to 4.8 μ g/L in MWBP-06B (Table 3).

Results for PCE were consistent with the earlier sampling event in that it was only detected in two wells (MWBP-06B and MWBP-05B). Concentrations remained relatively unchanged. Perhaps more importantly, PCE was not detected in the "C" series wells, indicating that migration of PCE has not impacted the lower aquifer zones.

Cis-1,2-dichloroethene was detected in MWBP-06B at a trace concentration. 1,2-dichloro-propane (1,2-DCP), which was detected in two wells at low concentrations in December 1993, was not detected in any February 1995 samples. Detection of 1,2-DCP has been sporadic throughout the sampling program at the Base (IT, 1993b).

4.2 Pumping Tests

4.2.1 Background Monitoring

Water level fluctuations in the background wells over the test period are shown in Figure 5. As is evident from the figure, fluctuations are inversely related to variations in the barometric pressure changes. The total differential fluctuation is approximately 0.45 feet, within the range of drawdown measurements in the observation wells during the pump tests; therefore, drawdown measurements in the observation wells were corrected based on the recorded background water level fluctuations. The break in background monitoring which occurred on March 25 and March 26 did not affect data interpretation because no tests were conducted during that time period.

Until the present, the first occurrence of water has been referred to as the water table, assuming unconfined conditions. However, the marked correlation between atmospheric pressure changes and water level changes suggests a confined or semiconfined condition (Todd, 1980; Davis and

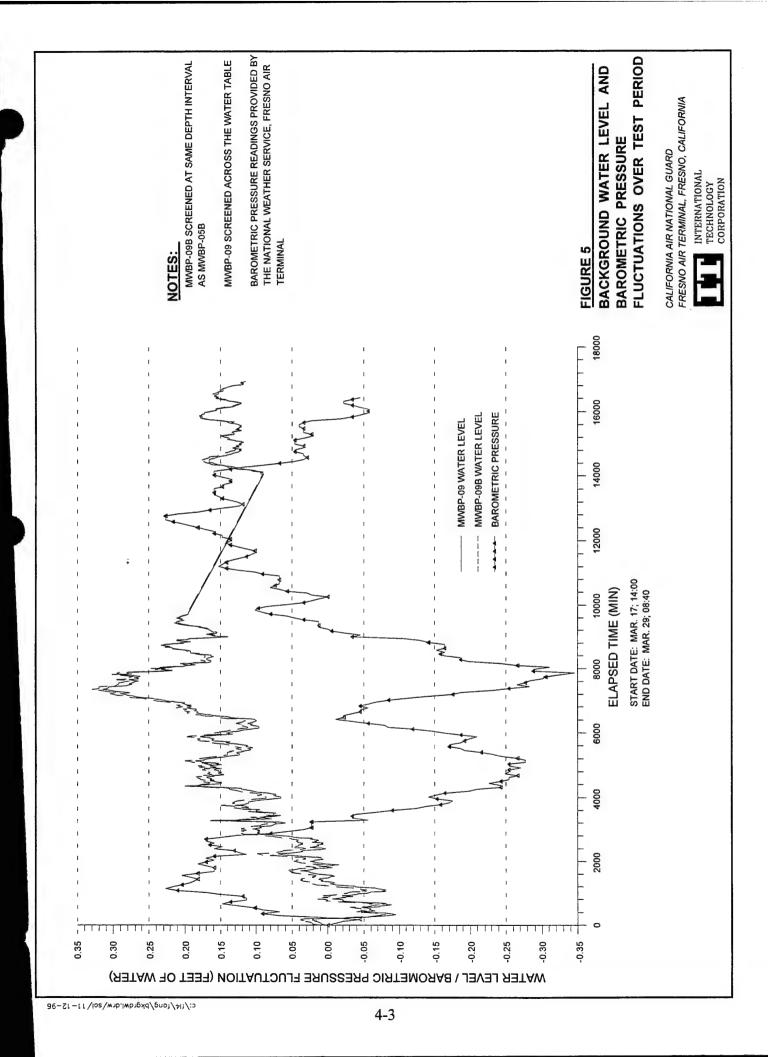
Table 3

Summary of Deep Monitoring Well Groundwater Analytical Data California Air National Guard - Fresno, California

	Sample No	MW5-01B-12/93	/93	MW5-01B-2/95	MW5-01C-12/93	MW5-01C-2/95	MWBP-05B-12/93	MWBP-05B-2/95
	Sample Date	8-Dec-93		14-Feb-95	9-Dec-93	15-Feb-95	9-Dec-93	15-Feb-95
PARAMETER	Units	Result	Qual	Result Qual	Result Qual	Result Qual	Result Qual	Result Qual
1,2-Dichloropropane	μg/L							
Tetrachloroethene	μg/L						16	9.8
Trichloroethene	μg/L	250		200	120	81	130	99
cis-1,2-Dichloroethene	μg/L							

	Sample No	1-050-48WM	35C-12/93	MWBP-05C-2/95	5 MWBP-06B-12/93	MWBP-06B-2/95	MWBP-06C-12/93	MWBP-06C-2/95
	Sample Date	9-Dec-93		16-Feb-95	9-Dec-93	15-Feb-95	9-Dec-93	15-Feb-95
PARAMETER	Units	Result	Qual	Result	Qual Result Qual	Result Qual	Result Qual	Result Qual
1,2-Dichloropropane	hg/L	3.9			0.88			
Tetrachloroethene	μg/L				23	18		
Trichloroethene	hg/L	79		53	7.5	4.8	260	09
cis-1,2-Dichloroethene	hg/L				1.2	99'0		

							Г				Γ
	Sample No	MWBP-09B-1	2/93	09B-12/93 MWBP-09B-12/93Z	7,93Z	MWBP-09B-2/95		MWBP-09C-12/93	MWBP-09C-2/95	MWBP-09C-2/95FD	_
	Sample Date	8-Dec-93		8-Dec-93		14-Feb-95		8-Dec-93	14-Feb-95	14-Feb-95	
PARAMETER	Units	Result	Qual	Result Qual	Qual	Result Qual	Qual	Result Qual	Result Qual	Result Qual	ā
1,2-Dichloropropane	μg/L										
Tetrachloroethene	µg/L										
Trichloroethene	µg/L	200		520		350		25	12	10	
cis-1,2-Dichloroethene	μg/L										



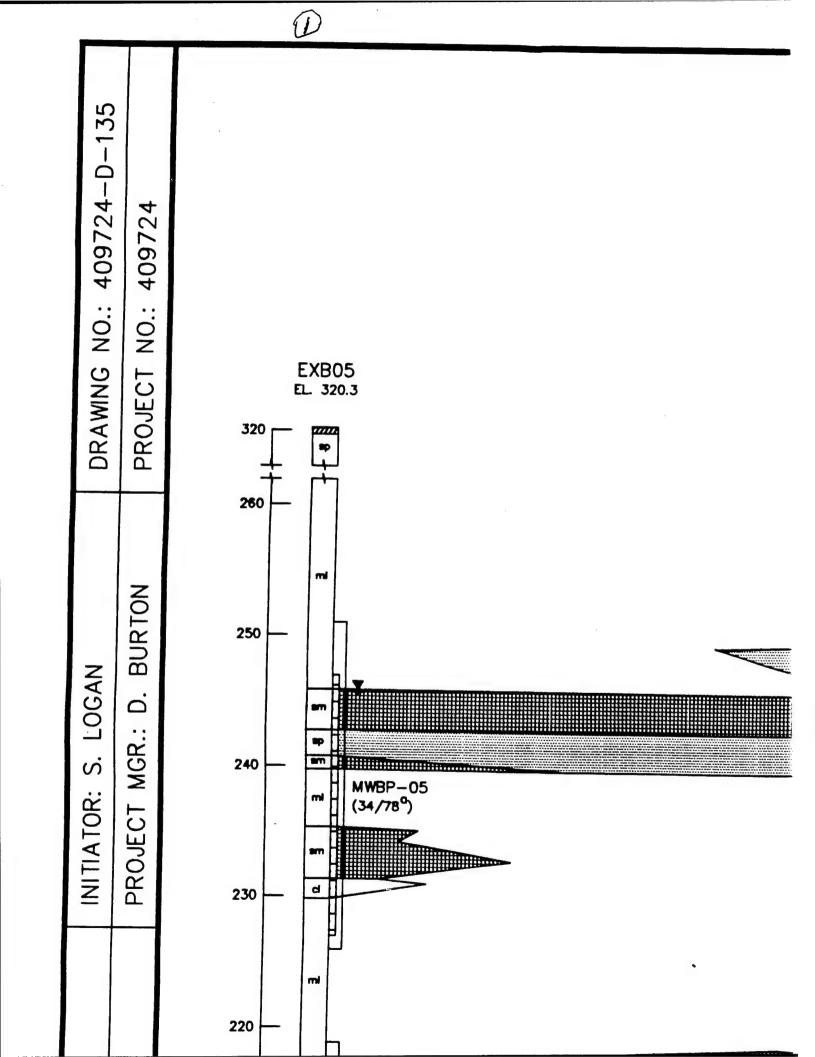
DeWeist, 1966). The definition of the water table is that the water surface is at atmospheric pressure at all points. Fluctuations in barometric pressure would be instantaneously transmitted to the water surface and absorbed such that the fluctuations, while perhaps observable, would be dampened (Vacher, 1978). Literature generally attributes water table changes to atmospheric pressure changes only in shallow sediments (Peck, 1960; Smedema and Zwerman, 1967). Yet, correlations of water level fluctuations to barometric pressure loading cannot, by themselves, determine whether the aquifer type penetrated by a well is unconfined or semiconfined (Rojstaczer and Riley, 1990). This determination can only be made by pumping tests and a thorough knowledge of the hydrogeologic setting.

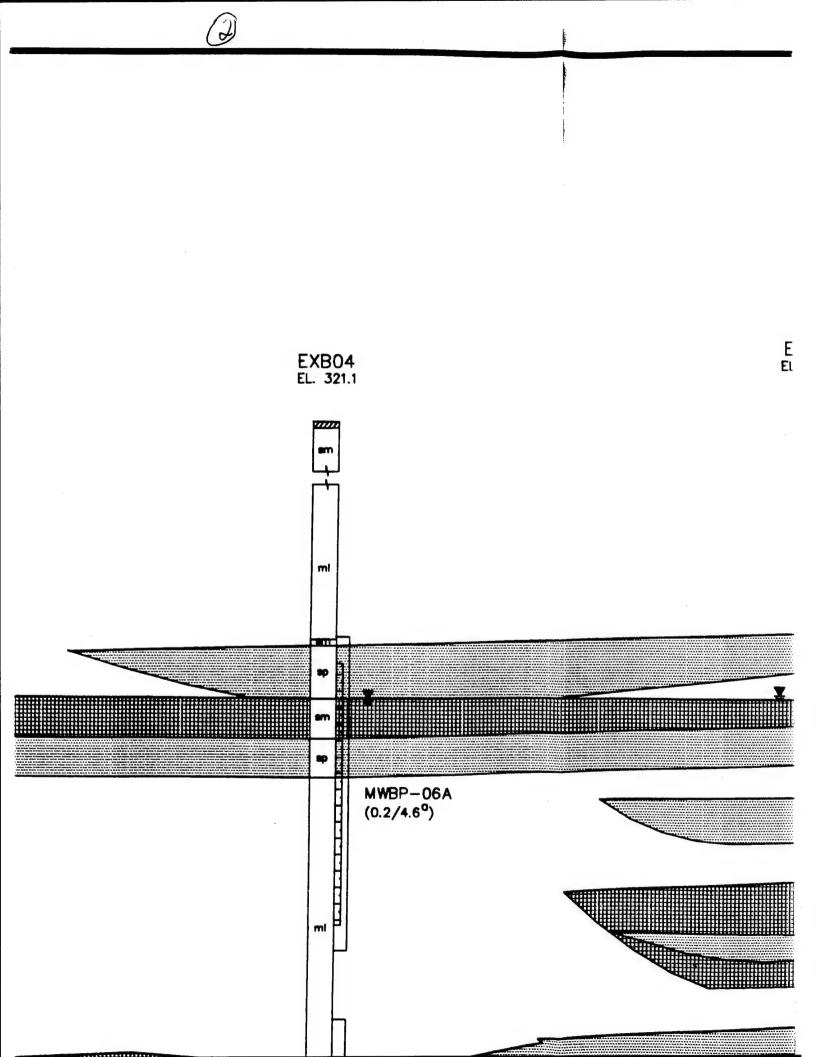
However, observations by several researchers (among others, Ferris et al., 1967, Turk, 1975) indicate that if a layer or bed of low permeability lies between the water table and the ground surface, then air flow is restricted. This implies that the atmospheric pressure changes would not be instantaneously absorbed by the phreatic surface and a resulting fluctuation would occur. This is the case at the Fresno Air National Guard Base. Figure 6 shows a cross section of sediments that are present just above and somewhat below the water table, and a fine-grained silt layer is evident. This fine-grained material is the silt (ml)/clay (cl) layer which has a bottom elevation between 245 and 255 feet mean sea level (msl).

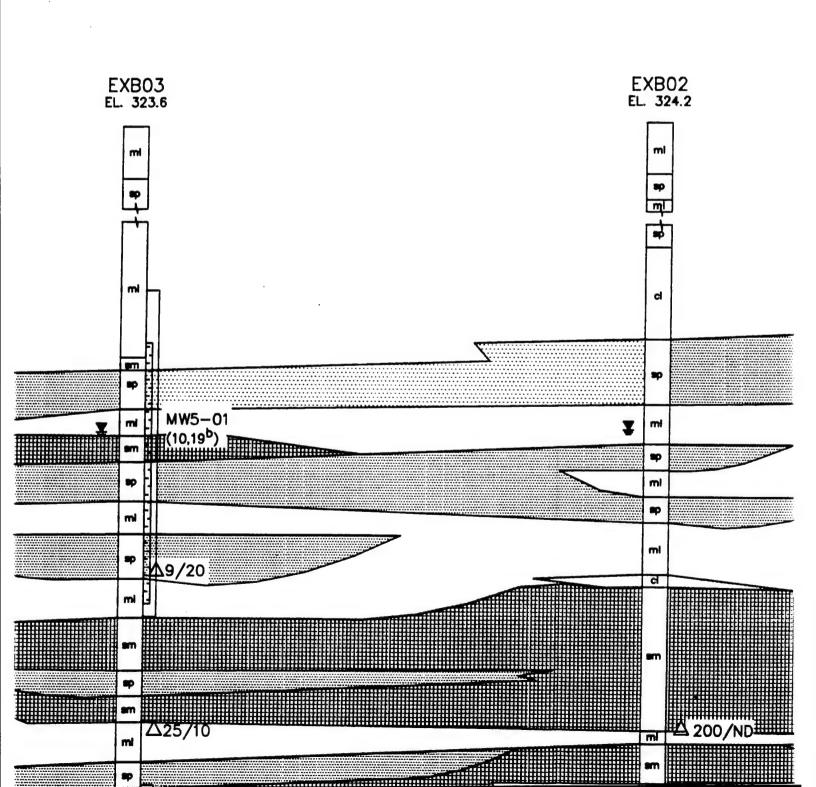
Also of consideration is the path that water must take in order to reach the water table. The SI report (IT, 1992) shows several site-specific geologic cross sections comprising alternating beds of fine- and coarse-grained layers or beds typical of the alluvial depositional environment. Fine-grained beds inhibit downward flow of water to the water table, thus causing a tortuous path of infiltration. This condition would also hold true for the transmission of air or barometric pressure; neither can be readily transmitted to the water surface and atmospheric pressure changes would not be instantaneously absorbed.

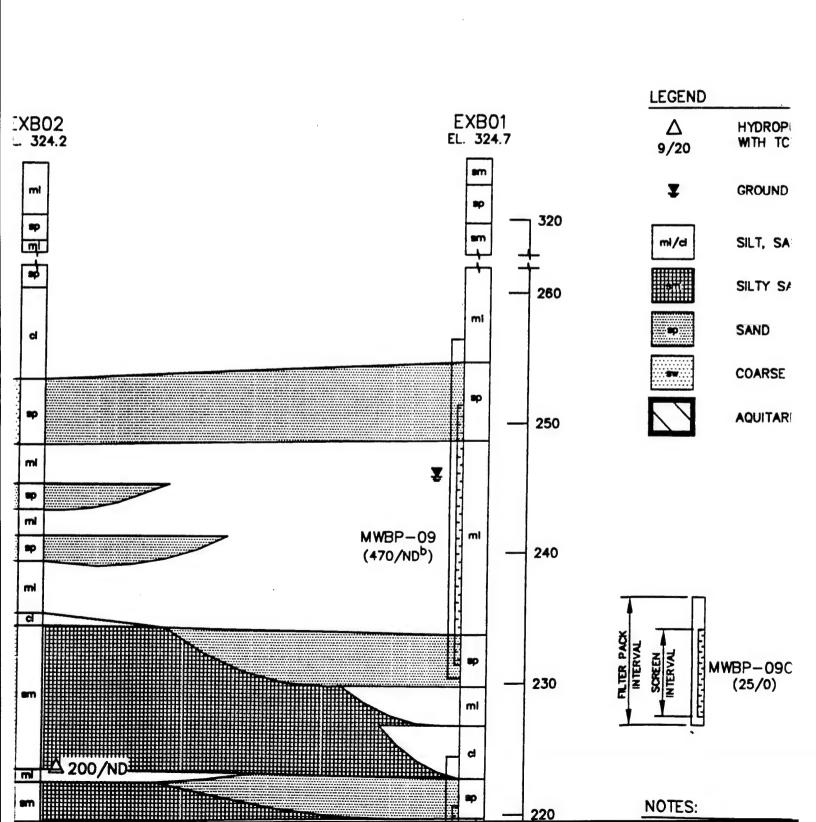
Therefore, although the first occurrence of water may be referred to as the "water table," the aquifer behaves as though it is semiconfined as determined through pumping tests (Section 4.2.3). The correlation to barometric pressure changes with water table fluctuations also supports this aquifer type.

Barometric efficiency is defined as the change in water level divided by the change in barometric pressure for the same time period. An analysis of barometric efficiencies at approximate 24-hour time intervals was conducted for the background monitoring period. Efficiencies varied widely from 1 to 62 percent, depending on the time period. Average barometric efficiencies for the "A"









HYDROPUNCH GROUNDWATER SCREENING SAMPLE LOCATION WITH TCE/PCE CONCENTRATION IN PPB

GROUND WATER TABLE ELEVATION, 12/93

SILT, SANDY SILT, CLAY

SILTY SAND

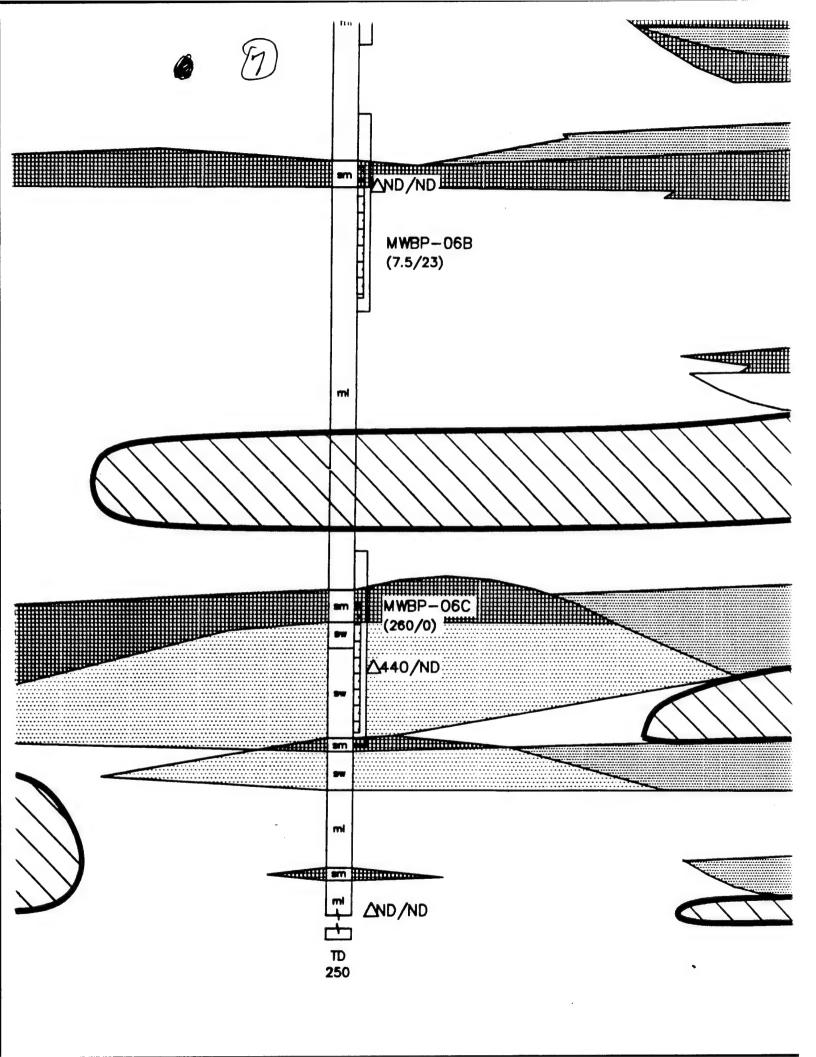
SAND

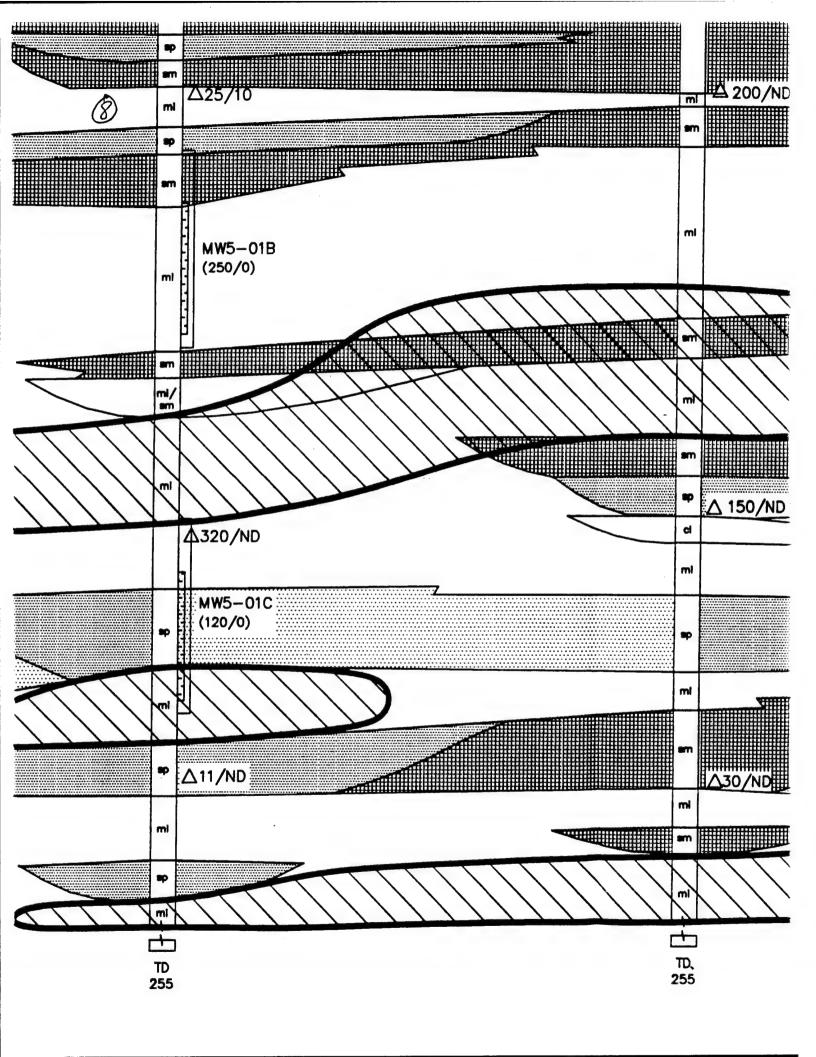
COARSE SAND, GRAVEL

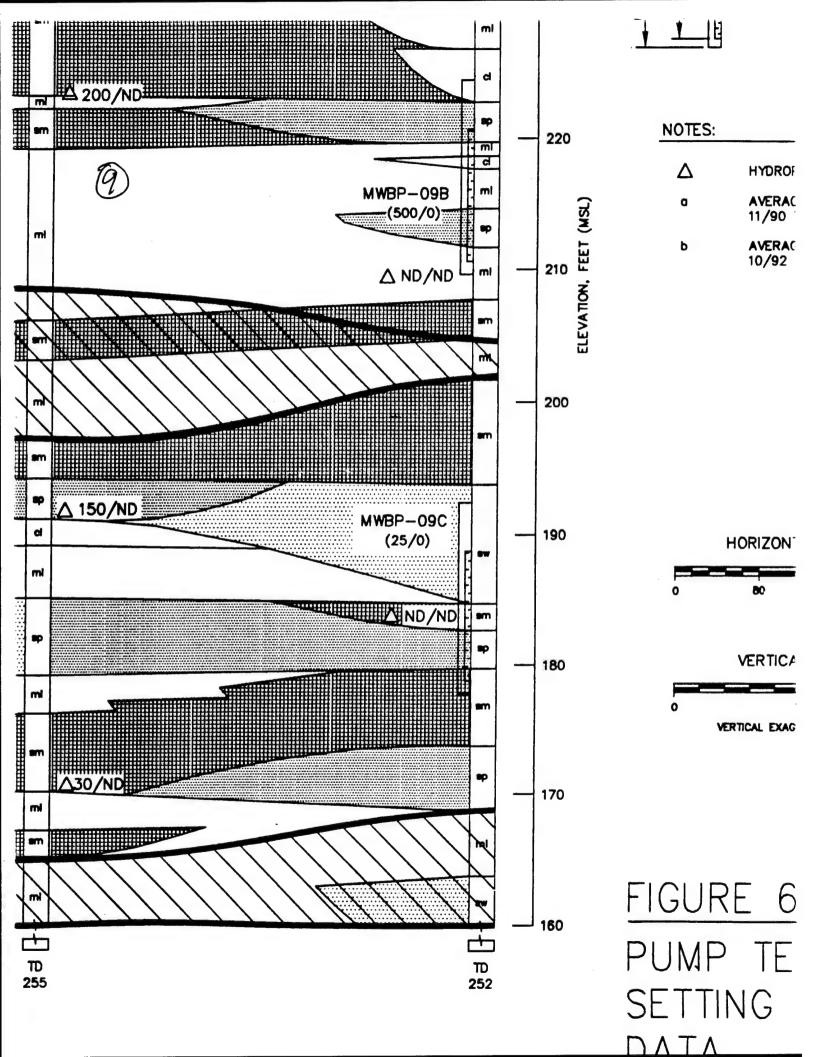
AQUITARD MATERIAL

3P-09C WELL NOMENCLATURE WITH TCE/PCE CONCENTRATION (25/0) IN PPB (WELLS SAMPLED 12/93)

		1		
		6		mi
			220	
		ET (MSL)		<u>1</u> <u>1</u> <u>1</u> <u>2</u> 290 / 106
REV.:		ELEVATION, FEET (MSL)	210	MWBP-05B
AST	BY:	ELEVA		mi (130/16)
DATE LAST REV.:	DRAWN BY:		200	
Q	DR			
			190 —	
/95				mi and the second secon
	GS		180 —	MWBP-05C em [[62/0]
	. HIGGS		180	(62/0) \(\triangle 54/ND \)
DA	BY: D.			
RTIN			170	
STA	DRAWN			DZ9/NB
			160	
	DAA			TD 250 ·
	am DAA			









NOTES:

△ HYDROPUNCH SAMPLES COLLECTED 10/93

a AVERAGE CONCENTRATION OF 6 SAMPLES COLLECTED FROM 11/90 TO 4/93



b AVERAGE CONCENTRATION OF 3 SAMPLES COLLECTED FROM 10/92 TO 4/93

240 FEET

HORIZONTAL SCALE

80

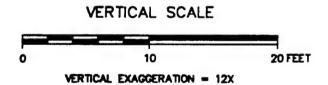
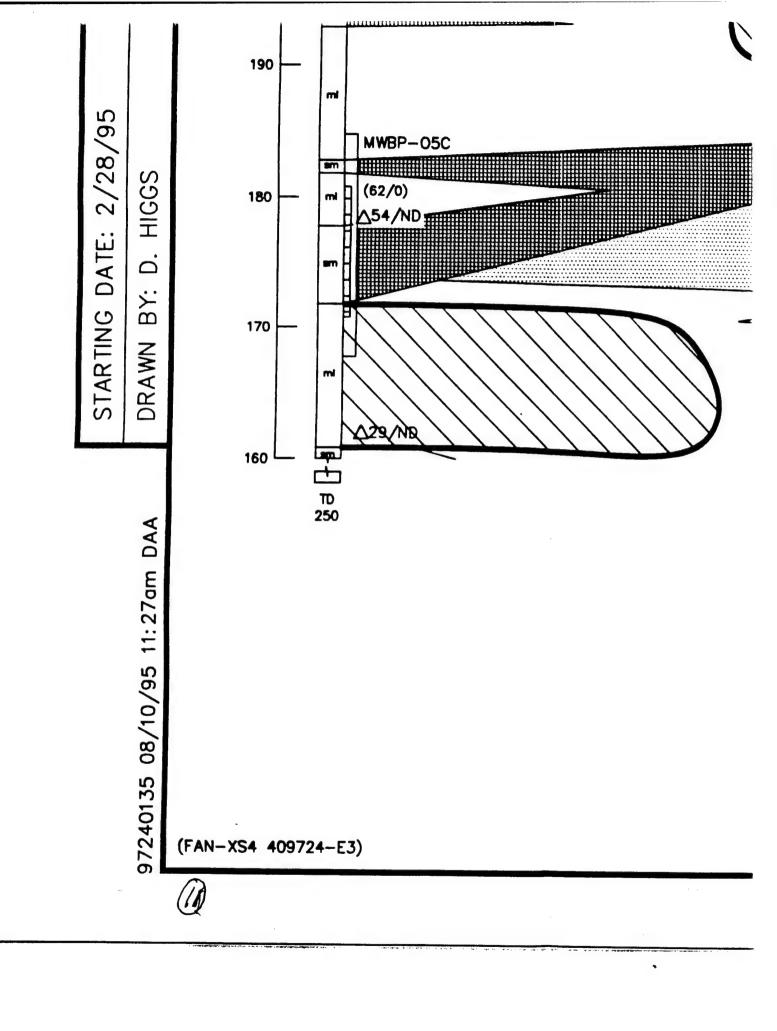
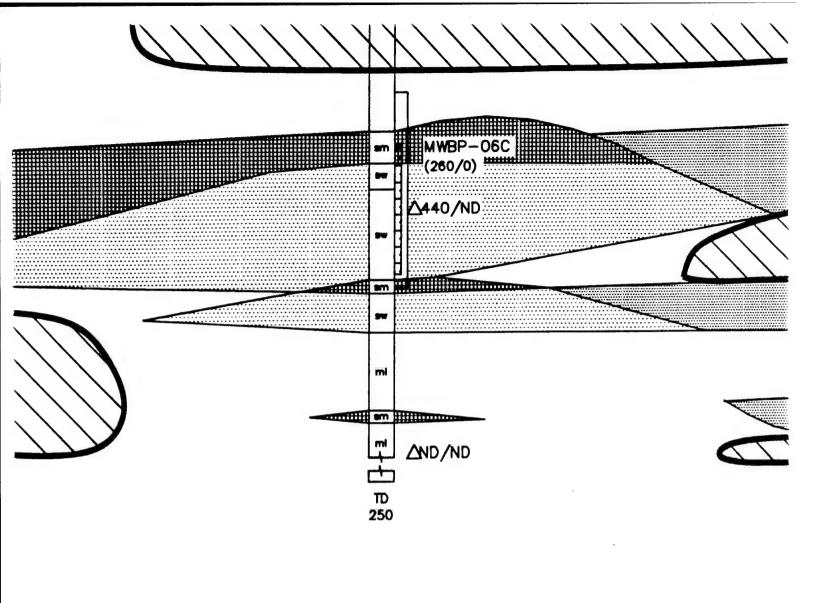
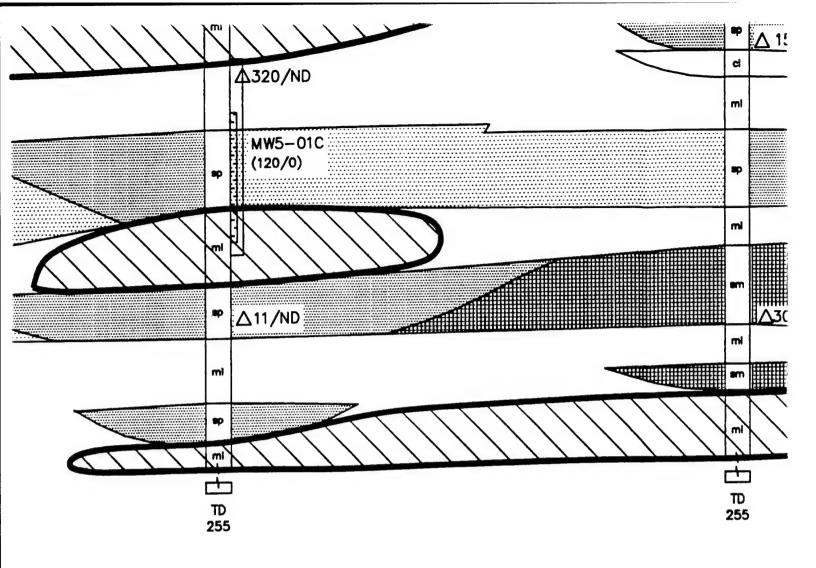


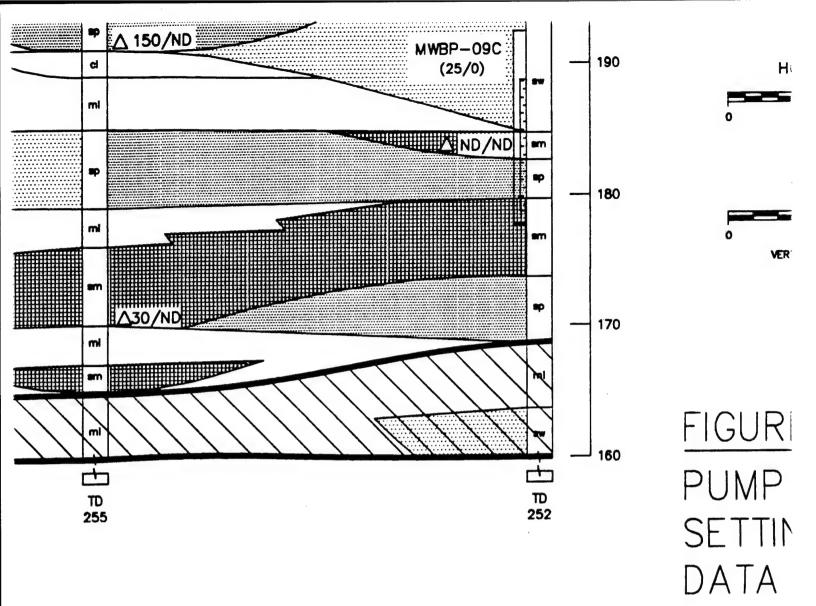
FIGURE 6

PUMP TEST HYDROGEOLOGIC SETTING WITH CHEMICAL



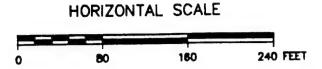






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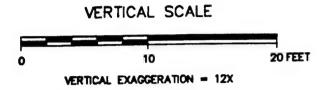


FIGURE 6

PUMP TEST HYDROGEOLOGIC SETTING WITH CHEMICAL DATA

CALIFORNIA AIR NATIONAL GUARD FRESNO AIR TERMINAL FRESNO, CALIFORNIA





and "B" zones were essentially equivalent, with 39 percent for the "A" zone and 37 percent for the "B" zone.

4.2.2 Step-Drawdown Tests

The wells in which pump tests were performed were 4- and 5-inch monitoring wells with limited screen lengths. They are not considered production wells, and well efficiency and well loss characteristics were not calculated. Step-drawdown tests were performed in order to assess the practical yield of each well for long-term testing. Summaries of step-drawdown test data are included as Appendix A.

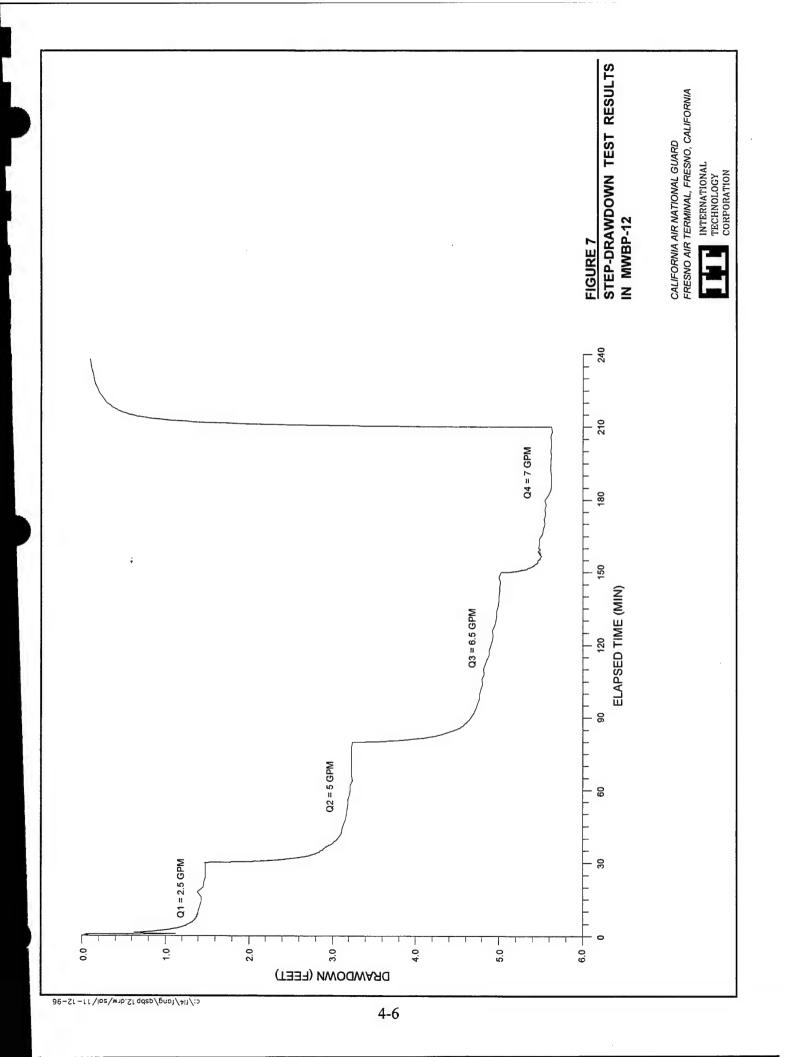
MWBP-12. The step-drawdown test in MWBP-12 was conducted at the flow rates listed in Table 2. Figure 7 displays the drawdown measurements for the test duration. Initially, the water column standing in MWBP-12 was 11.9 feet and by the end of the test drawdown approached 50 per cent of this height at a pumping rate of 7 gpm. Approximately 0.6 feet of drawdown was recorded in observation well P-1 at the end of the test (Appendix A).

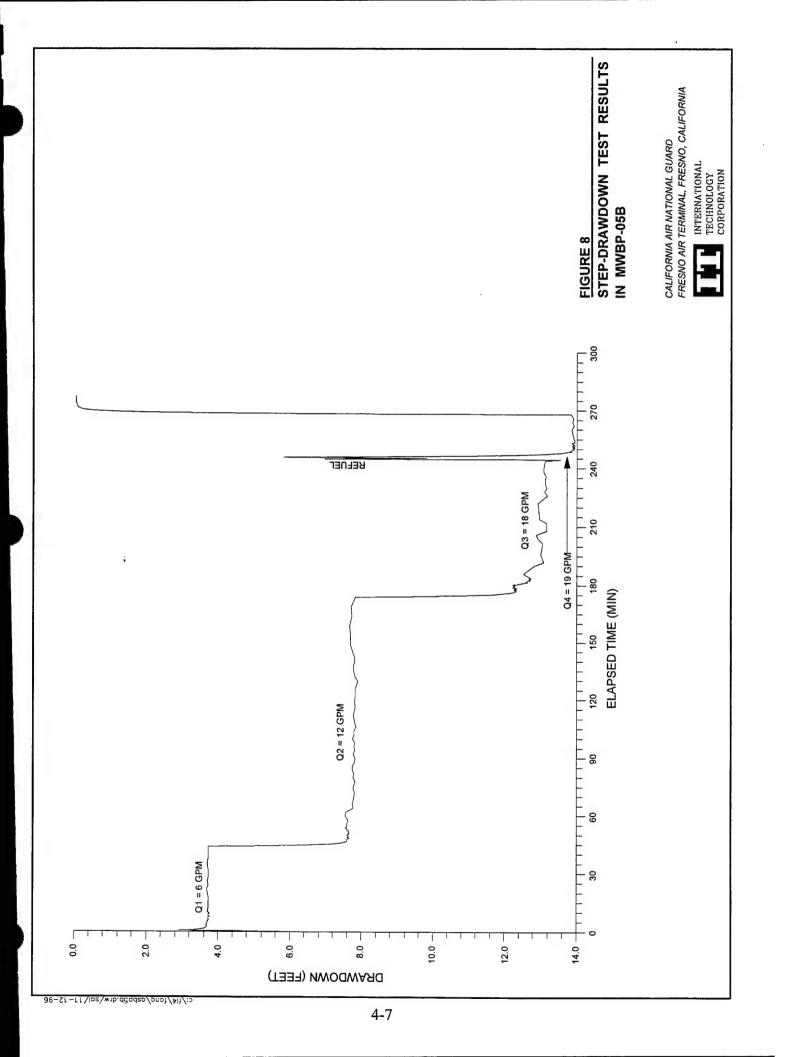
Given the type of material in which MWBP-12 was installed (silty sands), the initial water column height, and the total pumping lift, the well was pumped at a rate greater than that which was originally expected. The pump was lifting water through a 1-inch discharge line to the carbon filtration system to the top of the temporary holding tank, causing additional head loss. With this amount of head loss, the pump was at its maximum rate at 7 gpm. It was theorized that if the size of the discharge line were increased and the total lift of the pump reduced, then a greater pump rate could be achieved for the long-term test. For these reasons, a rate of 7.5 gpm was set for the long-term test.

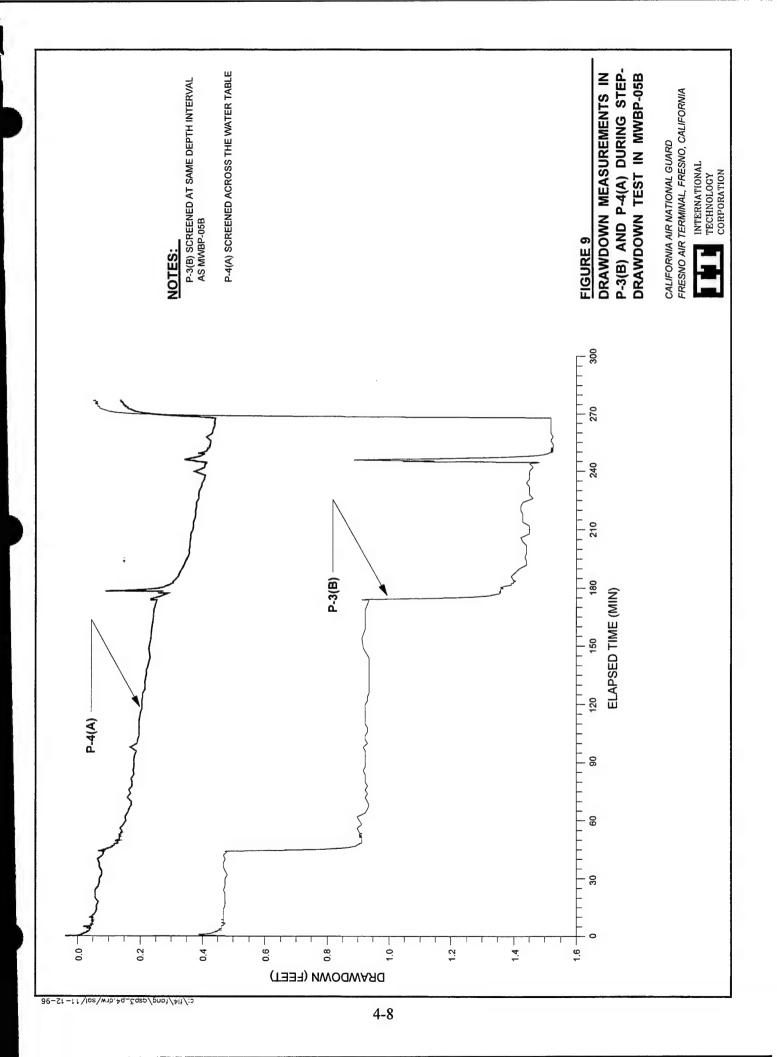
MWBP-05B. Drawdown measurements for the step-drawdown test in MWBP-05B are shown in Figure 8. Observation well data from piezometers P-3B and P-4A are shown in Figure 9.

The first objective of the aquifer testing program was to determine if the "A" and "B" zones are in hydraulic communication. This objective was met with the step-drawdown test. As seen in Figure 9, the piezometer installed in the shallower sediments responds to the pumping in the lower sediments almost instantaneously. The hypothesis that the "A" and "B" zones are part of a single aquifer appears to be correct at this particular location.

Based on the response of MWBP-05B during the step-drawdown test, a pumping rate of 16 gpm was selected for the long-term test.







Recovery Analysis. A method for determining transmissivity from the recovery data after a step-drawdown or variable rate pump test has been developed by Kawecki (1993). Equations developed by Kawecki are based on the Theis recovery method, and if the pump test has only one pumping stage followed by recovery, then Kawecki's method reduces to the Theis recovery method. The analysis method, equations, graphs, and recovery data are included in Appendix A. From this analysis, a transmissivity value for the "A" and "B" zones was calculated to be 89 square feet per day (ft²/day) and 62 ft²/day, respectively.

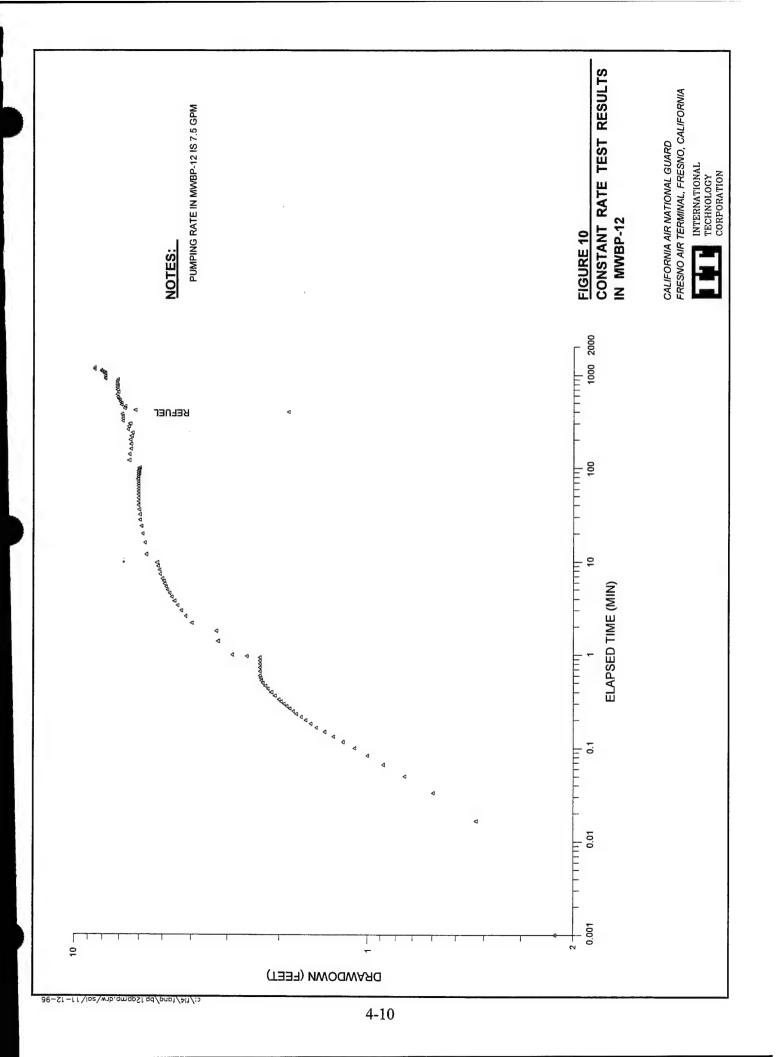
4.2.3 Long-Term Tests

Constant rate aquifer tests were conducted in MWBP-12 and MWBP-05B. Discharge rates were measured by a direct-read flow meter and were maintained through adjustments in the pump controller. Drawdown measurements were collected in the pumping well and nearby observation points with both pressure transducers and manual measurements. All data has been adjusted based on ambient background readings. The adjusted data are presented. Constant rate test data and analysis summaries are included in Appendix B.

Aquifer parameter estimates will be presented in the following manner. First, observations from each test will be described, then responses to pumping from the pumping well and each observation well will be addressed. The characteristic of the response curves will be discussed as to the type of aquifer model (unconfined, confined, or semi-confined) that best represents observed data patterns for each well. Numerical aquifer parameter estimates are summarized in a table; this is followed by a general synthesis of aquifer property values. Only the parameter estimates calculated for the pumping phases are used to determine average aquifer property values. Values derived from recovery phases are used only as a secondary check on the averaged aquifer properties.

4.2.3.1 Pumping Test Results at MWBP-12

The constant rate test in MWBP-12 was conducted at a flow rate of 7.5 gpm. It was originally scheduled to be conducted for 36 hours; however, due to excessive drawdown, it was stopped after a period of 20 hours. A graph of drawdown versus elapsed test time for MWBP-12 is shown in Figure 10. The initial two breaks in the graph (in the first 10 minutes) were caused by flow rate adjustments. After 10 minutes, the small jumps in the drawdown curve are believed to be caused by successively draining thin permeable layers near to the pumping well. This is consistent with the conceptual model for the composition of the aquifer in that it comprises multiple layers and lenses of permeable material interspersed among thicker, more extensive fine-grained beds. In addition, some jumps in the drawdown curve may have occurred because

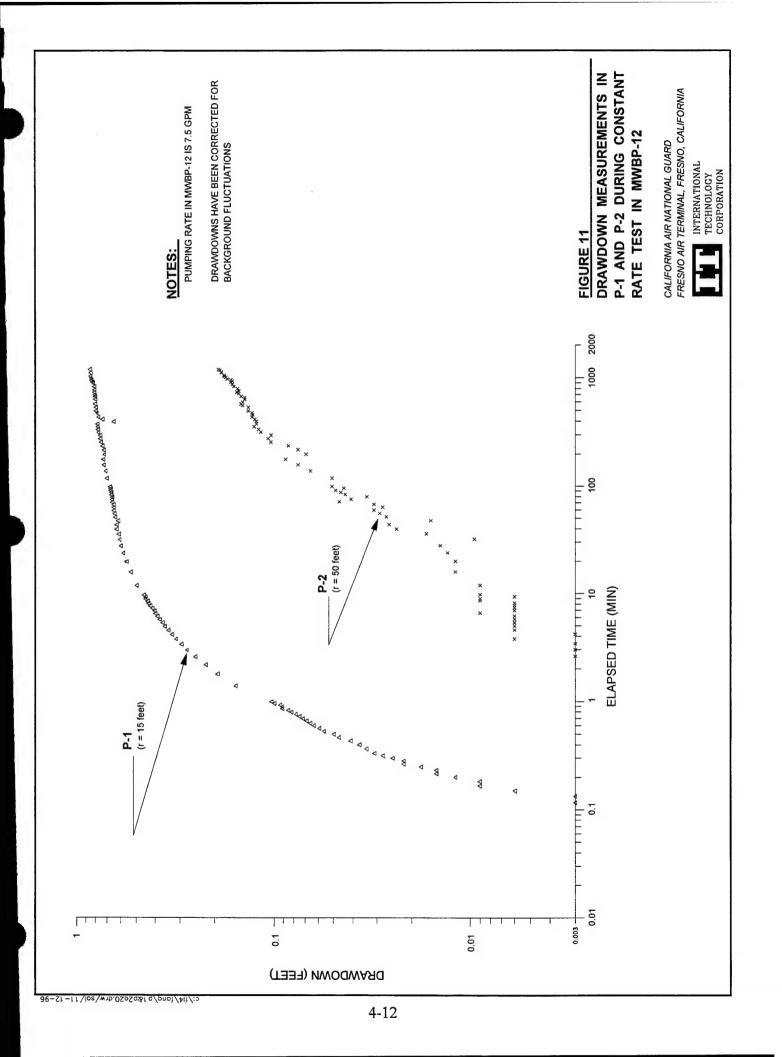


the data for individual wells has been adjusted based on ambient fluctuations observed at the background monitoring well. Heterogeneities in the subsurface could mean that whereas the observed ambient fluctuations are generally applicable, they may not represent accurately the actual fluctuations due to "natural" causes at the wells monitored for the long-term pumping tests.

Figure 10 shows that drawdown in MWBP-12 begins to increase more rapidly after about 1,000 minutes. Total drawdown at the end of the test was 8.6 feet; only 12 feet of water was available within the well and this amount of drawdown neared the level of the pump. The aquifer was essentially dewatered. Due to the shorter length of time that the test was run, it is unknown whether or not the flatter portion of the curve between 10 and 1,000 minutes was due to delayed yield effects similar to the response of a typical unconfined aquifer or whether the aquifer was simply dewatered. Because of the relatively thin cone of depression available to contribute water from gravity drainage, it is unlikely that delayed yield effects occurred.

A graph of the drawdown in observation points P-1 and P-2 is shown in Figure 11. Total drawdown for P-1 (15 feet from MWBP-12) at the end of the test was 0.86 feet, and for P-2 (50 feet from MWBP-12), 0.19 feet (Appendix B). No drawdown was observed at MW2-02, located 130 feet from MWBP-12. The radius of influence is likely approximately 75 feet from the pumping well.

Analysis of MWBP-12 Time-Drawdown Data. Limited analytical methods are available for determining a transmissivity (T) value from pumping wells. Various type-curves were tested for fit against the time-drawdown data for the pumping portion of the test plotted on a log-log scale. The best fit was obtained by one of the Papadopulos-Cooper (1967) type curves. The Papadopulos-Cooper method is more applicable to large-diameter wells with significant well-bore storage; however, application is useful after larger pumping times such that the effects of storage are diminished. This method was used to calculate T but the calculated value of S was not taken as representative because S can not be calculated from pumping well data. Time-drawdown data plotted on a semi-log scale was analyzed using the Jacob straight line method (Kruseman and deRidder, 1990). Late time data only was used because this is likely representative of the formation only (no well-bore storage). The recovery data was analyzed using the Theis recovery method (Kruseman and deRidder, 1990). Although storage values for some of the methods were calculated by the computer program used for test analysis, the storage value is meaningless for the pumping well and no storage values are presented here. Table 4 lists the



Aquifer Test Analysis Summary California Air National Guard, Fresno, California

Average T ^b (ft²/day)	250	700	2200	420	1085	740	5415	650	2410	2410	1400
Storativity		.0033	.063			.0002	.0002		.004	.024	
Transmissivity, T (ft²/day)	168 328 60 89	703 619	2206 5818	420	359 1811 68 62	846 931 294 533	5653 5176 9893	650	2414 4147	2414 6896	1410
Data Set	Drawdown Drawdown, late time data Recovery Step-drawdown recovery	Drawdown Recovery	Drawdown Recovery	Distance-drawdown	Drawdown Drawdown, late time data Recovery Step-drawdown recovery	Drawdown Drawdown Drawdown Recovery	Drawdown, late time data Drawdown Recovery	Distance-drawdown	Drawdown Recovery	Drawdown Recovery	Distance-drawdown
Model Type	Confined, large diameter well Confined Confined Confined/unconfined	Confined Confined	Confined Confined	Confined/unconfined	Confined, large diameter well Confined Confined Confined/unconfined	Leaky confined Leaky confined Confined, partial penetration Confined	Confined Confined Confined	Confined	Confined Confined	Confined Confined	Confined
Analytical Model	P-Cooper ^a Jacob straight line Theis recovery Kawecki	Theis Theis recovery	Theis Theis recovery	Thiem-Dupuit	P-Cooper Jacob straight line Theis recovery Kawecki	Hantush-Jacob Walton Hantush modification Theis recovery	Jacob straight line Theis Theis recovery	Theim-Dupuit	Theis Theis recovery	Theis Theis recovery	Thiem-Dupuit
Observation Well ID	MWBP-12	P-1	P-2	P-1/P-2	MWBP-05B	P-3B	P-5B	P-3B/P-5B	P-4A	MWBP-05	P-4A/MWBP-05
Pumping Well ID	MWBP-12				MWBP-05B						

 $^{\rm a}{\rm Papadopulos\text{-}Cooper.}$ $^{\rm b}{\rm T}$ values calculate an average T.

calculated T values for the various analytical methods. Results of the step-drawdown test recovery analysis are also included in Table 4 for completeness.

Recovery analyses are provided in Appendix B. On each recovery graph, a value for S' is given by the computer program. S' is defined as the ratio of storativity values during the pumping phase (S) and recovery phase (S"), or S' = S/S". However, dissecting the analyses to determine and fully assess various S values for different portions of the tests was seen to provide information of little importance in relation to the length of the tests and ultimate use of this data.

Analysis of P-1 Time-Drawdown Data. Time-drawdown data for P-1 is shown in Figure 11. When plotted with the Theis curve (Appendix B), the time-drawdown data for P-1 shows that the data departs below the Theis curve (i.e., there is less drawdown than expected from the model) beyond approximately 40 minutes. This indicates either leakage effects or delayed yield. For the types of sediments being tested (silty sands), delayed yield effects would have been typically expected between 10 and 100 minutes of pumping (Dawson and Istok, 1991). However, because the aquifer was over-stressed, no completion of delayed yield effects was observable such that the data did not fit any of the Neuman (1972) or Boulton (1954) type curves for unconfined aquifers. Consequently, the early time time-drawdown data were analyzed by the Theis method for confined aquifers, which best matched the data set. T and S were determined as indicated in Table 4. The Theis recovery method was applied to the recovery data for P-1 for further estimation of T.

Analysis of P-2 Time-Drawdown Data. The time drawdown curve for P-2 (Figure 11) shows that the test was not run long enough for sufficient development of a curve for confident analysis of delayed yield or partial penetration effects. Consequently, the Theis curve for confined conditions was applied. Since the data is for the initial portions of the drawdown curve and actual drawdown was very small, little confidence is given to the resulting T and S values calculated.

Analysis of Distance-Drawdown Data. The Thiem-Dupuit (Kruseman and de Ridder, 1990) analysis, for distance-drawdown analysis, was performed for the final drawdowns measured in P-1 and P-2. It is understood that the Thiem-Dupuit method is a steady-state analysis, although as the rate of change of drawdown with time becomes smaller (i.e., as steady state is approached), this method becomes more applicable. A resulting T value of 420 ft²/day was calculated, and this value is within the reasonable range reported from P-1 and MWBP-12 (Table 4).

Synthesis of Results of Aquifer Test at MWBP-12. Table 4 lists the calculated T and S values for the data collected during testing of MWBP-12. An average value for T in MWBP-12 and P-1 is 250 and 700 ft²/day, respectively. This range is believed to be representative of the aquifer material at this location. The lower values of 89 ft²/day and 60 ft²/day calculated from the recovery data from the pumping well is likely representative of the material in the immediate vicinity of the screen, but higher values calculated from the drawdown portion of the test for both the pumped well and the observation well P-1 indicate that the higher values are perhaps more indicative of long-term yield capabilities of the shallow sediments. An average transmissivity was not calculated from the response in P-2 because of the reasons presented above. This higher value is due to the pumping rate (7.5 gpm) being applied where drawdown was only 0.2 feet. Given a representative T value of 700 ft²/day, the drawdown at P-2 should have been closer to 0.9 feet (as opposed to 0.2 feet of measured drawdown), suggesting that additional recharge was occurring from an outside source, possibly from an adjacent sand bed of high permeability.

Storativity for the aquifer, obtained from the analysis at P-1, is 0.003 (Table 4). This value indicates that the amount of water released from storage is more akin to a confined aquifer than to an unconfined aquifer.

Table 5 shows the calculated and representative average T, hydraulic conductivity (K), and S values obtained from analysis of data from the aquifer test at MWBP-12. A more detailed discussion of K is included at the end of the following section.

4.2.3.2 Pumping Test Results at MWBP-05B

The constant rate test in MWBP-05B was conducted at a flow rate of 16 gpm for a period of 36 hours. A graph of drawdown versus elapsed time for MWBP-05B is shown in Figure 12. A jump of approximately 0.9 feet of drawdown is noted between 10 and 12 minutes. As in the test in MWBP-12, this was interpreted to be caused by a successive draining of thin permeable layers near to the pumping well within the cone of depression. Figure 13 shows the response of observation points P-3B and P-4A during the constant rate test. A similar break in the drawdown is noted in P-3B, but not in P-4A, indicating that the dewatered layer was at a depth similar to the pumping well. Total drawdown in P-3B and P-4A at the end of the test were 1.5 and 0.7 feet, respectively (Appendix B).

Figure 14 provides drawdown graphs for observation points P-5B and MWBP-05, which are further from MWBP-05B than P-3B and P-4A. Total drawdown in P-5B and MWBP-05 at the end of the test were 0.3 and 0.4 feet, respectively. The slightly smaller drawdown in P-5B, which

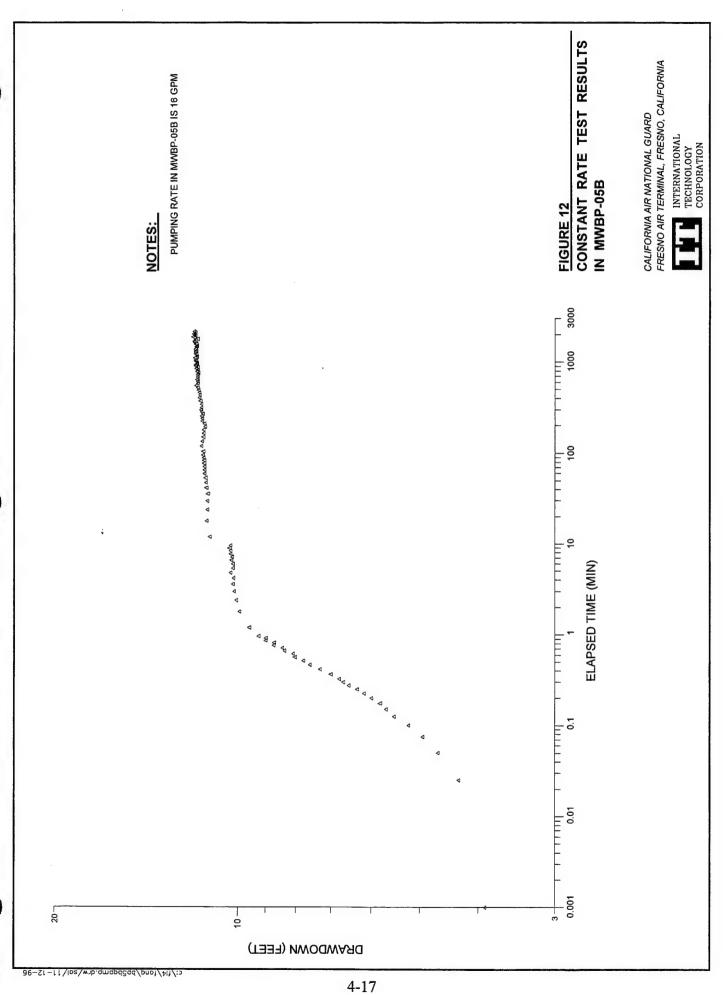
Table 5 **Calculated Average Properties** California Air National Guard, Fresno, California

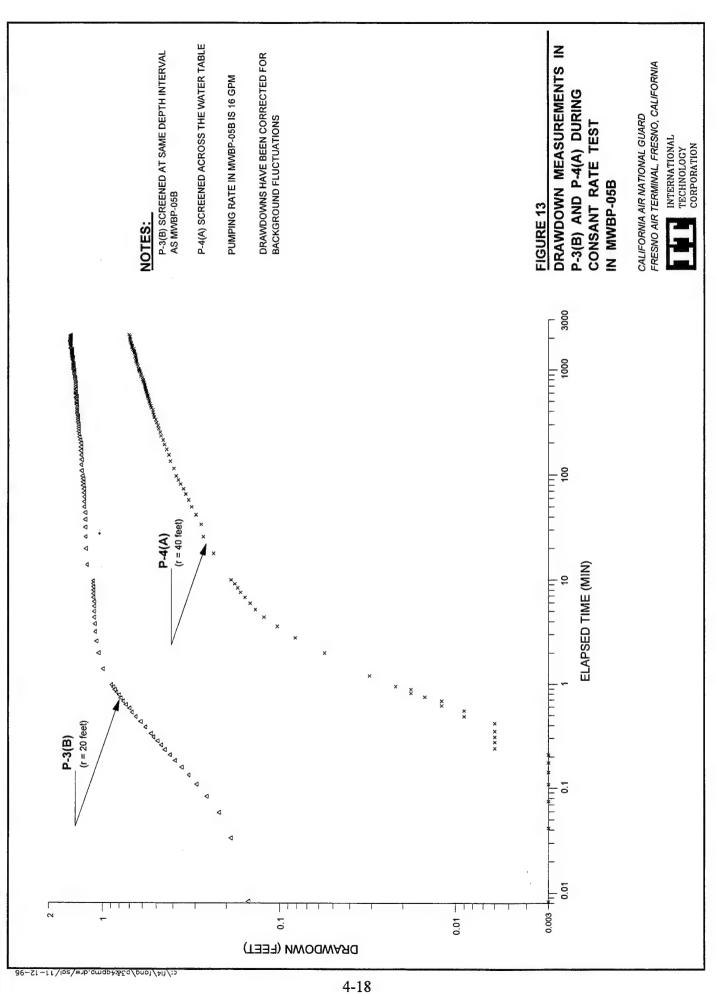
Location/Zone	Test Wells	T (ft ² /day)	S	
MWBP-12/Shallow Sediments	MWBP-12 P-1 P-2 ^a	250 700 Not used	0.003	b ^b = 45 ft K ^b = T/b = 10.2 ft/day
	Thiem-Dupuit	420		
	Average T, S	460	0.003	
MWBP-05B/Deeper Sediments	MWBP-05B P-3B P-5B ^c	1085 740 Not used	0.0002	Average of entire section:
	Thiem-Dupuit	650		$T = 1450 \text{ ft}^2/\text{day}$
	Average T, S	825	0.0002	S = 0.007
, MWBP-05B/Shallow Sediments	P-4A MWBP-05	2410 2410	0.004 0.024	b = 45 ft K = T/b = 32 ft/day
	Thiem-Dupuit	1400		
	Average T, S	2070	0.014	

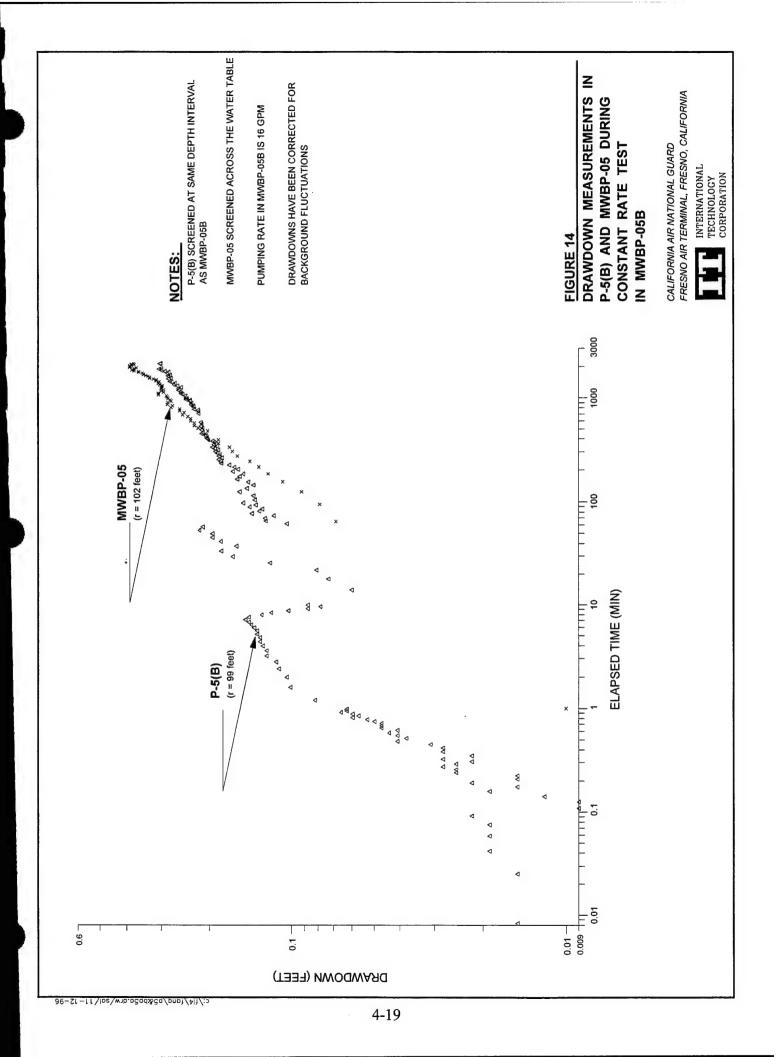
 $^{^{\}rm a}\text{P-2}$ not used due to very small drawdown and unreasonably high T values. $^{\rm b}\text{b} = \text{aquifer thickness}$

K = hydraulic conductivity

°P-5B not used due to erratic data pattern and unreasonably high T values.







is screened at the same depth interval as the pumping well, suggests that leakage was induced from overlying sediments.

Analysis of MWBP-05B Time-Drawdown Data. Drawdown data for the constant rate test are presented in Figure 12. As with MWBP-12, the Theis recovery, Papadopulos-Cooper (for large diameter wells) and Jacob straight line methods were applied to the pumping well MWBP-05B. Early time data were fit to the Papadopulos-Cooper curve whereas the Jacob method was applied to the late time data. Analysis by the Papadopulos-Cooper method more likely characterizes the sediments at the screened portion of the aquifer. These sediments comprise predominantly silts and sandy silts (Figure 6). Late-time data analysis would be expected to be more representative of the entire aquifer within the radius of influence since at later times leakage effects appear to have been induced. The late-time data would take into account the shallow sediments which comprise more coarse-grained materials (Figure 6). Transmissivity calculated with the Papadopulos-Cooper method does indicate less permeable material near the well while T from the Jacob method includes the influences from more permeable material.

Table 4 lists the calculated T values for the various analytical models. Results of the step-drawdown test recovery analysis are also included in Table 4 for completeness.

Analysis of P-3B Time-Drawdown Data. P-3B is screened at a similar elevation to MWBP-05B. The stratigraphic setting indicated that there was a strong likelihood of leakage from upper (more permeable) layers. Therefore leaky confined methods were applied (Hantush-Jacob, 1955 and Walton, 1962). The data (Figure 13) exhibits characteristics of partial penetration. Therefore, in addition to applying the methods for leaky-confined conditions, the Hantush method for partial penetration (Hantush, 1961a, 1961b) was applied, which involved derivation of the appropriate type curve. The best fit of data was obtained from the Hantush partial penetration type curve (Appendix B). Leakage (i.e., water derived from slow release from a bed above the layer being pumped) is likely to have come from an 8-foot thick sandy silt bed identified between the shallow and deeper wells. The Theis recovery method was applied to the recovery data for P-3B for further comparison of T. Table 4 lists the calculated T and S values for the various analytical methods.

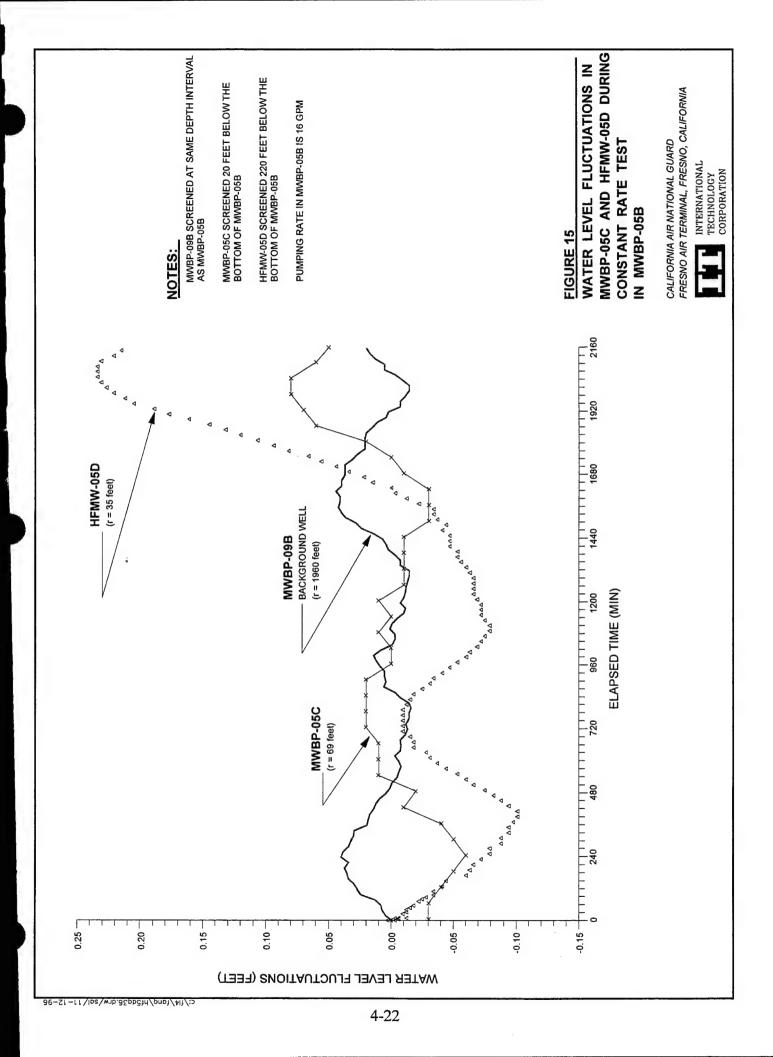
Analysis of P-5B Time-Drawdown Data. Data from P-5B (Figure 14), which is screened at a similar elevation to P-3B and MWBP-05B, shows unexplained fluctuations after 10 minutes. Because there was no explanation for these fluctuations, the first 10 minutes of data only were analyzed. Because of the short time period of data for analysis, the Theis curve was fitted to the

log-log data and the Jacob straight line method was applied for the semi-log data plot. Both of these methods are applicable to confined aquifers. The Theis recovery method was applied to the recovery data for P-5B for further estimation of T. The calculated values of T were unreasonably high when compared to the analyses from P-3B and MWBP-05B (Table 4); therefore, little confidence was given to the values of T and S calculated from P-5B.

Analysis of P-4A Time-Drawdown Data. The drawdown response in observation point P-4A (Figure 13), which is screened in the upper portion of the aquifer, is characteristic of a confined aquifer response. No partial penetration or leakage effects are noted in the drawdown response. Consequently the Theis curve was applied to the time drawdown data. The Theis recovery method was applied to the recovery data for P-5B for comparison of T. The calculated T and S for P-4A are presented in Table 4. The relatively high T value indicates the heterogeneous nature of the aquifer, i.e., there is a greater percentage of coarse-grained aquifer material screened in the shallower wells (A-series) when compared to the deeper wells (B-series) (Figure 6).

Analysis of MWBP-05 Time-Drawdown Data. The drawdown response in observation point MWBP-05 (Figure 14), which is screened in the upper portion of the aquifer (similar to P-4A) is characteristic of a confined aquifer. Consequently the Theis curve was applied to the time drawdown data. The Theis recovery method was applied to the recovery data for P-5B for comparison of T. The calculated T and S for MWBP-05 are presented in Table 4. The T value calculated from the drawdown portion of the test is the same as the value of T calculated for P-4A. No partial penetration or leakage effects are noted in the drawdown response. However, after approximately 1500 minutes the drawdown curve indicates more drawdown than would be anticipated (the data departs above the Theis curve) which may indicate the presence of a barrier boundary (i.e., possible facies change). The test was not run long enough to allow evaluation of the possible barrier boundary. The T value calculated from the recovery portion of the test is relatively high in comparison to the T obtained from the drawdown portion of the test.

Analysis of MWBP-05C and HFMW-05D Time-Drawdown Data. Figure 15 shows water level fluctuations in deep wells MWBP-05C (screened at a depth 20 to 30 feet below the bottom of the pumping well) and HFMW-05D (screened 220 feet below the pumping well). Water level fluctuations in the background well (MWBP-09B) are also displayed in Figure 15. Figure 15 shows that no drawdown response was induced in either well due to pumping in MWBP-05B. This is more significant in MWBP-05C than in HFMW-05D. Two hypotheses are proposed, although neither can be proved or disproved from the pumping test: (1) the pumping rate of 16



gpm was insufficient to alter the deeper potentiometric lines such that no significant upward flow to the pumping well was created, or (2) a barrier to flow exists between MWBP-05B and MWBP-05C, thereby separating the two flow systems. Chemical sampling data (Table 3) tends to support the second hypothesis in that PCE was detected in the intermediate-depth well (MWBP-05B), but not in the deep well (MWBP-05C).

If a retarding layer is present between the "B" and "C" zones, it is likely a fine-grained silt layer above well MWBP-05C (Figure 6). The aquitard unit displayed in Figure 6 that is present between wells MWBP-06B and MWBP-06C and MW5-01B and MW5-01C may very well extend beneath MWBP-05B. The top elevation of this layer is approximately 194 feet and groundwater is measured at 239 feet. Therefore, the aquifer thickness (b) is 45 feet. Since hydraulic conductivity (K) equals T/b, K near MWBP-12 = 10.2 ft/day and near MWBP-05B = 32 ft/day (Table 5).

Analysis of Distance-Drawdown Data. Thiem-Dupuit distance-drawdown analysis was performed for the wells associated with MWBP-05B. The calculated T value is presented in Table 4.

Synthesis of Results of Aquifer Test at MWBP-05B. Table 4 lists the calculated T and S values for the data collected during testing of MWBP-05B. Table 5 lists the various average T values calculated for both shallow and deep zones during the test in MWBP-05B. The range of values shows the heterogeneity of the aquifer, as is expected from the alluvial type of composition. From Table 5, the average T for the shallow portion is approximately 2,070 ft²/day, while for the deeper portion it is 825 ft²/day. T values derived from recovery data were not used to calculate an average T. When all of the pumping phase values for the analyses are averaged, T for the entire thickness is approximately 1,450 ft²/day. Storativity values from the individual analyses ranged from 0.0002 to 0.024. Higher values were calculated from the shallow sediments. The lower value of 0.0002 was derived from the analysis for P-3B, indicating that water was not released by gravity drainage, but from storage or leakage from above.

4.2.4 Summary and Discussion

It is apparent from the results of the aquifer test analyses that the saturated sediments in the southwestern portion of the Base have highly variable hydraulic properties. Average transmissivity for the uppermost material at MWBP-12 is 460 ft²/day, whereas near MWBP-05B, it approaches 2,070 ft²/day, illustrating the anisotropic nature of the sediments. Deeper sediments around MWBP-05B have an average T of 825 ft²/day, indicating sediments similar in properties

to the sediments at MWBP-12. A reasonable transmissivity value through the entire sediment thickness at MWBP-05B is 1,450 ft²/day.

The derived hydraulic conductivity (K) around MWBP-12 is 10.2 ft/day, whereas K through the entire portion of material at MWBP-05B is 32 ft/day.

Observation well responses during the test in MWBP-05B show that the "A" and "B" sections are connected and should be considered one unit. This fact suggests that if a groundwater extraction system were to be installed at any point in the future, then it should be designed to intercept the entire aquifer thickness if hydraulic control is a remedial goal. Determining hydraulic properties of small intervals within the upper unit has importance, but has limited value in designing a remedial system. What the aquifer tests demonstrate best is that the individual layers with higher contaminant concentrations can indeed be stressed and can affect a limited radius of influence. If hydraulic control is a remedial objective, then a fully penetrating well would be better suited.

Aquifer tests at MWBP-12 determined that an extraction well with a similar design would be of nominal value in affecting large areas of the PCE plume and several wells would have to be installed to create a barrier across the width of the plume. Tests in MWBP-05B showed that an extraction well with a similar design could produce greater water and affect a larger area. It would also be able to draw water from the more impacted (shallower) zones. However, a well installed through the entire thickness would provide greater efficiency in capturing contaminated groundwater.

5.0 Summary of Events and Findings

Objectives of the field events associated with the pump tests were accomplished:

- A second round of groundwater samples was collected from the eight deep wells
 installed during the deep aquifer investigation. Results confirmed the findings of
 earlier samples in that PCE was not detected in the "C" series wells and was only
 detected in wells at, and downgradient of, the BCP.
- Pumping tests were performed that demonstrated that the "A" and "B" portions of the aquifer are well connected and can be considered part of the same aquifer system.
- Analysis of the pumping test data provided estimates of hydraulic properties of the saturated material around the two test sites.

Responses of observation wells during the pumping tests and background monitoring provided the following understanding of the aquifer system:

- The uppermost water-bearing zone behaves as a confined or semiconfined aquifer.
 This is thought to be due to fine-grained layers directly overlying the water surface, which inhibit the downward migration of water and the dissipation of atmospheric pressure changes. Responses during the pumping tests were similar to a confined aquifer.
- Shallow sediments around MWBP-12 have a representative transmissivity value of 460 ft²/day with a storativity of 0.003. Transmissivity around MWBP-05B has a reasonable value of 1,450 ft²/day and a storativity of 0.007. With a saturated thickness of 45 feet, hydraulic conductivity at MWBP-12 is 10.2 ft/day and at MWBP-05B is 32 ft/day.
- The flow system between the "B" and "C" zones may be separated by a low permeability layer. This is suggested by the lack of water level response in the "C" well when pumping MWBP-05B and by the absence of PCE contamination in groundwater at lower zones. However, contamination by other compounds does exist in deeper aquifer zones, indicating some pathway for migration to deeper regions. More permeable water bearing zones are therefore interconnected across the western portion of the Base.

6.0 References

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APPENDIX A

STEP-DRAWDOWN TEST SUMMARY DATA AND RECOVERY ANALYSIS

Table A-1 Step-Drawdown Test Data Summary for MWBP-12

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Discha	rge	Step	Elapsed	MWBP-12	P-1
Rate	-	Time	Test Time	Drawdown	Drawdown
(gpm	1)	(min)	(min)	(ft)	(ft)
	2.5	0	0	0.003	0.003
		0.5	0.5	0.044	0.003
		1	1	0.807	0.019
		2	2	0.924	0.019
		3	3	1.126	0.072
		4	4	1.224	0.091
		5	5	1.284	0.11
		6	6	1.331	0.123
		7	7	1.356	0.133
		8	8	1.385	0.139
		9	9	1.397	0.155
		10	10	1.394	0.155
		20	20	1.46	0.183
		28	28	1.486	0.19
		0	30	1.483	0.199
	5	0.0083	30.0083	1.486	0.199
	Ū	0.5	30.5	1.959	0.202
		1	31	2.24	0.218
		2	32	2.549	0.25
		3	33	2.719	0.269
		4	34	2.814	0.285
		5	35	2.864	0.297
		6	36	2.899	0.307
		7	37	2.949	0.317
		8	38	3	0.326
		9	39	3.037	0.336
		10	40	3.063	0.345
		16	46	3.138	0.374
		20	50	3.167	0.383
		30	60	3.211	0.399
		40	70	3.233	0.408
		50	80	3.242	0.408
	6.5	0.0083	80.0083	3.302	0.412
	0.0	0.5	80.5	3.715	0.418
		1	81	3.901	0.427
		2	82	4.157	0.443
		3	83	4.296	0.456
		4	84	4.387	0.465
		5	85	4.459	0.475
		6	86	4.541	0.485
		7	87	4.576	0.491
		8	88	4.601	0.497
		9	89	4.639	0.504
		10	90	4.667	0.507
		14	94	4.724	0.523
		20	100	4.771	0.535
		30	110	4.816	0.548
		50	1,0	7.010	0.040

Table A-1
Step-Drawdown Test Data Summary for MWBP-12

(Page 2 of 2)

	(Page 2 of 2)					
Discharge	Step	Elapsed	MWBP-12	P-1		
Rate	Time	Test Time	Drawdown	Drawdown		
(gpm)	(min)	(min)	(ft)	(ft)		
	40	120	4.901	0.561		
	50	130	4.961	0.573		
	60	140	4.998	0.586		
	70	150	5.024	0.589		
7.0	0.0083	150.0083	5.09	0.589		
	0.5	150.5	5.2	0.595		
	1	151	5.282	0.595		
	2	152	5.373	0.602		
	3	153	5.414	0.602		
	4	154	5.468	0.605		
	5	155	5.465	0.608		
	6	156	5.49	0.608		
	7	157	5.5	0.611		
	8	158	5.477	0.611		
	9	159	5.474	0.611		
	10	160	5.471	0.611		
	14	164	5.481	0.618		
	20	170	5.544	0.618		
	30	180	5.547	0.627		
	40	190	5.622	0.64		
	50	200	5.61	0.633		
	60	210	5.626	0.64		
	0.0083	210.0083	5.572	0.64		
	0.0003	210.0003	4.8	0.637		
0.0	0.1	210.1	4.258	0.633		
Recovery	0.2	210.2	3.883	0.627		
Data	0.3	210.3	3.536	0.621		
Data	0.5	210.4	3.265	0.614		
	0.5	210.5	3.203	0.608		
	0.7	210.7	2.851	0.599		
	0.7	210.7	2.678	0.592		
	0.9	210.0	2.53	0.586		
	1	210.3	2.394	0.576		
	2	212	1.441	0.504		
	3	213	1.019	0.437		
	4	213	0.76	0.383		
	5	214	0.70	0.342		
	6		0.508	0.342		
	7	216 217	0.506	0.301		
	8	217	0.432	0.272		
	9	219	0.376	0.23		
	10	219	0.34	0.228		
	12	220	0.302	0.212		
	14	222	0.252	0.163		
	20	230	0.142	0.101		
	26	236	0.142	0.095		
	28	238	0.104	0.093		
	20	230	0.091	0.031		

Table A-2 Step-Drawdown Test Data Summary for MWBP-05B

(Page 1 of 2)

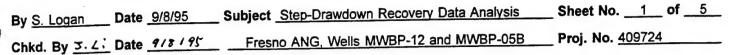
(rage 1 012)					
Discharge	Step	Elapsed	MWBP-05B	P-3B	P-4A
Rate	Time	Test Time	Drawdown	Drawdown	Drawdown
(gpm)	(min)	(min)	(ft)	(ft)	(ft)
6	0	0	3.401	0.094	-0.025
	0.5	0.5	3.185	0.443	0.009
	1	1	3.427	0.398	0.015
	2	2	3.649	0.436	0.028
	3	3	3.675	0.449	0.038
	4	4	3.687	0.462	0.041
	5	5	3.687	0.462	0.019
	6	6	3.719	0.468	0.047
	7	7	3.732	0.462	0.047
	8	8	3.738	0.468	0.047
	9	9	3.745	0.468	0.047
	10	10	3.713	0.468	0.044
	14	14	3.725	0.468	0.06
	20	20	3.706	0.474	0.057
	30	30	3.719	0.474	0.069
	40	40	3.725	0.474	0.063
	44	44	3.725	0.481	0.085
12	0.0083	44.0083	3.776	0.474	0.079
	0.5	44.5	5.714	0.613	0.076
	1	45	6.718	0.74	0.088
	2	46	7.454	0.86	0.104
	3	47	7.613	0.892	0.114
	4	48	7.607	0.905	0.12
	5	49	7.626	0.911	0.129
	6	50	7.594	0.911	0.129
	7	51	7.651	0.911	0.133
	8	52	7.638	0.905	0.133
	9	53	7.588	0.905	0.136
	10	54	7.581	0.905	0.142
	14	58	7.619	0.911	0.148
	20	64	7.772	0.924	0.158
	30	74	7.778	0.93	0.168
	40	84	7.746	0.924	0.18
	50	94	7.81	0.924	0.183
	60	104	7.797	0.924	0.196
	70	114	7.784	0.924	0.199
	80	124	7.841	0.93	0.209
	90	134	7.784	0.936	0.218
	100	144	7.772	0.936	0.231
	120	164	7.721	0.924	0.24
	130	174	7.835	0.936	0.253
18	0.0083	174.0083	7.905	0.911	0.234
	0.5	174.5	10.063	1.069	0.237
	1	175	11.173	1.202	0.244
	2	176	12.036	1.316	0.266
	3	177	12.327	1.354	0.282
	4	178	12.264	1.36	0.269

Table A-2 Step-Drawdown Test Data Summary for MWBP-05B

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Discharge	Step	Elapsed	MWBP-05B	P-3B	P-4A
Rate	Time	Test Time	Drawdown	Drawdown	Drawdown
(gpm)	(min)	(min)	(ft)	(ft)	(ft)
	5	179	12.245	1.36	0.177
	6	180	12.257	1.367	0.256
	7	181	12.473	1.373	0.282
	8	182	12.581	1.392	0.294
	9	183	12.67	1.398	0.304
	10	184	12.714	1.398	0.31
	14	188	12.663	1.405	0.326
	20	194	13.031	1.442	0.345
	30	204	12.923	1.43	0.358
	40	214	12.949	1.43	0.37
	50	224	13.044	1.43	0.38
	60	234	13.113	1.442	0.399
	70	244	13.126	1.449	0.408
19	0.0083	244.0083	13.151	1.461	0.408
	0.5	244.5	12.498	1.474	0.412
	1	245	8.089	1.044	0.389
	2	246	8.114	0.892	0.348
	3	247	12.619	1.322	0.367
	4	248	13.627	1.468	0.393
	5	249	13.842	1.506	0.405
	6	250	13.912	1.525	0.402
	7	251	13.912	1.525	0.412
	8	252	13.95	1.518	0.418
	9	253	13.861	1.525	0.421
	10	254	13.931	1.525	0.424
	14	258	13.887	1.525	0.412
	20	264	13.868	1.518	0.437
	24	268	13.836	1.518	0.44
0.0	0.0083	268.0083	12.923	1.455	0.431
Recovery	0.1	268.1	11.332	1.436	0.431
Data	0.2	268.2	9.682	1.354	0.431
	0.3	268.3	8.273	1.253	0.424
	0.4	268.4	7.061	1.145	0.418
	0.5	268.5	6.025	1.037	0.405
	0.6	268.6	5.136	0.936	0.399
	0.7	268.7	4.38	0.848	0.393
	0.8	268.8	3.738	0.759	0.374
	0.9	268.9	3.185	0.683	0.358
	1	269	2.721	0.613	0.345
	2	270	0.591	0.234	0.247
	3	271	0.178	0.12	0.199
	4	272	0.082	0.094	0.177
	5	273	0.057	0.075	0.161
	6	274	0.044	0.069	0.155
	7	275	0.031	0.063	0.148
	8	276	0.038	0.056	0.142
	9	277	0.031	0.056	0.139





1.0 Objective

To estimate aquifer parameters from step-drawdown test recovery data using the method of analysis given in Kawecki (1993).

2.0 Background

Step-drawdown tests were performed in two monitoring wells at the Fresno Air National Guard Base in Fresno, California. The wells tested were MWBP-12 and MWBP-05B. Well MWBP-12 is 4 inches in diameter and is installed to a depth of 92.5 feet below ground surface (bgs). It is screened from 92.5 to 72.5 feet bgs; groundwater occurs at 80.6 feet bgs.

Well MWBP-05B has a diameter of 5 inches and is installed to a depth of 116 feet bgs. It is screened from 116 to 106 feet bgs; groundwater was measured at 80.2 feet bgs at the start of the test.

Traditionally, step-drawdown tests are performed to estimate well efficiencies and specific yields. These analyses are not pertinent in this case because the wells are monitoring wells and were not designed to be extraction/production wells. Step-drawdown tests were run in order to assess the yields of each well for subsequent, more sustained aquifer tests. However, an estimate of the aquifer parameters can be obtained from a fairly recent analysis method published by Kawecki (1993).

2.1 Method

Kawecki states that the popular recovery method of Theis (Theis, 1935; Kruseman and deRidder, 1983) is used to estimate transmissivity by analyzing data from the recovery data from a constant rate discharge test. The equations in the stepped discharge recovery method are a direct extension of the Theis recovery method. If the pump test comprises only one pumping rate and a recovery stage, then the Kawecki method reduces to the Theis recovery method.

Kawecki develops the following equation for residual drawdown (s"):

$$s''(t) = \frac{2.3}{4\pi T} \log[F(t)]$$
 (1)

where s"(t) is the residual drawdown at any post-pumping time "t" and T is the aquifer transmissivity. The function F(t) is a time function given by:

$$F(t) = \left(\frac{t-t_1}{t-t_2}\right)^{Q_1} \times \left(\frac{t-t_2}{t-t_3}\right)^{Q_2} \times \ldots \times \left(\frac{t-t_{N-1}}{t-t_N}\right)^{Q_{N-1}}$$
(2)

Equations (1) and (2) are the basis for the stepped discharge recovery method.

2.2 Explanation

The time function F(t) is calculated for each recovery time, t ($t > t_N$), where a recovery measurement is recorded. Q_1 through Q_{N-1} are the consecutive pumping rates for the test and t_1 through t_{N-1} are the cumulative times at which the pumping rates were changed. The time value for t1 is the beginning of the



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first step, or t = 0, and t_2 is the end of step 1 and the beginning of step 2. Q_N is the last pump rate, defined as the recovery period, or in other words, Q = 0. Likewise, t_N is the elapsed time from the beginning of the test when the recovery period began. The logarithm₁₀ of F(t) is then calculated.

An arithmetic graph of residual drawdown vs corresponding values for $\log_{10}[F(t)]$ is then constructed and a straight line is fitted to the data. The slope of the straight line is calculated; the slope is equal to $(2.3/4\pi T)$. Then the transmissivity is found by:

$$T = \frac{2.3}{4\pi \times slope} \tag{3}$$

2.3 Units

Equation (2) provides F(t) in interesting units. Suppose that the time measurements are in minutes and the pumping rate is in gallons per minute (gpm). The corresponding units are therefore (min/min)^{gpm}. When the logarithm is calculated, the units become simply gpm.

The slope from the straight line also has units which bear some clarification. Slope, by definition, is rise/run, or $\Delta y/\Delta x$. The y-value on the plot is the residual drawdown, measured in feet, for example. In order for the units to cancel correctly, the pumping rate must be converted into ft^3/min . This must be done within the F(t) calculations before it is plotted. Then the unit of the slope is equal to $(ft/ft^3/min)$ which is equal to min/ft^2 .

The units in Eq. (3) are then resolved into meaningful units for transmissivity.

3.0 Step-Drawdown Tests

Step-drawdown tests were performed in two wells at the Fresno ANG Base in March 1995. Pumping rates and step durations are provided in Table 1. Residual drawdown measurements were collected electronically



By S. Logan Date 9/8/95 Subject Step-Drawdown Recovery Data Analysis Sheet No. 3 of 5

Chkd. By 5.4: Date 9/8/95 Fresno ANG, Wells MWBP-12 and MWBP-05B Proj. No. 409724

Table 1 Step-Drawdown Summary Information

Step No.	Step Duration (min)	Elapsed Time (min)	Flow Rate (gpm)	Flow Rate (ft³/min)		
Well MWBP-	12					
1.	30	30	2.5	0.334		
2	50	80	5	0.669		
3	70	150	6.5	0.869		
4	60	210	7	0.936		
5	NA	NA	0	0		
MWBP-05B						
1	44	44	6	0.802		
. 2	130	174	12	1.605		
3	70	244	18	2.408		
4	24	268	19	2.542		
5	NA	NA	0	0		

with pressure transducers and a data logger. Graphs of drawdown versus time are included for each well in Attachment 1. Attachment 2 contains the residual drawdown (recovery) data for each test and the spreadsheets with the calculations for F(t) and log[F(t)].

4.0 Example Calculation

The following example for calculating F(t) is taken from the data for MWBP-12 at recovery time 0.1 minutes (min). The total test duration was 210 min, so $t_n = 210.1$ min and $t_1 = 0$, $t_2 = 30$, $t_3 = 80$, $t_4 = 150$, and $t_5 = 210$ min (see Table 1). Step pumping rates are also in Table 1 with $Q_1 = Q$ for step 1, etc. The calculation for F(t) at $t_n = 210.1$ min is as follows:

$$F(t) = \left(\frac{210.1 - 0}{210.1 - 30}\right)^{0.334} \times \left(\frac{210.1 - 30}{210.1 - 80}\right)^{0.668} \times \left(\frac{210.1 - 80}{210.1 - 150}\right)^{0.869} \times \left(\frac{210.1 - 150}{210.1 - 210}\right)^{0.936} (4)$$

Equation 4 reduces to:



By S. Logan Date 9/8/95 Subject Step-Drawdown Recovery Data Analysis Sheet No. 4 of 5

Chkd. By 5. 4: Date 9/8/95 Fresno ANG, Wells MWBP-12 and MWBP-05B Proj. No. 409724

$$F(t) = (1.1666)^{0.334} \times (1.3843)^{0.668} \times (2.1647)^{0.869} \times (601.0)^{0.936}$$

$$F(t) = 1.0528 \times 1.2426 \times 1.9564 \times 399.0493 = 1021.32$$

and the log(1021.32) = 3.0092.

This calculation is then performed for each recovery measurement. The spreadsheets in Attachment 2 were developed to perform these calculations. The graph for log[F(t)] vs. residual drawdown for MWBP-12 is shown in Attachment 2; also shown on the graph is the selected straight line fit. The slope of the line is:

Slope =
$$\left(\frac{4.5-0.5 (ft)}{2.78-1.43 (ft^3/min)}\right) = 2.96 min/ft^2$$

From Eq. 3, the transmissivity, T, is $0.062 \text{ ft}^2/\text{min} = 89 \text{ ft}^2/\text{day}$.

5.0 Results

Table 2
Summary of Recovery Analysis

Well ID	Slope from Graphs (min/ft²)	T (ft²/day)
MWBP-12	2.946.	89
MWBP-05B	4.23	62

Attachment 2 contains the recovery data curves, selected straight line fits, slope calculations and T-value calculations.

6.0 Discussion

Once a spreadsheet is developed for handling the tedious F(t) calculations, this method is relatively simple to implement. However, it is highly dependent on the interpretation for the straight line. A linear regression can also be evaluated to provide a second assessment of the slope. These are listed at the end of the spreadsheets in Attachment 2.



By S. Logan Date 9/8/95 Subject Step-Drawdown Recovery Data Analysis Sheet No. 5 of 5

Chkd. By 5.4 Date 9/8/95 Fresno ANG, Wells MWBP-12 and MWBP-05B Proj. No. 409724

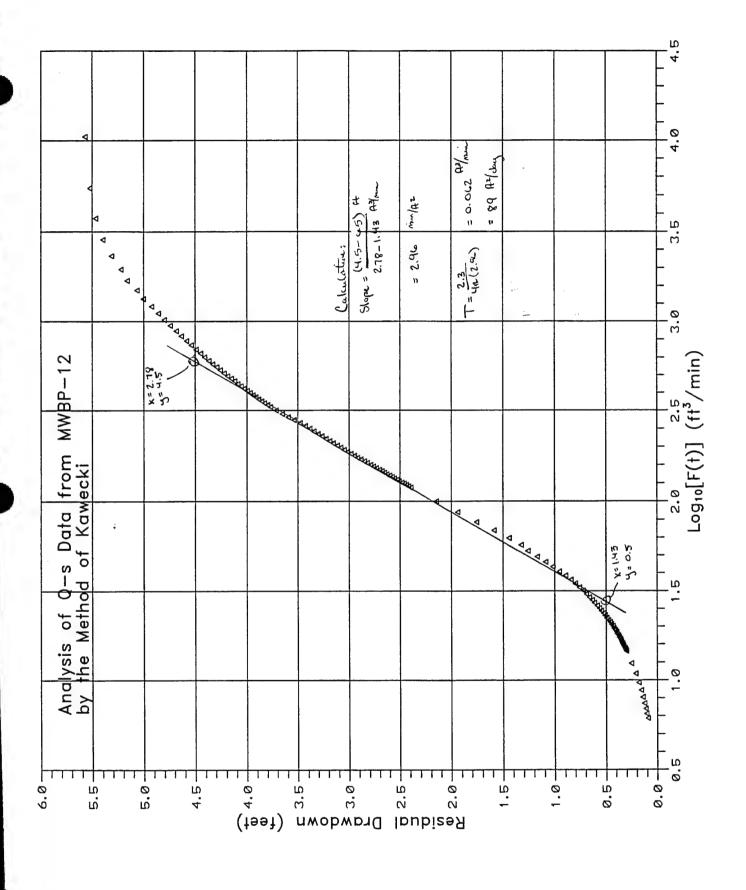
7.0 References

Kawecki, M. W., 1993, "Recovery Analysis from Pumping Tests with Stepped Discharge," Groundwater, Vol. 31, No. 4, pp. 585-592.

Kruseman, G. P., N. A. deRidder, 1990, Analysis and Evaluation of Pumping Test Data, International Institute for Land Reclamation and Improvement, Wageningen, The Netherlands, Second edition, 377 pp.

Theis, C. V., 1935, The Relation Between the Lowering of the Piezometric Surface and the Rate and Duration of Discharge of a Well Using Groundwater Storage, Transactions, American Geophysical Union, Vol. 16, pp. 519-524.

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Pum	pina	Data
	ping	Dutu

	Elapsed Time (min)	Flow Rate (gpm)	Flow Rate (cu.ft/min)	
Q_1, t_1	0	. 2.5	0.334	
Q_2 , t_2	30	5	0.668	
Q_3, t_3	80	6.5	0.869	
Q ₄ , t ₄	150	7	0.936	
Q ₅ , t ₅	210	0	0	

		Recovery Dat	a		
	Elapsed	Residual			Residual
	Recovery Time	Drawdown			Drawdown
	(min)	MWBP-12	F(t)	log[F(t)]	MWBP-12
0.0083	210.0083	5.572	10487.84	4.0207	5.572
0.0166	210.0166	5.525	5482.061	3.7389	5.525
0.025	210.025	5.468	3736.934	3.5725	5.468
0.0333	210.0333	5.396	2857.601	3.4560	5.396
0.0416	210.0416	5.314	2320.385	3.3656	5.314
0.05	210.05	5.219	1953.519	3.2908	5.219
0.0583	210.0583	5.159	1692.037	3.2284	5.159
0.0666	210.0666	5.065	1493.915	3.1743	5.065
0.075	210.075	5.002	1336.788	3.1261	5.002
0.0833	210.0833	4.923	1211.764	3.0834	4.923
0.0916	210.0916	4.857	1108.74	3.0448	4.857
÷ 0.1	210.1	4.8	1021.377	3.0092	4.8
0.1083	210.1083	4.74	947.973	2.9768	4.74
0.1166	210.1166	4.683	884.7088	2.9468	4.683
0.125	210.125	4.633	828.9812	2.9185	4.633
0.1333	210.1333	4.582	780.6088	2.8924	4.582
0.1416	210.1416	4.538	737.7365	2.8679	4.538
0.15	210.15	4.491	699.0324	2.8445	4.491
0.1583	210.1583	4.447	664.7014	2.8226	4.447
0.1666	210.1666	4.409	633.6872	2.8019	4.409
0.175	210.175	4.368	605.2034	2.7819	4.368
0.1833	210.1833	4.33	579.5446	2.7631	4.33
0.1916	210.1916	4.292	556.0409	2.7451	4.292
0.2	210.2	4.258	534.1794	2.7277	4.258
0.2083	210.2083	4.22	514.2568	2.7112	4.22
0.2166	210.2166	4.185	495.8141	2.6953	4.185
0.225	210.225	4.15	478.4919	2.6799	4.15
0.2333	210.2333	4.119	462.5633	2.6652	4.119
0.2416	210.2416	4.087	447.6954	2.6510	4.087
0.25	210.25	4.056	433.6225	2.6371	4.056
0.2583	210.2583	4.028	420.5883	2.6239	4.028
0.2666	210.2666	3.996	408.3405	2.6110	3.996
0.275	210.275	3.968	396.6746	2.5984	3.968
0.2833	210.2833	3.939	385.806	2.5864	3.939
0.2916	210.2916	3.911	375.5369	2.5747	3.911
0.3	210.3	3.883	365.7047	2.5631	3.883
0.3083	210.3083	3.854	356.4993	2.5521	3.854

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		5.4			
	-, ,	Recovery Data			Desident
	Elapsed	Residual			Residual
	Recovery Time		Ε(Δ)	I==(E/A)1	Drawdown
0.0400	(min)	MWBP-12	F(t)	log[F(t)]	MWBP-12
0.3166	210.3166	3.826	347.7617	2.5413	3.826
0.325	210.325	3.797	339.359	2.5307	3.797
0.3333	210.3333	3.769	331.4593	2.5204	3.769
0.35	210.35	3.712	316.6654	2.5006 2.4818	3.712
0.3666	210.3666	3.652	303.2551	2.4617	3.652 3.592
0.3833	210.3833	3.592	290.9002		
0.4	210.4	3.536	279.5454	2.4465	3.536
0.4166	210.4166	3.479	269.1332	2.4300	3.479
0.4333	210.4333	3.428	259.4385	2.4140	3.428
0.45	210.45	3.384	250.4412	2.3987	3.384
0.4666	210.4666	3.343	242.1165	2.3840	3.343
0.4833	210.4833	3.302	234.3008	2.3698	3.302
0.5	210.5	3.265	226.9912	2.3560	3.265
0.5166	210.5166	3.227	220.1792	2.3428	3.227
0.5333	210.5333	3.189	213.7408	2.3299	3.189
0.55	210.55	3.154	207.6814	2.3174	3.154
0.5666	210.5666	3.116	202.0012	2.3054	3.116
0.5833	210.5833	3.082	196.603	2.2936	3.082
0.6	210.6	3.047	191.4959	2.2822	3.047
0.6166	210.6166	3.012	186.6851	2.2711	3.012
0.6333	210.6333	2.981	182.0918	2.2603	2.981 2.946
0.65	210.65 210.6666	2.946 2.914	177.7273 173.5989	2.2498 2.2395	2.946
0.6666 0.6833	210.6833	2.883	169.6417	2.2395	2.883
0.0033	210.0033	2.851	165.8675	2.2198	2.851
0.7166	210.7166	2.823	162.2848	2.2193	2.823
0.7333	210.7333	2.788	158.839	2.2010	2.788
0.75	210.755	2.76	155.542	2.1918	2.76
0.7666	210.7666	2.732	152.4026	2.1830	2.732
0.7833	210.7833	2.703	149.3743	2.1743	2.703
0.7033	210.7653	2.678	146.4686	2.1657	2.678
0.8166	210.8166	2.653	143.6944	2.1574	2.653
0.8333	210.8333	2.628	141.0115	2.1493	2.628
0.85	210.85	2.602	138.4307	2.1412	2.602
0.8666	210.8666	2.577	135.9609	2.1334	2.577
0.8833	210.8833	2.555	133.5669	2.1257	2.555
0.9	210.9	2.53	131.2591	2.1181	2.53
0.9166	210.9166	2.508	129.0457	2.1107	2.508
0.9333	210.9333	2.482	126.896	2.1034	2.482
0.95	210.95	2.46	124.8196	2.0963	2.46
0.9666	210.9666	2.438	122.8244	2.0893	2.438
0.9833	210.9833	2.416	120.8831	2.0824	2.416
1	211	2.394	119.0046	2.0756	2.394
1.2	211.2	2.145	100.456	2.0020	2.145
1.4	211.4	1.94	87.06408	1.9398	1.94
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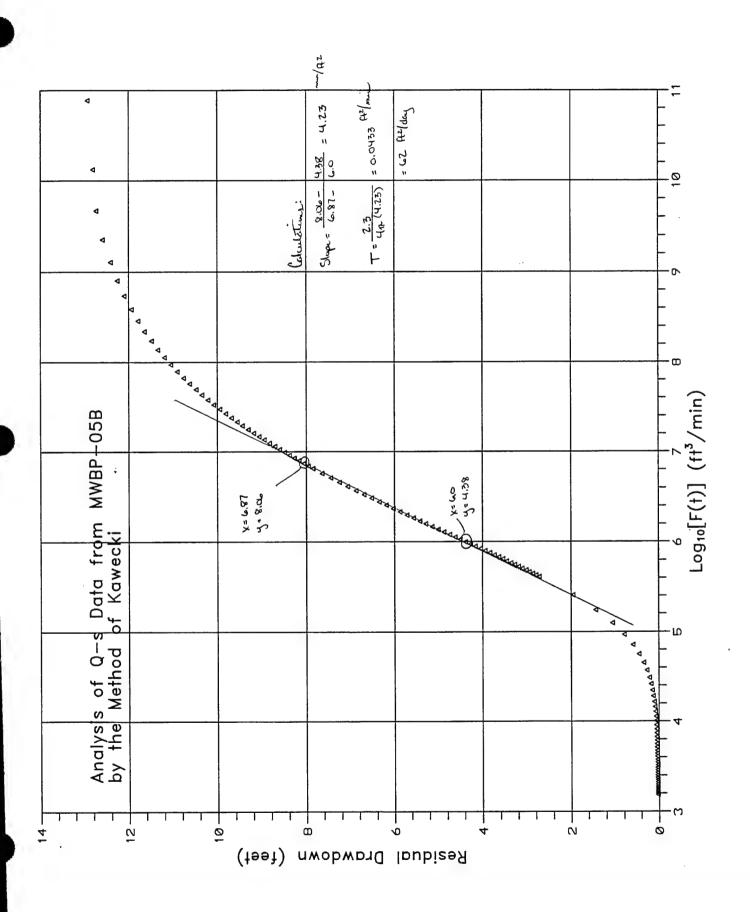
		Recovery Data	a		
	Elapsed	Residual			Residual
	Recovery Time	Drawdown			Drawdown
	(min)	MWBP-12	F(t)	log[F(t)]	MWBP-12
1.6	211.6	1.757	76.92774	1.8861	1.757
1.8	211.8	1.587	68.98073	1.8387	1.587
2	212	1.441	62.57798	1.7964	1.441
2.2	212.2	1.325	57.30598	1.7582	1.325
2.4	212.4	1.259	52.88726	1.7234	1.259
2.6	212.6	1.17	49.12856	1.6913	1.17
2.8	212.8	1.091	45.89113	1.6617	1.091
3	213	1.019	43.07269	1.6342	1.019
3.2	213.2	0.956	40.59617	1.6085	0.956
3.4	213.4	0.896	38.4024	1.5844	0.896
3.6	213.6	0.842	36.44516	1.5616	0.842
3.8	213.8	0.801	34.68783	1.5402	0.801
4	214	0.76	33.10102	1.5198	0.76
4.2	214.2	0.722	31.66082	1.5005	0.722
4.4	214.4	0.691	30.34765	1.4821	0.691
4.6	214.6	0.662	29.14527	1.4646	0.662
4.8	214.8	0.634	28.04008	1.4478	0.634
5	215	0.612	27.02067	1.4317	0.612
5.2	215.2	0.586	26.07733	1.4163	0.586
5.4	215.4	0.564	25.20178	1.4014	0.564
5.6	215.6	0.545	24.38689	1.3872	0.545
5.8	215.8	0.523	23.62652	1.3734	0.523
6	216	0.508	22.91533	1.3601	0.508
6.2	216.2	0.492	22.24864	1.3473	0.492
6.4	216.4	0.476	21.62237	1.3349	0.476
6.6	216.6	0.46	21.03292	1.3229	0.46
6.8	216.8	0.448	20.47711	1.3113	0.448
7	217	0.432	19.95211	1.3000	0.432
7.2	217.2	0.422	19.45539	1.2890	0.422
7.4	217.4	0.41	18.98473	1.2784	0.41
7.6 7.8	217.6	0.397	18.53809 18.11368	1.2681 1.2580	0.397 0.391
8	217.8 218	0.391 0.378	17.70984	1.2482	0.391
8.2	218.2	0.378	17.32512	1.2387	0.369
8.4	218.4	0.359	16.95817	1.2394	0.359
8.6	218.4	0.353	16.60778	1.2294	0.353
8.8	218.8	0.333	16.27284	1.2115	0.333
9	219	0.347	15.95234	1.2028	0.34
9.2	219.2	0.331	15.64536	1.1944	0.331
9.4	219.4	0.325	15.35105	1.1861	0.325
9.4	219.4	0.325	15.06864	1.1781	0.325
9.8	219.8	0.319	14.79741	1.1702	0.309
10	220	0.309	14.53671	1.1625	0.303
12	222	0.252	12.39487	1.0932	0.252
14	224	0.232	10.84931	1.0354	0.232
14	224	0.211	10.04331	1.0004	0.211

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Recovery Date	Recover	v Data	ì
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		recovery D	ata		
	Elapsed	Residual			Residual
	Recovery Time	Drawdown			Drawdown
	(min)	MWBP-12	F(t)	log[F(t)]	MWBP-12
16	226	0.183	9.680078	0.9859	0.183
18	228	0.157	8.763837	0.9427	0.157
20	230	0.142	8.025986	0.9045	0.142
22	232	0.126	7.418717	0.8703	0.126
24	234	0.113	6.909955	0.8395	0.113
26	236	0.104	6.477369	0.8114	0.104
28	238	0.091	6.104925	0.7857	0.091

$$\mathsf{F}(\mathsf{t}) = [(t_{\mathsf{n}} - t_{\mathsf{1}})/(t_{\mathsf{n}} - t_{\mathsf{2}})^{\mathsf{Q}_1} \times (t_{\mathsf{n}} - t_{\mathsf{2}})/(t_{\mathsf{n}} - t_{\mathsf{3}})^{\mathsf{Q}_2} \times (t_{\mathsf{n}} - t_{\mathsf{3}})/(t_{\mathsf{n}} - t_{\mathsf{4}})^{\mathsf{Q}_3} \times (t_{\mathsf{n}} - t_{\mathsf{4}})/(t_{\mathsf{n}} - t_{\mathsf{5}})^{\mathsf{Q}_{\mathsf{4}}}]$$



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Pumping Data

Recovery Data Residual

Elapsed

0.15

0.1583

0.1666

0.1833

0.1916

0.2083

0.2166

0.2333

0.2416

0.2583

0.2666

0.275

0.2833

0.2916

0.3083

0.3

0.25

0.225

0.2

0.175

Recovery Time Drawdown

268.15

268.1583

268.1666

268.1833

268.1916

268.2083

268.2166

268.2333

268.2416

268.2583

268.2666

268.2833

268.2916

268.3083

268.3

268.275

268.25

268.225

268.2

268.175

	Elapsed Time (min)	Flow Rate (gpm)	Flow Rate (cu.ft/min)		
Q_1, t_1	0	6	0.802		
Q_2 , t_2	44	12	1.604		
Q_3 , t_3	174	18	2.406		
Q_4 , t_4	244	19	2.54		
Q_5 , t_5	268	0	0		

Residual

10.475

10.342

10.209

10.075

9.942

9.815

9.682

9.555

9.435

9.308

9.187

9.067

8.952

8.832 8.717

8.603

8.489

8.381

8.273

8.165

Drawdown

		recovery rime	Diawacwii			Diamaouii
		(min)	MWBP-05B	F(t)	log[F(t)]	MWBP-05B
-	0.0083	268.0083	12.923	7.68E+10	10.88528	12.923
	0.0166	268.0166	12.803	1.32E+10	10.12073	12.803
	0.025	268.025	12.727	4.67E+09	9.669117	12.727
	0.0333	268.0333	12.587	2.25E+09	9.352951	12.587
	0.0416	268.0416	12.403	1.28E+09	9.107536	12.403
	0.05	268.05	12.257	8.03E+08	8.904725	12.257
	0.0583	268.0583	12.099	5.44E+08	8.735385	12.099
	0.0666	268.0666	11.934	3.88E+08	8.588633	11.934
	0.075	268.075	11.782	2.87E+08	8.457678	11.782
	0.0833	268.0833	11.636	2.2E+08	8.341969	11.636
	0.0916	268.0916	11.477	1.73E+08	8.237268	11.477
	. 0.1	268.1	11.332	1.38E+08	8.140558	11.332
	0.1083	268.1083	11.186	1.13E+08	8.052676	11.186
	0.1166	268.1166	11.04	93603509	7.971292	11.04
	0.125	268.125	10.894	78456754	7.89463	10.894
	0.1333	268.1333	10.754	66648073	7.823788	10.754
	0.1416	268.1416	10.615	57178126	7.75723	10.615

49400810 7.693734

33412827 7.523913

29707873 7.472872 26551800 7.424094

23814287 7.376838

21481141 7.332057

17665828 7.247134

16115673 7.207248

13524888 7.131134

9851285 6.993493

43092205

37852984

19454942

14748911

12450293

11491191

10622333

9156154

8520410

7951149

7.634399

7.5781

7.28903

7.16876

7.09518

7.060365

7.02622

6.961713

6.93046

6.90043

10.475

10.342

10.209

10.075

9.942

9.815

9.682

9.555

9.435

9.308

9.187

9.067

8.952

8.832

8.717

8.603

8.489

8.381

8.273

8.165

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Recovery	Data
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		Recovery Data			
	Elapsed	Residual			Residual
	Recovery Time				Drawdown
	(min)	MWBP-05B	F(t)	log[F(t)]	MWBP-05B
0.3166		8.057	7433599	6.871199	8.057
0.325		7.949	6956458	6.842388	7.949
0.3333		7.848	6525960	6.814644	7.848
0.35		7.645	5765838	6.760862	7.645
0.3666		7.442	5127370	6.709895	7.442
0.3833		7.245	4580406	6.660904	7.245
0.4		7.061	4111585	6.614009	7.061
0.4166		6.876	3709393	6.569303	6.876
0.4333		6.699	3358115	6.526096	6.699
0.45	268.45	6.521	3051602	6.484528	6.521
0.4666	268.4666	6.349	2784300	6.444716	6.349
0.4833	268.4833	6.184	2547264	6.406074	6.184
0.5	268.5	6.025	2337489	6.36875	6.025
0.5166	268.5166	5.867	2152133	6.332869	5.867
0.5333	268.5333	5.714	1985739	6.297922	5.714
0.55	268.55	5.562	1836781	6.264057	5.562
0.5666	268.5666	5.416	1703743	6.231404	5.416
0.5833	268.5833	5.276	1583104	6.199509	5.276
0.6	268.6	5.136	1474075	6.168519	5.136
0.6166	268.6166	5.003	1375822	6.138562	5.003
; 0.6333	268.6333	4.869	1285972	6.109232	4.869
0.65	268.65	4.742	1204116	6.080668	4.742
0.6666	268.6666	4.621	1129790	6.052998	4.621
0.6833	268.6833	4.501	1061332	6.025851	4.501
0.7	268.7	4.38	998535.2	5.999363	4.38
0.7166	268.7166	4.266	941145.4	5.973657	4.266
0.7333	268.7333	4.158	887958.3	5.948393	4.158
0.75	268.75	4.043	838881.5	5.923701	4.043
0.7666	268.7666	3.942	793777.4	5.899699	3.942
0.7833	268.7833	3.834	751751.3	5.876074	3.834
0.8	268.8	3.738	712772.9	0.00=00.	3.738
0.8166	268.8166	3.637	676773.1	5.830443	3.637
0.8333	268.8333	3.541		5.808259	3.541
0.85	268.85	3.452		5.786519	3.452
0.8666	268.8666	3.357	582546.2	5.76533	3.357
0.8833	268.8833	3.268	555166	5.744423	3.268
0.9	268.9	3.185	529553.2	5.72391	3.185
0.9166	268.9166	3.103	505703.2	5.703896	3.103
0.9333	268.9333	3.02	483199.2	5.684126	3.02
0.95	268.95	2.944	462072.4	5.66471	2.944
0.9666	268.9666	2.867	442331.5	5.645748	2.867
0.9833	268.9833	2.791	423642.8	5.627	2.791
1	269	2.721	406041.1	5.60857	2.721
1.2	269.2	1.958	256574.9	5.409214	1.958
1.4	269.4	1.437	174151.9	5.240928	1.437
1.6	269.6	1.055	124561	5.095382	1.055

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		Recovery Data			
	Elapsed	Residual			Residual
	Recovery Time	Drawdown			Drawdown
	(min)	MWBP-05B	F(t)	log[F(t)]	MWBP-05B
1.8	269.8	0.788	92726.16	4.967202	0.788
2	270	0.591	71239.44	4.85272	0.591
2.2	270.2	0.451	56146.14	4.74932	0.451
2.4	270.4	0.343	45192.71	4.655068	0.343
2.6	270.6	0.273	37025.32	4.568499	0.273
2.8	270.8	0.216	30794.32	4.488471	0.216
3	271	0.178	25946.56	4.41408	0.178
3.2	271.2	0.152	22110.44	4.344597	0.152
3.4	271.4	0.127	19029.5	4.279427	0.127
3.6	271.6	0.108	16522.51	4.218076	0.108
3.8	271.8	0.095	14458.71	4.16013	0.095
4		0.082	12742.02	4.105238	0.082
4.2	272.2	0.076	11300.64	4.053103	0.076
4.4	272.4	0.069	10080.16	4.003467	0.069
4.6	272.6	0.063	9038.749	3.956108	0.063
4.8	272.8	0.057	8143.889	3.910832	0.057
5	273	0.057	7369.999	3.867467	0.057
5.2	273.2	0.057	6696.761	3.825865	0.057
5.4	273.4	0.05	6107.881	3.785891	0.05
5.6	273.6	0.05	5590.183	3.747426	0.05
÷ 5.8	273.8	0.05	5132.925	3.710365	0.05
6	274	0.044	4727.285	3.674612	0.044
6.2	274.2	0.044	4365.968	3.640081	0.044
6.4	274.4	0.044	4042.903	3.606693	0.044
6.6	274.6	0.038	3753.009	3.57438	0.038
6.8	274.8	0.038	3492.006	3.543075	0.038
7	275	0.031	3256.273	3.512721	0.031
7.2	275.2	0.038	3042.729	3.483263	0.038
7.4	275.4	0.038	2848.741	3.454653	0.038
7.6	275.6	0.038	2672.05	3.426845	0.038
7.8	275.8	0.038	2510.708	3.399796	0.038
8	276	0.038		3.373469	0.038
8.2	276.2	0.031	2227.553	3.347828	0.031
8.4	276.4	0.031	2102.999	3.322839	0.031
8.6	276.6	0.031		3.298472	0.031
8.8	276.8	0.031		3.274697	0.031
9		0.031	1784.385	3.251489	0.031
9.2		0.031	1693.64	3.228821	0.031
9.4		0.031	1609.426	3.206671	0.031
9.6	277.6	0.031	1531.146	3.185017	0.031

$$\mathsf{F}(\mathsf{t}) = [(t_n - t_1)/(t_n - t_2)^{Q_1} \times (t_n - t_2)/(t_n - t_3)^{Q_2} \times (t_n - t_3)/(t_n - t_4)^{Q_3} \times (t_n - t_4)/(t_n - t_5)^{Q_4}]$$

APPENDIX B

CONSTANT RATE TEST DATA BACKGROUND MONITORING DATA DATA ANALYSIS SUMMARY

Table B-1
20-Hour Constant Rate Discharge Test Data for MWBP-12
(Flow Rate = 7.5 gpm)

(Page 1 of 6)

								Ва	ackground Re	adings
ı	Elapsed		Transduc	er Readi	ngs of Draw	down (ft)		Elapsed	Relative	Cumulative
	Time of				MWBP-12	P-1	P-2	Time	Fluctuation in	
Т	est (min)	MWBP-12	P-1	P-2	(corrected)	(corrected)	(corrected)	(minutes)	MWBP-09A	MWBP-09A
	0	0.231	0	0	0.231	0	0			
	0.0083	0.329	0	0	0.329	0	0			
	0.0166	0.427	0	0	0.427	0	0			
	0.025	0.503	0	0	0.503	0	0			
	0.0333	0.598	0	0	0.598	0	0			
	0.0416	0.681	0	0	0.681	0	0			
	0.05	0.747	0	0	0.747	0	0			
	0.0583	0.814	0	0	0.814	0	0			
	0.0666	0.883	0	0	0.883	0	0			
	0.075	0.947	0	0	0.947	0	0			
	0.0833	1	0	0.003	1	0	0.003			
	0.0916	1.061	0	0.003	1.061	0	0.003			
	0.1	1.108	0	0	1.108	0	0			
	0.1083	1.162	0	0	1.162	0	0			
	0.1166	1.216	0.003	0	1.216	0.003	0 003			
	0.125	1.26	0.003	0.003	1.26	0.003	0.003			
	0.1333	1.311	0.003	0.003	1.311	0.003	0.003			
	0.1416	1.352	0.006	0	1.352	0.006	0			
	0.15	1.403	0.006	0	1.403	0.006 0.006	0 0			
	0.1583	1.444	0.006	0	1.444 1.491	0.009	0			
	0.1666	1.491	0.009	0	1.523	0.009	0			
	0.175	1.523 • 1.561	0.009	0.003	1.523	0.009	0.003			
	0.1833 0.1916	1.599	0.009	0.003	1.599	0.003	0.003			
	0.1910	1.631	0.012	0.003	1.631	0.012	0.003			
	0.2083	1.672	0.012	0.003	1.672	0.012	0.003			
	0.2063	1.688	0.012	0.000	1.688	0.015	0.000			
	0.2100	1.716	0.015	0.003	1.716	0.015	0.003			
	0.223	1.757	0.015	0.000	1.757	0.015	0.000			
	0.2416	1.77	0.015	Ö	1.77	0.015	0			
	0.25	1.795	0.018	0	1.795	0.018	0			
	0.2583	1.821	0.018	0.003	1.821	0.018	0.003			
	0.2666	1.849	0.022	0.003	1.849	0.022	0.003			
	0.275	1.862	0.022	0	1.862	0.022	0			
	0.2833	1.893	0.022	0.003	1.893	0.022	0.003			
	0.2916	1.912	0.025	0.003	1.912	0.025	0.003			
	0.3	1.931	0.025	0	1.931	0.025	0			
	0.3083	1.954	0.028	0	1.954	0.028	0			
	0.3166	1.976	0.028	0	1.976	0.028	0			
	0.325	1.985	0.028	0	1.985	0.028	0			
	0.3333	2.011	0.031	0	2.011	0.031	0			
	0.35	2.042	0.031	0	2.042	0.031	0			
	0.3666	2.077	0.034	0.003	2.077	0.034	0.003			
	0.3833	2.112	0.037	0	2.112	0.037	0 000			
	0.4	2.137	0.037	0.003	2.137	0.037	0.003			
	0.4166	2.162	0.041	0	2.162	0.041	0			
	0.4333	2.194	0.041	0	2.194	0.041	0			
	0.45	2.216	0.044	0	2.216	0.044 0.047	0			
	0.4666	2.238	0.047	0	2.238 2.264	0.047	0			
	0.4833	2.264	0.047 0.05	0	2.283	0.047	0			
	0.5	2.283	0.05	U	2.203	0.00	U			

BP12Q24.XLS: Sheet1(11/15/96)sal

Table B-1
20-Hour Constant Rate Discharge Test Data for MWBP-12
(Flow Rate = 7.5 gpm)

(Page 2 of 6)

				(, -	.90 = 0. 0,				
							В	ackground Re	adings
Elapsed		Transdu	cer Readi	ngs of Draw	down (ft)		Elapsed	Relative	Cumulative
Time of				MWBP-12	P-1	P-2	Time	Fluctuation in	Fluctuation in
Test (min)	MWBP-12	P-1	P-2	(corrected)	(corrected)	(corrected)	(minutes)	MWBP-09A	MWBP-09A
0.5166		0.053	0	2.299	0.053	0			
0.5333	2.314	0.056	0	2.314	0.056	0			
0.55	2.321	0.056	0	2.321	0.056	0			
0.5666	2.327	0.059	0	2.327	0.059	0			
0.5833	2.33	0.059	0	2.33	0.059	0			
0.6	2.333	0.063	-0.003	2.333	0.063	-0.003			
0.6166	2.333	0.063	0	2.333	0.063	0			
0.6333	2.333	0.066	0	2.333	0.066	0			
0.65		0.066	0	2.333	0.066	0			
0.6666		0.069	0	2.333	0.069	0			
0.6833		0.072	-0.003	2.333	0.072	-0.003			
0.7	2.333	0.072	-0.003	2.333	0.072	-0.003			
0.7166		0.075	0	2.337	0.075	0			
0.7333		0.075	0	2.333	0.075	0			
0.75		0.078	0	2.337	0.078	0			
0.7666		0.078	0	2.333	0.078	0			
0.7833	2.333	0.082	-0.003	2.333	0.082	-0.003			
8.0	2.337	0.082	-0.003	2.337	0.082	-0.003			
0.8166		0.085	0	2.333	0.085	0			
0.8333	2.333	0.085	-0.003	2.333	0.085	-0.003			
0.85	2.333	0.088	0	2.333	0.088	0			
0.8666		0.091	-0.003	2.337	0.091	-0.003			
0.8833		0.091	-0.003	2.333	0.091	-0.003			
0.9	2.333	0.091	-0.003	2.333	0.091	-0.003			
0.9166	2.333	0.094	-0.003	2.333	0.094	-0.003			
0.9333	2.333	0.094	-0.003	2.333 2.435	0.094 0.097	-0.003 -0.003			
0.95	2.435	0.097	-0.003 -0.003	2.435	0.097	-0.003			
0.9666 0.9833	2.593 2.742	0.1 0.1	-0.003	2.593	0.1	-0.003			
0.9633	2.742	0.104	-0.003	2.742	0.104	-0.003	1	0.000	0.163
1.2	3.248	0.132	-0.003	3.248	0.132	-0.003		0.000	0.100
1.4		0.152	0.000	3.245	0.157	0.000		0.000	
1.6	3.245	0.176	0	3.245	0.176	Ō		0.000	
1.8	3.289	0.195	0	3.289	0.195	ō		0.000	
2		0.211	0	3.419	0.211	0		0.000	
2.2		0.223	0	3.992	0.223	0		0.000	
2.4		0.239	0	4.096	0.239	0		0.000	
2.6		0.252	0.003	4.182	0.252	0.003		0.000	
2.8		0.265	0.003	4.261	0.265	0.003		0.000	
3		0.277	0.003	4.337	0.277	0.003		0.000	
3.2		0.29	0.006	4.4	0.29	0.006		0.000	
3.4		0.296	0.003	4.463	0.296	0.003		0.000	
3.6		0.306	0.006	4.526	0.306	0.006		0.000	
3.8	4.58	0.315	0.006	4.58	0.315	0.006		0.000	
4	4.631	0.324	0.006	4.631	0.324	0.006		0.000	
4.2	4.678	0.331	0.003	4.678	0.331	0.003		0.000	
4.4	4.716	0.334	0.003	4.716	0.334	0.003		0.000	
4.6		0.343	0.006	4.754	0.343	0.006		0.000	
4.8		0.353	0.006	4.792	0.353	0.006		0.000	
5		0.359	0.006	4.824	0.359	0.006		0.000	
5.2	4.855	0.362	0.006	4.855	0.362	0.006		0.000	

Table B-1
20-Hour Constant Rate Discharge Test Data for MWBP-12
(Flow Rate = 7.5 gpm)

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							В	ackground Re	adings
Elapsed		Transdu	cer Readi	ngs of Draw	down (ft)		Elapsed	Relative	Cumulative
Time of				MWBP-12	P-1	P-2	Time	Fluctuation in	
Test (min)	MWBP-12	P-1	P-2		(corrected)		(minutes)	MWBP-09A	MWBP-09A
5.4	4.881	0.369	0.006	4.881	0.369	0.006		0.000	
5.6	4.906	0.375	0.006	4.906	0.375	0.006		0.000	
5.8	4.938	0.381	0.006	4.938	0.381	0.006		0.000	
6	4.963	0.384	0.006	4.963	0.384	0.006		0.000	
6.2	4.985	0.391	0.006	4.985	0.391	0.006		0.000	
6.4	5.007	0.394	0.009	5.007	0.394	0.009		0.000	
6.6	5.033	0.4	0.009	5.033	0.4	0.009		0.000	
6.8	5.052	0.403	0.006	5.052	0.403	0.006		0.000	
7	5.071	0.406	0.006	5.071	0.406	0.006		0.000	
7.2	5.093	0.413	0.006	5.093	0.413	0.006		0.000	
7.4	5.112	0.416	0.006	5.112	0.416	0.006		0.000 0.000	
7.6	5.102	0.422	0.009	5.102	0.422	0.009 0.006		0.000	
7.8	5.124	0.425	0.006	5.124	0.425	0.006		0.000	
8	5.143	0.429	0.006	5.143 5.162	0.429 0.432	0.006		0.000	
8.2	5.162	0.432 0.435	0.006		0.432	0.006		0.000	
8.4	5.175	0.435	0.009	5.175	0.438	0.000		0.000	
8.6 8.8	5.188 5.2	0.430	0.009	5.2	0.441	0.006		0.000	
9.0	5.219	0.447	0.000	5.219	0.447	0.009		0.000	
9.2	5.219	0.444	0.009	5.229	0.444	0.006		0.000	
9.4	5.241	0.447	0.006	5.241	0.447	0.006		0.000	
9.6	5.245	0.454	0.006	5.245	0.454	0.006		0.000	
9.8	5.254	0.457	0.009	5.254	0.457	0.009		0.000	
10	5.295	0.46	0.009	5.295	0.46	0.009		0.000	
12		0.495	0.009	5.697	0.495	0.009		0.000	
14		0.514	0.012	5.725	0.514	0.012		0.000	
16		0.533	0.012	5.788	0.533	0.012		0.000	
18		0.548	0.012	5.849	0.548	0.012		0.000	
20		0.561	0.012	5.883	0.561	0.012	20	0.000	0.163
22	5.915	0.571	0.009	5.9156	0.5716	0.0096		0.0006	
24	5.95	0.58	0.012	5.9512	0.5812	0.0132		0.0012	
26	5.975	0.586	0.012	5.9768	0.5878	0.0138		0.0018	
28	6.019	0.596	0.012	6.0214	0.5984	0.0144		0.0024	
30		0.602	0.012	6.0410	0.6050	0.0150		0.0030	
32	6.013	0.602	0.006	6.0166	0.6056	0.0096		0.0036	
34		0.602	0.009	6.0452	0.6062	0.0132		0.0042	
36		0.608	0.012	6.0498	0.6128	0.0168		0.0048	
38		0.615	0.018	6.0814	0.6204	0.0234	40	0.0054	0.460
40		0.624	0.018	6.0850	0.6300	0.0240	40	0.006 0.007	0.169
42		0.627	0.022	6.0830	0.6340	0.0290 0.0260		0.007	
44		0.621 0.63	0.018 0.022	6.0940 6.0980	0.6290 0.6390	0.0200		0.008	
46 48		0.608	0.022	6.0890	0.6390	0.0310		0.010	
50		0.624	0.000	6.0970	0.6350	0.0260		0.011	
52		0.63	0.015	6.1010	0.6420	0.0270		0.012	
54		0.637	0.018	6.1050	0.6500	0.0310		0.013	
56		0.634	0.015	6.1090	0.6480	0.0290		0.014	
58		0.637	0.018	6.1130	0.6520	0.0330		0.015	
60		0.637	0.015	6.0950	0.6530			0.016	0.179
62		0.637	0.015	6.1080	0.6530			0.016	
64		0.634	0.012	6.1080	0.6500			0.016	
- •							•		

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Table B-1
20-Hour Constant Rate Discharge Test Data for MWBP-12
(Flow Rate = 7.5 gpm)

(Page 4 of 6)

							Ва	ackground Rea	adings
Elapsed		Transduc	er Readi	ngs of Draw	down (ft)		Elapsed	Relative	Cumulative
Time of				MWBP-12	P-1	P-2	Time	Fluctuation in	Fluctuation in
Test (min)	MWBP-12	P-1	P-2	(corrected)	(corrected)	(corrected)	(minutes)	MWBP-09A	MWBP-09A
66	6.092	0.634	0.012	6.1080	0.6500	0.0280		0.016	
68	6.092	0.634	0.015	6.1080	0.6500	0.0310		0.016	
70	6.092	0.64	0.018	6.1080	0.6560	0.0340		0.016	
72	6.095	0.646	0.031	6.1110	0.6620	0.0470		0.016	
74	6.089	0.649	0.031	6.1050	0.6650	0.0470		0.016	
76	6.098	0.649	0.025	6.1140	0.6650	0.0410		0.016	
78	6.083	0.653	0.025	6.0990	0.6690	0.0410		0.016	
80	6.086	0.646	0.018	6.1020	0.6620	0.0340	80	0.016	0.179
82	6.073	0.646	0.015	6.0903	0.6633	0.0323		0.0173	
84	6.073	0.649	0.025	6.0916	0.6676	0.0436		0.0186	
86	6.064	0.643	0.009	6.0839	0.6629	0.0289		0.0199	
88	6.06	0.646	0.025	6.0812	0.6672	0.0462		0.0212	
90	6.073	0.649	0.028	6.0955	0.6715	0.0505		0.0225	
92	6.07	0.649	0.025	6.0938	0.6728	0.0488		0.0238	
94	6.054	0.649	0.022	6.0791	0.6741	0.0471		0.0251	
96	6.054	0.649	0.018	6.0804	0.6754	0.0444		0.0264	
98	6.038	0.653	0.022	6.0657	0.6807	0.0497		0.0277	
100	6.029	0.649	0.022	6.0580	0.6780	0.0510	100	0.029	0.192
110	6.503	0.662	0.018	6.5320	0.6910	0.0470		0.029	
120	6.535	0.675	0.022	6.5640	0.7040	0.0510	120	0.029	0.192
130	6.56	0.684	0.037	6.5890	0.7130	0.0660		0.029	
140	6.522	0.684	0.037	6.5510	0.7130	0.0660	140	0.029	0.192
150	6.506	0.687	0.037	6.5350	0.7160	0.0660		0.029	
160	6.452	0.697	0.047	6.4810	0.7260	0.0760	160	0.029	0.192
170	6.449	0.69	0.044	6.4810	0.7220	0.0760		0.032	
180	6.44	0.697	0.053	6.4750	0.7320	0.0880	180	0.035	0.198
190	6.506	0.697	0.05	6.5455	0.7365	0.0895		0.0395	
200	6.471	0.681	0.025	6.5150	0.7250	0.0690	200	0.044	0.207
210	6.449	0.687	0.034	6.4950	0.7330	0.0800		0.046	
220	6.418	0.681	0.028	6.4660	0.7290	0.0760	220	0.048	0.211
230	6.418	0.684	0.034	6.4690	0.7350	0.0850		0.051	0.047
240	6.377	0.684	0.031	6.4310	0.7380	0.0850	240	0.054	0.217
250	6.367	0.69	0.05	6.4210	0.7440	0.1040		0.054	0.047
260	6.579	0.697	0.05	6.6330	0.7510	0.1040	260	0.054	0.217
270	6.544	0.7	0.044	6.6030	0.7590	0.1030	200	0.059	0.227
280	6.541	0.697	0.044	6.6050	0.7610	0.1080	280	0.064	0.227
290	6.538	0.697	0.053	6.5985	0.7575	0.1135	000	0.0605	0.000
300	6.497	0.7	0.047	6.5540	0.7570	0.1040	300	0.057	0.220
310	6.81	0.703	0.047	6.8720	0.7650	0.1090	220	0.062	0.220
320	6.863	0.709	0.05	6.9300	0.7760	0.1170	320	0.067	0.230
330	6.867	0.712	0.05	6.9355	0.7805	0.1185	240	0.0685	0.222
340	6.857	0.709	0.05	6.9270	0.7790	0.1200	340	0.070	0.233
350	6.854	0.716	0.056	6.9210	0.7830	0.1230 0.1270	260	0.067	0.227
360	6.845	0.719	0.063	6.9090	0.7830		360	0.064 0.0575	U.ZZ1
370	6.901	0.722	0.06	6.9585	0.7795 0.7860	0.1175 0.1230	380	0.0575	0.214
380	6.892	0.735	0.072 0.082	6.9430	0.7860	0.1230	300	0.031	U.Z 14
390	6.92 1.868	0.738 0.615	0.085	6.9645 1.9060	0.7625	0.1283	400	0.0445	0.201
400 410	5.981	0.646	0.082	6.0205	0.6855	0.1230	400	0.0395	0.201
420	6.237	0.697	0.085	6.2780	0.7380	0.1213	420	0.0393	0.204
420	6.683	0.697	0.088	6.7180	0.7540	0.1230		0.035	0.204
430	0.003	0.718	0.000	0.7 100	0.7540	0.1230		0.000	

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Table B-1
20-Hour Constant Rate Discharge Test Data for MWBP-12
(Flow Rate = 7.5 gpm)

(Page 5 of 6)

							В	ackground Rea	adings
Elapsed		Transduc	er Readi	ngs of Draw	down (ft)		Elapsed	Relative	Cumulative
Time of				MWBP-12	P-1	P-2	Time	Fluctuation in	Fluctuation in
Test (min)	MWBP-12	P-1	P-2	(corrected)	(corrected)	(corrected)	(minutes)	MWBP-09A	MWBP-09A
440	6.784	0.747	0.101	6.8130	0.7760	0.1300	440	0.029	0.192
450	6.845	0.757	0.104	6.8785	0.7905	0.1375		0.0335	
460	6.747	0.741	0.091	6.7850	0.7790	0.1290	460	0.038	0.201
470	6.87	0.741	0.082	6.9130	0.7840	0.1250		0.043	
480	6.924	0.741	0.082	6.9720	0.7890	0.1300	480	0.048	0.211
490	6.911	0.744	0.082	6.9590	0.7920	0.1300		0.048	
500	6.946	0.75	0.088	6.9940	0.7980	0.1360	500	0.048	0.211
510	6.977	0.763	0.104	7.0170	0.8030	0.1440		0.04	
520	7.009	0.763	0.104	7.0410	0.7950	0.1360	520	0.032	0.195
530	7.009	0.769	0.104	7.0410	0.8010	0.1360		0.032	
540	7.022	0.769	0.104	7.0540	0.8010	0.1360	540	0.032	0.195
550	7.044	0.779	0.117	7.0645	0.7995	0.1375		0.0205	
560	7.091	0.794	0.136	7.1000	0.8030	0.1450	560	0.009	0.172
570	7.11	0.798	0.139	7.1130	0.8010	0.1420		0.003	
580	7.142	0.81	0.151	7.1390	0.8070	0.1480	580	-0.003	0.160
590	7.138	0.823	0.164	7.1270	0.8120	0.1530		-0.011	
600	7.135	0.823	0.164	7.1160	0.8040	0.1450	600	-0.019	0.144
610	7.151	0.813	0.154	7.1400	0.8020	0.1430		-0.011	
620	7.164	0.807	0.148	7.1610	0.8040	0.1450	620	-0.003	0.160
630	7.145	0.81	0.151	7.1420	0.8070	0.1480		-0.003	
640	7.12	0.807	0.145	7.1170	0.8040	0.1420	640	-0.003	0.160
650	7.113	0.807	0.145	7.1115	0.8055	0.1435		-0.0015	
660	7.107	0.804	0.142	7.1070	0.8040	0.1420	660	0.000	0.163
670	7.088	0.798	0.136	7.0910	0.8010	0.1390		0.003	
680	7.116	0.801	0.142	7.1220	0.8070	0.1480	680	0.006	0.169
690	7.151	0.807	0.145	7.1555	0.8115	0.1495		0.0045	
700	7.161	0.807	0.145	7.1640	0.8100	0.1480	700	0.003	0.166
710	7.148	0.81	0.151	7.1480	0.8100	0.1510		0	
720	7.192	0.813	0.154	7.1890	0.8100	0.1510	720	-0.003	0.160
730	7.173	0.817	0.158	7.1700	0.8140	0.1550		-0.003	
740	7.183	0.817	0.158	7.1800	0.8140	0.1550	740	-0.003	0.160
750	7.189	0.817	0.154	7.1860	0.8140	0.1510		-0.003	
760	7.167	0.813	0.154	7.1640	0.8100	0.1510	760	-0.003	0.160
770	7.138	0.813	0.154	7.1365	0.8115	0.1525		-0.0015	0.400
780	7.157	0.813	0.154	7.1570	0.8130	0.1540	780	0.000	0.163
790	7.173	0.813	0.154	7.1730	0.8130	0.1540	000	0	0.400
800	7.202	0.817	0.154	7.2020	0.8170	0.1540	800	0.000	0.163
810	7.202	0.817	0.158	7.2035	0.8185	0.1595	000	0.0015	0.466
820	7.17	0.813	0.154	7.1730	0.8160	0.1570	820	0.003	0.166
830	7.173	0.817 0.813	0.154	7.1760	0.8200	0.1570 0.1610	840	0.003 0.003	0.166
840	7.195	0.813	0.158 0.154	7.1980	0.8160 0.8190	0.1610	040	0.003	0.166
850	7.167	0.81	0.154	7.1730 7.1730	0.8190	0.1600	860	0.009	0.172
860	7.164 7.164	0.81	0.131	7.1730	0.8190	0.1570	800	0.009	0.172
870 880	7.1 04 7.164	0.813	0.146	7.1730	0.8220	0.1630	880	0.009	0.172
890	7.164	0.81	0.154	7.1730	0.8225	0.1635	550	0.009	0.172
900	7.143	0.807	0.131	7.1640	0.8230	0.1640	900	0.0123	0.179
910	7.146	0.81	0.148	7.7475	0.8235	0.1655	300	0.016	0.173
920	7.878	0.813	0.148	7.8970	0.8320	0.1670	920	0.017	0.182
930	7.878	0.813	0.148	7.8985	0.8335	0.1685	020	0.0205	0.102
940	7.862	0.81	0.142	7.8840	0.8320	0.1640	940	0.022	0.185
340	1.002	0.01	V. 172	7.00-10	0.0020	0.1040	J-10	J.UZZ	0.100

Table B-1
20-Hour Constant Rate Discharge Test Data for MWBP-12
(Flow Rate = 7.5 gpm)

(Page 6 of 6)

							В	ackground Rea	adings
Elapsed		Transdu	cer Readi	ngs of Draw	down (ft)		Elapsed	Relative	Cumulative
Time of				MWBP-12	P-1	P-2	Time	Fluctuation in	Fluctuation in
Test (min)	MWBP-12	P-1	P-2	(corrected)	(corrected)	(corrected)	(minutes)	MWBP-09A	MWBP-09A
950	7.878	0.807	0.136	7.9065	0.8355	0.1645		0.0285	
960	7.843	0.804	0.132	7.8780	0.8390	0.1670	960	0.035	0.198
970	7.85	0.801	0.132	7.8880	0.8390	0.1700		0.038	
980	7.869	0.801	0.132	7.9100	0.8420	0.1730	980	0.041	0.204
990	7.869	0.801	0.132	7.9115	0.8435	0.1745		0.0425	
1000	7.878	0.801	0.132	7.9220	0.8450	0.1760	1000	0.044	0.207
1010	7.834	0.801	0.132	7.8800	0.8470	0.1780		0.046	
1020	7.894	0.801	0.129	7.9420	0.8490	0.1770	1020	0.048	0.211
1030	7.881	0.801	0.129	7.9305	0.8505	0.1785		0.0495	
1040	7.894	0.801	0.129	7.9450	0.8520	0.1800	1040	0.051	0.214
1050	7.9	0.801	0.132	7.9495	0.8505	0.1815		0.0495	
1060	7.938	0.801	0.132	7.9860	0.8490	0.1800	1060	0.048	0.211
1070	7.951	0.801	0.132	7.9990	0.8490	0.1800		0.048	
1080	7.995	0.801	0.136	8.0430	0.8490	0.1840	1080	0.048	0.211
1090	8.02	0.807	0.139	8.0660	0.8530	0.1850		0.046	
1100	8.087	0.807	0.142	8.1310	0.8510	0.1860	1100	0.044	0.207
1110	8.121	0.813	0.148	8.1620	0.8540	0.1890		0.041	
1120	8.159	0.813	0.148	8.1970	0.8510	0.1860	1120	0.038	0.201
1130	8.147	0.813	0.148	8.1865	0.8525	0.1875		0.0395	
1140	8.557	0.813	0.145	8.5980	0.8540	0.1860	1140	0.041	0.204
1150	8.557	0.813	0.148	8.5995	0.8555	0.1905		0.0425	
1160	8.561	0.813	0.145	8.6050	0.8570	0.1890	1160	0.044	0.207
1170	÷ 8.561	0.813	0.148	8.6035	0.8555	0.1905		0.0425	
1180	8.567	0.813	0.148	8.6080	0.8540	0.1890	1180	0.041	0.204
1190	8.567	0.813	0.145	8.6115	0.8575	0.1895		0.0445	
1200	8.567	0.81	0.145	8.6150	0.8580	0.1930	1200	0.048	0.211

Table B-2
Recovery Data for 20-Hour Constant Rate Discharge Test in MWBP-12

(Page 1 of 4)

Elapsed	Total Test	Drawdown M	leasurements	(feet)
Time	Time	MWBP-12	P-1	P-2
(minute)	(minute)	IPING DATA (1 -2
	0.1	1.108	Q-7.5 gpiii)	0
0.1	1	2.91	0.104	-0.003
1		5.295	0.104	0.009
10	10	6.029	0.40	0.009
100	100 1000	7.878	0.801	0.022
1000	1100	8.087	0.807	0.132
1100	1120	8.159	0.807	0.148
1120	1140	8.557	0.813	0.145
1140			0.813	0.145
1160	1160	8.561	0.813	0.143
1180	1180	8.567		0.145
1200	1200	8.567 OVERY DATA	0.81	0.145
0.0000				0.145
0.0083	1200.008	8.564	0.813 0.813	0.145
0.0166	1200.017	8.564	0.813	0.145
0.025	1200.025	8.564		0.145
0.0333	1200.033	8.564	0.813	
0.0416	1200.042	8.561	0.813	0.145
0.05	1200.050	8.482	0.813	0.145
0.0583	1200.058	8.365	0.813	0.145
0.0666	1200.067	8.238	0.813	0.145
0.075	1200.075	8.118	0.813	0.145
0.0833	1200.083	7.995	0.813	0.145 0.145
0.0916	1200.092	7.875	0.813	0.145
0.1	1200.100	7.748	0.813	
0.1083	1200.108	7.635	0.813 0.813	0.148 0.145
0.1166	1200.117	7.527	0.813	0.145
0.125	1200.125	7.413		0.145
0.1333	1200.133	7.303	0.813	0.145
0.1416	1200.142	7.195	0.813	0.145
0.15	1200.150	7.085	0.813	
0.1583	1200.158	6.98	0.813	0.145 0.145
0.1666	1200.167	6.876	0.813	0.145
0.175	1200.175	6.769	0.813	0.145
0.1833	1200.183	6.664	0.813	0.145
0.1916	1200.192	6.56	0.813	0.145
0.2	1200.200	6.462	0.813 0.813	0.145
0.2083	1200.208	6.361		0.145
0.2166	1200.217	6.263	0.813	0.145
0.225	1200.225	6.165	0.813	
0.2333	1200.233	6.07 5.975	0.813 0.813	0.145 0.145
0.2416	1200.242	5.975 5.88	0.813	0.145
0.25	1200.250 1200.258	5.00 5.788	0.81	0.145
0.2583		5.766	0.813	0.145
0.2666	1200.267 1200.275		0.813	0.148
0.275	1200.275	5.611 5.523	0.813	0.148
0.2833	1200.283	0.023	0.01	U. 14U

Table B-2
Recovery Data for 20-Hour Constant Rate Discharge Test in MWBP-12

(Page 2 of 4)

	Elapsed	Total Test	Drawdown Measurem		ents (feet)	
	Time	Time	Diawaowii w	Casaromonia	(1001)	
	(minute)	(minute)	MWBP-12	P-1	P-2	
•	0.2916	1200.292	5.441	0.813	0.148	
	0.3	1200.300	5.358	0.81	0.145	
	0.3083	1200.308	5.282	0.81	0.145	
	0.3166	1200.317	5.21	0.81	0.145	
	0.325	1200.325	5.14	0.81	0.145	
	0.3333	1200.333	5.074	0.81	0.148	
	0.35	1200.350	4.954	0.81	0.145	
	0.3666	1200.367	4.843	0.807	0.148	
	0.3833	1200.383	4.742	0.807	0.145	
	0.4	1200.400	4.65	0.804	0.145	
	0.4166	1200.417	4.561	0.804	0.148	
	0.4333	1200.433	4.482	0.804	0.145	
	0.45	1200.450	4.409	0.801	0.145	
	0.4666	1200.467	4.34	0.801	0.145	
	0.4833	1200.483	4.27	0.798	0.145	
	0.5	1200.500	4.207	0.798	0.145	
	0.5166	1200.517	4.15	0.798	0.145	
	0.5333	1200.533	4.093	0.798	0.145	
	0.55	1200.550	4.049	0.794	0.145	
	0.5666	1200.567	4.023	0.794	0.145	
	0.5833	1200.583	3.97	0.794	0.145	
	0.6	1200.600	3.919	0.791	0.145	
	0.6166	1200.617	3.865	0.791	0.145	
	0.6333	1200.633	3.811	0.788	0.145	
	0.65	1200.650	3.758	0.788	0.145	
	0.6666	1200.667	3.701	0.785	0.145	
	0.6833	1200.683	3.647	0.785	0.145	
	0.7	1200.700	3.59	0.782	0.145	
	0.7166	1200.717	3.539	0.782	0.145	
	0.7333	1200.733	3.489	0.782	0.145	
	0.75	1200.750	3.448	0.779	0.145	
	0.7666	1200.767	3.413	0.779	0.148	
	0.7833	1200.783	3.378	0.779	0.145	
	0.8	1200.800	3.343	0.776	0.145	
	0.8166	1200.817	3.311	0.776	0.148	
	0.8333	1200.833	3.277	0.772	0.145	
	0.85	1200.850	3.248	0.772	0.145	
	0.8666	1200.867	3.217	0.772	0.145	
	0.8833	1200.883	3.185	0.769	0.145	
	0.9	1200.900	3.156	0.769	0.145	
	0.9166	1200.917	3.125	0.766	0.145	
	0.9333	1200.933	3.096	0.766	0.145	
	0.95	1200.950	3.065	0.763	0.145	
	0.9666	1200.967	3.039	0.763	0.145	
	0.9833	1200.983	3.011	0.763	0.145	
	1	1201.0	2.982	0.76	0.145	
	1.2	1201.2	2.688	0.747	0.145	

Table B-2
Recovery Data for 20-Hour Constant Rate Discharge Test in MWBP-12

(Page 3 of 4)

Elapsed	Total Test	Drawdown M	s (feet)	
Time	Time			, ,
(minute)	(minute)	MWBP-12	P-1	P-2
1.4	1201.4	2.451	0.731	0.145
1.6	1201.6	2.245	0.716	0.145
1.8	1201.8	2.074	0.703	0.145
2	1202.0	1.925	0.687	0.145
2.2	1202.2	1.783	0.675	0.145
2.4	1202.4	1.656	0.662	0.145
2.6	1202.6	1.542	0.649	0.145
2.8	1202.8	1.444	0.637	0.145
3	1203.0	1.371	0.621	0.145
3.2	1203.2	1.32	0.612	0.148
3.4	1203.4	1.251	0.599	0.145
3.6	1203.6	1.19	0.589	0.145
3.8	1203.8	1.137	0.577	0.145
4	1204.0	1.089	0.567	0.145
4.2	1204.2	1.045	0.555	0.145
4.4	1204.4	1	0.545	0.145
4.6	1204.6	0.962	0.539	0.145
4.8	1204.8	0.924	0.526	0.142
5	1205.0	0.893	0.52	0.145
5.2	1205.2	0.867	0.511	0.142
5.4	1205.4	0.842	0.501	0.142
5.6	1205.6	0.817	0.492	0.142
5.8	1205.8	0.791	0.488	0.145
6	1206.0	0.772	0.479	0.142
6.2	1206.2	0.753	0.473	0.142
6.4	1206.4	0.738	0.466	0.142
6.6	1206.6	0.722	0.46	0.142
6.8	1206.8	0.706	0.454	0.142
7	1207.0	0.69	0.447	0.142
7.2	1207.2	0.677	0.441	0.142
7.4	1207.4	0.662	0.435	0.142
7.6	1207.6	0.652	0.429	0.142
7.8	1207.8	0.639	0.425	0.142
8	1208.0	0.627	0.429	0.142
8.2	1208.2	0.614	0.419	0.142
8.4	1208.4	0.605	0.413	0.142
8.6	1208.6	0.595	0.406	0.142
8.8	1208.8	0.586	0.4	0.142
9	1209.0	0.576	0.397	0.142
9.2	1209.2	0.567	0.391	0.142
9.4	1209.4	0.557	0.388	0.142
9.6	1209.6	0.551	0.381	0.142
9.8	1209.8	0.541	0.378	0.142
10	1210.0	0.535	0.372	0.142
12	1212.0	0.471	0.34	0.139
14	1214.0	0.424	0.309	0.136
16	1216.0	0.392	0.287	0.136

Table B-2
Recovery Data for 20-Hour Constant Rate Discharge Test in MWBP-12

(Page 4 of 4)

Elapsed Time	Total Test Time	Drawdown Me	easurements	s (feet)
(minute)	(minute)	MWBP-12	P-1	P-2
18	1218.0	0.364	0.268	0.136
20	1220.0	0.338	0.252	0.132
22	1222.0	0.319	0.242	0.129
24	1224.0	0.304	0.23	0.129
26	1226.0	0.291	0.223	0.129
28	1228.0	0.278	0.214	0.126
30	1230.0	0.269	0.205	0.126
32	1232.0	0.259	0.198	0.123
34	1234.0	0.25	0.189	0.123
36	1236.0	0.243	0.186	0.12
38	1238.0	0.234	0.179	0.12
40	1240.0	0.231	0.176	0.12
42	1242.0	0.224	0.173	0.117
44	1244.0	0.221	0.167	0.117
46	1246.0	0.215	0.167	0.117
48	1248.0	0.212	0.164	0.117
50	1250.0	0.209	0.16	0.117
52	1252.0	0.209	0.157	0.113
54	1254.0	0.202	0.154	0.113
56	1256.0	0.199	0.151	0.113
58	1258.0	0.199	0.151	0.113
60	1260.0	0.193	0.148	0.113
62	1262.0	0.193	0.148	0.11
64	1264.0	0.19	0.145	0.11
66	1266.0	0.186	0.145	0.11
68	1268.0	0.186	0.138	0.11
70	1270.0	0.183	0.138	0.11
72	1272.0	0.18	0.135	0.107
74	1274.0	0.177	0.135	0.107
76	1276.0	0.174	0.132	0.104
78	1278.0	0.174	0.129	0.104
80	1280.0	0.171	0.129	0.104
82	1282.0	0.171	0.126	0.104
84	1284.0	0.167	0.126	0.104
86	1286.0	0.164	0.126	0.104
88	1288.0	0.164	0.123	0.101
90	1290.0	0.164	0.123	0.101
92	1292.0	0.164	0.123	0.101
94	1294.0	0.161	0.123	0.101
96	1296.0	0.161	0.119	0.101
98	1298.0	0.161	0.119	0.101
100	1300.0	0.158	0.116	0.101
110	1310.0	0.152	0.113	0.094
120	1320.0	0.145	0.11	0.091
130	1330.0	0.142	0.107	0.091

Table B-3 36-Hour Constant Rate Discharge Data for MWBP-05B (Flow Rate = 16 gpm)

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						, ,	,			_	
-			-		D						ckground Readings Relative Relative
Elapsed			1	ransducer	Readings of I	Drawdown (ft) MWBP-05B		P-4(A)	P-5(B)	Elapsed Time	Fluctuation in Fluctuation i
Time of	MWBP-05B	P-3(B)	P-4(A)	P-5(B)	HFMW-05D		P-3(B)	(corrected)			
0		0.139	0.003	0.012	0	3.906	0.139	0.003	0.012	(maratee)	MITTEL COST MITTEL COE
0.0083		0.159	0.003	0.012	-0.003	3.982	0.151	0.003	0.015		
0.0166		0.164	0.003	0.012	0.000	4.205	0.164	0.003	0.012		
0.025		0.177	0.003	0.015	-0.006	4.319	0.177	0.003	0.015		
0.0333		0.189	0.003	0.019	0.003	4.389	0.189	0.003	0.019		
0.0416		0.202	0.003	0.019	-0.006	4.523	0.202	0.003	0.019		
0.05	4.662	0.214	0.003	0.012	0.003	4.662	0.214	0.003	0.012		
0.0583		0.221	0.003	0.019	0	4.771	0.221	0.003	0.019		
0.0666		0.233	0.003	0.022	-0.003	4.898	0.233	0.003	0.022		
0.075		0.246	0.003	0.019	0.003	4.949	0.246	0.003	0.019		
0.0833		0.259	0.003	0.015	0 003	5.05	0.259 0.271	0.003 0.003	0.015 0.022		
0.0916		0.271 0.284	0.003 0.003	0.022 0.022	0.003	5.133 5.209	0.271	0.003	0.022		
0.1 0.1083		0.204	0.003	0.022	0	5.336	0.297	0.003	0.009		
0.1166		0.309	0.003	0.012	-0.003	5.4	0.309	0.003	0.012		
0.125		0.322	0.003	0.009	0.003	5.508	0.322	0.003	0.009		
0.1333		0.328	0.003	0.012	0.003	5.495	0.328	0.003	0.012		
0.1416		0.341	0.003	0.012	-0.003	5.54	0.341	0.003	0.012		
0.15		0.354	0.003	0.019	0	5.686	0.354	0.003	0.019		
0.1583	5.8	0.36	0.003	0.019	0	5.8	0.36	0.003	0.019		
0.1666		0.373	0.003	0.019	0	5.743	0.373	0.003	0.019		
0.175		0.379	0.003	0.015	0	5.819	0.379	0.003	0.015		
0.1833		0.392	0.003	0.012	-0.003	5.908	0.392	0.003	0.012		
0.1916		0.398	0.003	0.022	0.003	5.978	0.398	0.003 0.003	0.022 0.015		
0.2083		0.41 0.417	0.003 0.003	0.015 0.015	0.003	6.01 6.093	0.41 0.417	0.003	0.015		
0.2083		0.429	0.003	0.013	0.003	6.131	0.417	0.006	0.022		
0.2100		0.436	0.003	0.015	-0.006	6.182	0.436	0.003	0.015		
0.2333		0.448	0.006	0.025	-0.003	6.232	0.448	0.006	0.025		
0.2416		0.455	0.006	0.025	-0.003	6.277	0.455	0.006	0.025		
0.25		0.461	0.006	0.028	-0.003	6.341	0.461	0.006	0.028		
0.2583		0.467	0.006	0.025	0	6.385	0.467	0.006	0.025		
0.2666		0.48	0.006	0.028	0	6.41	0.48	0.006	0.028		
0.275		0.486	0.006	0.028	-0.003	6.55	0.486	0.006	0.028		
0.2833		0.493	0.006	0.028	0	6.544	0.493	0.006	0.028		
0.2916		0.499 0.512	0.006 0.006	0.025 0.022	-0.003 -0.003	6.588 6.684	0.499 0.512	0.006 0.006	0.025 0.022		
0.3 0.3083		0.512	0.006	0.022	-0.003	6.69	0.512	0.006	0.022		
0.3166		0.524	0.006	0.025	0.000	6.76	0.524	0.006	0.025		
0.325		0.531	0.006	0.028	-0.003	6.792	0.531	0.006	0.028		
0.3333		0.537	0.006	0.025	0.003	6.849	0.537	0.006	0.025		
0.35	6.944	0.55	0.006	0.022	0.003	6.944	0.55	0.006	0.022		
0.3666		0.562	0.006	0.025	0	7.008	0.562	0.006	0.025		
0.3833		0.575	0.006	0.028	-0.003	7.103	0.575	0.006	0.028		
0.4		0.587	0.006	0.025	0.003	7.179	0.587	0.006	0.025		
0.4166		0.6	0.006	0.028	0	7.294	0.6	0.006 0.006	0.028 0.034		
0.4333 0.45		0.613 0.625	0.006	0.034 0.031	0.003	7.376 7.452	0.613 0.625	0.006	0.034		
0.4666		0.638	0.009	0.031	0.003	7.579	0.638	0.009	0.031		
0.4833		0.651	0.009	0.041	-0.003	7.662	0.651	0.009	0.041		
0.5		0.657	0.009	0.031	0.003	7.732	0.657	0.009	0.031		
0.5166		0.67	0.009	0.038	0	7.783	0.67	0.009	0.038		
0.5333		0.682	0.009	0.038	0	7.827	0.682	0.009	0.038		
0.55	7.935	0.689	0.009	0.041	0	7.935	0.689	0.009	0.041		
0.5666		0.701	0.009	0.038	0.003	8.031	0.701	0.009	0.038		
0.5833		0.708	0.009	0.044	0.003	8.075	0.708	0.009	0.044		
0.6		0.72	0.009	0.044	0 000	8.037	0.72	0.009	0.044		
0.6166		0.727	0.012	0.041	0.003	8.081 8.17	0.727 0.739	0.012 0.012	0.041 0.041		
0.6333		0.739 0.746	0.012 0.012	0.041 0.047	0	8.259	0.739	0.012	0.041		
0.65 0.6666		0.746	0.012	0.047	0.003	8.367	0.748	0.012	0.047		
0.6833		0.765	0.012	0.047	0.000	8.374	0.765	0.012	0.047		
0.7		0.777	0.012	0.047	-0.003	8.412	0.777	0.012	0.047		

Table B-3 36-Hour Constant Rate Discharge Data for MWBP-05B (Flow Rate = 16 gpm)

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Elapsed			т	ransducer	Readings of	Drawdown (fi	t)			Ba Elapsed	ckground Re Relative	adings Relative
Time of						MWBP-05B	P-3(B)	P-4(A)	P-5(B)	Time	Fluctuation in	Fluctuation in
	MWBP-05B	P-3(B)	P-4(A)	P-5(B)	HFMW-05D	(corrected)				(minutes)	MWBP-09A	MWBP-09B
0.7166	8.424	0.783	0.012	0.047				0.012 0.015	0.047 0.053			
0.7333	8.481	0.79 0.796	0.015 0.015	0.053 0.05			0.79 0.796	0.015	0.053			
0.75 0.7666	8.64 8.723	0.796	0.015	0.05				0.015	0.05			
0.7833	8.723	0.802	0.015	0.053				0.015	0.053			
0.7653	8.653	0.821	0.015	0.053				0.015	0.053			
0.8166	8.704	0.828	0.018	0.06				0.018	0.06			
0.8333	8.818	0.834	0.018	0.057				0.018	0.057			
0.85	8.875	0.84	0.018	0.057		8.875	0.84	0.018	0.057			
0.8666	8.996	0.847	0.018	0.06	0	8.996	0.847	0.018	0.06			
0.8833	8.996	0.853	0.018	0.06				0.018	0.06			
0.9	8.971	0.859	0.018	0.06			0.859	0.018	0.06			
0.9166	8.977	0.866	0.022	0.066				0.022	0.066			
0.9333	9.04	0.872	0.022	0.06				0.022	0.06 0.063			
0.95	9.167	0.872	0.022	0.063 0.066				0.022 0.022	0.063			
0.9666 0.9833	9.225 9.205	0.885 0.891	0.022 0.022	0.063				0.022	0.063			
0.9655	9.212	0.897	0.022	0.066				0.022	0.066	1	0.000	0.000
1.2	9.567	0.96	0.031	0.082				0.031	0.0823		0.00042	
1.4	9.745	0.992	0.037	0.098		9.745		0.037	0.09835		0.00049	
1.6	9.853	1.024	0.044	0.101	-0.003	9.853	1.024	0.044	0.1014		0.00056	
1.8	9.936	1.043	0.05	0.101	-0.009	9.936		0.05	0.10145		0.00063	
2	9.961	1.055	0.056	0.104			1.055	0.056	0.1045		0.0007	
2.2	10.025	1.068	0.063	0.104				0.063	0.10455		0.00077	
2.4	10.05	1.074	0.069	0.111	-0.006	10.05		0.069	0.1116		0.00084 0.00091	
2.6	10.094	1.081	0.075	0.111	-0.006			0.075 0.082	0.11165 0.1147		0.00091	
2.8	10.164 10.12	1.093 1.093	0.082 0.088	0.114 0.12				0.082	0.12075		0.00105	
3 3.2	10.12		0.088	0.123				0.094	0.1238		0.00112	
3.4	10.153	1.1	0.097	0.123				0.097	0.12385		0.00119	
3.6	10.177	1.106	0.104	0.123				0.104	0.1239		0.00126	0.0009
3.8	10.209	1.106	0.11	0.127	-0.009	10.209		0.11	0.12795		0.00133	
4	10.177	1.112	0.116	0.127				0.116	0.128		0.0014	
4.2	10.158	1.112	0.12	0.127				0.12	0.12805		0.00147	
4.4	10.196	1.112	0.123	0.13				0.123	0.1311		0.00154	
4.6	10.19	1.112	0.126	0.13				0.126	0.13115 0.1312		0.00161 0.00168	
4.8	10.266	1.112	0.129	0.13 0.13				0.129 0.135	0.13125		0.00175	
5 5.2	10.209 10.177	1.112 1.119	0.135 0.138	0.13				0.138	0.13123		0.00182	
5.4	10.177	1.119	0.142	0.136		10.19		0.142	0.13735		0.00189	
5.6	10.234	1.119	0.142	0.133				0.142	0.1344		0.00196	0.0014
5.8	10.209	1.119	0.145	0.136				0.145	0.13745		0.00203	
6	10.19	1.119	0.148	0.136	-0.009	10.19	1.119	0.148	0.1375		0.0021	
6.2	10.234	1.119	0.151	0.136				0.151	0.13755		0.00217	
6.4	10.24	1.125	0.154	0.139				0.154	0.1406		0.00224	
6.6	10.24	1.125	0.157	0.142				0.157	0.14365 0.1437		0.00231 0.00238	
6.8	10.215	1.125	0.157	0.142				0.157 0.161	0.1437		0.00236	
7 7.2	10.215 10.221	1.125 1.125	0.161 0.164	0.139 0.146				0.161	0.14075		0.00243	
7.4	10.221	1.125	0.164	0.140				0.164	0.14385		0.00259	
7.6	10.259	1.125	0.167	0.142				0.167	0.1439		0.00266	
7.8	10.259	1.131	0.17	0.139				0.17	0.14095		0.00273	0.00195
8	10.253	1.125	0.17	0.127		10.253	1.125	0.1728	0.129		0.0028	
8.2	10.24	1.125	0.17	0.12	-0.012			0.17287	0.12205		0.00287	
8.4	10.272	1.125	0.17	0.117				0.17294	0.1191		0.00294	
8.6	10.272	1.125	0.173	0.111				0.17601	0.11315		0.00301	
8.8	10.285	1.131	0.173	0.101				0.17608	0.1032		0.00308	
9	10.31	1.131	0.176	0.092				0.17915	0.09425		0.00315	
9.2	10.278	1.131	0.176	0.085				0.17922 0.17929	0.0873 0.08135		0.00322 0.00329	
9.4	10.31	1.131	0.176 0.18	0.079 0.076				0.17929	0.08135		0.00329	
9.6	10.272 10.291	1.131 1.131	0.183	0.076				0.18643	0.07845		0.00343	
9.8 10	10.251	1.131	0.186	0.076				0.1895	0.0875		0.0035	
10	10.239	1.131	0.100	0.000	J.012	10.200		0000	5.55.5	1		_,

Table B-3 36-Hour Constant Rate Discharge Data for MWBP-05B (Flow Rate = 16 gpm)

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						(Page 3 01 1	0,					
											ckground Rea	
Elapsed			Т	ransducer	Readings of [•		D 4(A)	D 5/D\	Elapsed Time	Relative	Relative Fluctuation in
Time of		D 0(D)	D 4/A)	D 6(D)	HFMW-05D	MWBP-05B (corrected)	P-3(B) (corrected)	P-4(A)	P-5(B)		MWBP-09A	MWBP-09B
	n) MWBP-05B	P-3(B)	P-4(A) 0.195	P-5(B) 0.076	-0.012	11.116	1.207	0.1992	0.079	(minutes)	0.0042	
	2 11.116 4 11.148	1.207 1.22	0.195	0.076	-0.012	11.118	1.22	0.2099	0.0605		0.0049	0.0035
	6 11.243	1.226	0.203	0.063	-0.012	11.243	1.226	0.2266	0.067		0.0056	
	8 11.243	1.232	0.23	0.069	-0.009	11.243	1.232	0.2363	0.0735		0.0063	0.0045
	0 11.205	1.232	0.243	0.098	-0.609	11.210	1.237	0.25	0.103	20	0.007	0.005
	2 11.218	1.232	0.243	0.076	-0.009	11.223	1.237	0.2503	0.0813		0.0073	0.0053
	11.224	1.239	0.255	0.092	-0.009	11.230	1.245	0.2626	0.0976		0.0076 0.0079	0.0056 0.0059
	11.237	1.239	0.262	0.114	-0.009	11.243	1.245 1.245	0.2699 0.2662	0.1199 0.1362		0.0079	
	28 11.269	1.239	0.258	0.13	-0.009 -0.009	11.275 11.238	1.245	0.2705	0.1645		0.0085	0.0065
	30 11.231 32 11.243	1.245 1.239	0.262 0.265	0.158 0.165	-0.009	11.250	1.246	0.2738	0.1718		0.0088	
	34 11.269	1.245	0.271	0.174	-0.012	11.276	1.252	0.2801	0.1811		0.0091	0.0071
	6 11.212	1.245	0.274	0.165		11.219	1.252	0.2834	0.1724		0.0094	
	8 11.313	1.245	0.281	0.152		11.321	1.253	0.2907	0.1597		0.0097	
	0 11.269	1.245	0.284	0.165		11.277	1.253	0.294	0.173	40	0.010	
4	11.275	1.251	0.287	0.174	-0.012	11.283	1.259	0.2979	0.1821		0.0109 0.0118	0.0081 0.0082
	11.218	1.245	0.29	0.174		11.226	1.253	0.3018	0.1822		0.0118	0.0082
	11.25	1.251	0.296	0.187	-0.015 -0.015	11.258 11.289	1.259 1.259	0.3087 0.3096	0.1953 0.2014		0.0127	
	11.281 10 11.319	1.251 1.258	0.296 0.3	0.193 0.187		11.328	1.259	0.3145	0.1955		0.0145	
	50 11.319 52 11.294	1.258	0.303	0.203		11.303	1.267	0.3184	0.2116		0.0154	
	54 11.3	1.258	0.306	0.209		11.309	1.267	0.3223	0.2177		0.0163	
	6 11.339	1.258	0.309	0.203		11.348	1.267	0.3262	0.2118		0.0172	
	11.319	1.258	0.309	0.203		11.328	1.267	0.3271	0.2119		0.0181	
6	11.351	1.258	0.315	0.117		11.360	1.267	0.334	0.126	60		
	32 11.345	1.258	0.312	0.095		11.355	1.268	0.3314	0.1045 0.121		0.0194 0.0198	
	11.345	1.258	0.315	0.111	-0.018 -0.022	11.355 11.356	1.268 1.269	0.3348 0.3422	0.121		0.0190	
	66 11.345 88 11.358	1.258 1.264	0.322 0.328	0.114 0.12		11.369	1.275	0.3486	0.131		0.0206	
	58 11.358 ; 70 11.389	1.204	0.325	0.114		11.401	1.282	0.346	0.1255		0.021	0.0115
	72 11.345	1.264	0.328	0.114		11.357	1.276	0.3494	0.126		0.0214	
	74 11.288	1.264	0.328	0.104	-0.018	11.301	1.277	0.3498	0.1165		0.0218	
	76 11.345	1.258	0.337	0.111	-0.025	11.358	1.271	0.3592	0.124		0.0222	
	78 11.364	1.264	0.341	0.127		11.378	1.278	0.3636	0.1405 0.134	80	0.0226 0.023	
	30 11.345	1.27	0.341	0.12		11.359 11.373	1.284 1.285	0.364 0.3646	0.1321	00	0.023	
	32 11.358 34 11.364	1.27 1.27	0.341 0.344	0.117 0.117		11.373	1.286	0.3682	0.1332		0.0242	
	34 11.364 36 11.358	1.27	0.344	0.117	-0.028	11.375	1.287	0.3718	0.1283		0.0248	
	38 11.364	1.264	0.347	0.117		11.382	1.282	0.3724	0.1354		0.0254	
	0 11.383	1.27	0.35	0.123		11.403	1.290	0.376	0.1425		0.026	
9	11.37	1.27	0.35	0.114	-0.025	11.391	1.291	0.3766	0.1346		0.0266	
	11.377	1.27	0.353	0.114		11.399		0.3802	0.1357		0.0272	
	96 11.402	1.27	0.344	0.114		11.425 11.458		0.3718 0.3844	0.1368 0.1509		0.0278 0.0284	
	11.434	1.277 1.277	0.356 0.356	0.127 0.107		11.430		0.385	0.1303	100		
	00 11.415 05 11.396	1.277	0.363	0.107		11.422		0.39275	0.13675		0.02975	
	10 11.434	1.283	0.36	0.107		11.461	1.310	0.3905	0.1335		0.0305	
	15 11.478	1.289	0.366	0.111		11.505		0.39725	0.13825		0.03125	
	20 11.472	1.289	0.369	0.114		11.500		0.401	0.142	120		
	25 11.497	1.289	0.378	0.127		11.526		0.41075	0.1555		0.03275	
	30 11.427	1.283	0.375	0.111		11.456		0.4085 0.41625	0.14 0.1465		0.0335 0.03425	
	35 11.44	1.289	0.382	0.117 0.107		11.470 11.470		0.413	0.1403	140		
	40 11.44 45 11.402	1.283 1.283	0.378 0.378	0.107		11.470		0.41375	0.13825	, , , ,	0.03575	
	50 11.402	1.283	0.385	0.107		11.429		0.4215	0.1495		0.0365	0.0325
	55 11.44	1.283	0.385	0.111				0.42225	0.14475		0.03725	
	50 11.358	1.289	0.394	0.123		11.393	1.324	0.432	0.158	160		
	55 11.377	1.289	0.397	0.123				0.436	0.15825		0.039	
	70 11.389	1.283	0.391	0.12				0.431	0.1555	1	0.04 0.041	
	75 11.465	1.302	0.397	0.12				0.438 0.443	0.15575 0.156			
	80 11.383	1.289	0.401 0.394	0.12 0.114				0.443	0.1505		0.042	
	85 11.377 90 11.345	1.289 1.289	0.394	0.114				0.446	0.16		0.042	
1	11.340	1.203	0.404	0.120	5.555	. 1.002				•		

Table B-3 36-Hour Constant Rate Discharge Data for MWBP-05B (Flow Rate = 16 gpm)

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										Ва	ckground Rea	•
Elapsed			Т	ransducer	Readings of			D 4/4)	D 5(D)	Elapsed	Relative	Relative Fluctuation in
Time of	MWBP-05B	P-3(B)	P-4(A)	P-5(B)	HFMW-05D	MWBP-05B (corrected)	P-3(B) (corrected)	P-4(A) (corrected)	P-5(B) (corrected)	Time (minutes)	MWBP-09A	MWBP-09B
195		1.289	0.407	0.127	-0.06	11.357	1.327	0.449	0.1645	(0.042	
200		1.289	0.407	0.123	-0.069	11.389	1.327	0.449	0.161	200	0.042	
205		1.289	0.404	0.12	-0.066	11.395	1.326	0.446	0.15725		0.042	
210		1.296	0.413	0.127	-0.066	11.382	1.333	0.455	0.1635		0.042	
215		1.296	0.416	0.127	-0.069	11.349	1.332	0.458	0.16275	200	0.042	
220		1.302	0.413	0.13	-0.069	11.418	1.337	0.455	0.165 0.1695	220	0.042 0.042	
225		1.308 1.308	0.42 0.42	0.133 0.133	-0.069 -0.072	11.483 11.459	1.345 1.346	0.462 0.462	0.1695		0.042	
230 235		1.306	0.429	0.133	-0.072	11.439	1.354	0.402	0.1815		0.042	
240		1.314	0.429	0.136	-0.072	11.487	1.355	0.471	0.177	240	0.042	
245		1.314	0.432	0.142	-0.075	11.487	1.355	0.474	0.1825		0.042	0.0405
250		1.314	0.432	0.142	-0.079	11.480	1.354	0.474	0.182		0.042	
255	11.472	1.314	0.435	0.146	-0.075	11.512	1.354	0.477	0.1855		0.042	
260		1.321	0.435	0.146	-0.079	11.492	1.360	0.477	0.185	260	0.042	
265		1.314	0.438	0.142	-0.082	11.478	1.352	0.479	0.18		0.041 0.04	0.038 0.037
270		1.321	0.442	0.146	-0.079 -0.082	11.458 11.482	1.358 1.357	0.482 0.484	0.183 0.185		0.039	
275 280		1.321 1.321	0.445 0.445	0.149 0.146	-0.082	11.494	1.356	0.483	0.181	280	0.038	
285		1.321	0.448	0.149	-0.085	11.513	1.356	0.48525	0.1835		0.03725	
290		1.327	0.448	0.149	-0.088	11.512	1.361	0.4845	0.183		0.0365	
295		1.327	0.454	0.155	-0.085	11.487	1.361	0.48975	0.1885		0.03575	
300		1.327	0.454	0.149	-0.088	11.524	1.360	0.489	0.182	300	0.035	
305		1.333	0.457	0.158	-0.091	11.517	1.366	0.49125	0.1905		0.03425 0.0335	
310		1.333	0.461	0.155 0.155	-0.088 -0.098	11.491 11.510	1.365 1.372	0.4945 0.49675	0.187 0.1865		0.0335	
315 320		1.34 1.34	0.464 0.467	0.155	-0.098	11.510	1.372	0.49075	0.1003	320	0.03273	
325		1.34	0.467	0.161	-0.091	11.509	1.371	0.49825	0.19175	V	0.03125	
330		1.34	0.47	0.165	-0.094	11.515	1.371	0.5005	0.1955		0.0305	0.0305
335		1.34	0.473	0.165	-0.094	11.495	1.370	0.50275	0.19525		0.02975	
340		1.34	0.476	0.161	-0.094	11.495	1.370	0.505	0.191	340	0.029	
345		1.34	0.476	0.161	-0.098	11.500	1.368	0.50425	0.1885		0.02825	
350		1.346	0.48	0.161	-0.094	11.522	1.371	0.5075 0.51275	0.186 0.1935		0.0275 0.02675	
355 360		1.359 1.352	0.486 0.486	0.171 0.177	-0.098 -0.098	11.577 11.555	1.382 1.372	0.51275	0.1935	360	0.02075	
365		1.352	0.489	0.177	-0.098	11.568	1.379	0.51325	0.19075	000	0.02425	
370		1.359	0.492	0.171	-0.098	11.555	1.379	0.5145	0.1905		0.0225	
375		1.359	0.495	0.174	-0.101	11.542	1.378	0.51575	0.19325		0.02075	
380	11.567	1.365	0.495	0.174	-0.101	11.586	1.384	0.514	0.193	380	0.019	
385		1.365	0.498	0.177	-0.101	11.529	1.384	0.51625	0.19575		0.01825	
390		1.365	0.502	0.184	-0.101	11.535	1.384	0.5195	0.2025		0.0175	
395		1.365	0.505	0.184	-0.101	11.566	1.383	0.52175 0.521	0.20225 0.202	400	0.01675 0.016	
400 405		1.371 1.371	0.505 0.508	0.184 0.187	-0.101 -0.101	11.547 11.584	1.389 1.388	0.52325	0.20425	400	0.01525	
410		1.371	0.511	0.19	-0.101	11.501	1.388	0.5255	0.2065		0.0145	
415		1.371	0.511	0.19	-0.098	11.532	1.387	0.52475	0.20575		0.01375	
420		1.371	0.514	0.19	-0.098	11.576	1.386	0.527	0.205	420	0.013	
425		1.371	0.517	0.19	-0.098	11.563	1.386	0.52925	0.2045		0.01225	
430		1.371	0.517	0.193	-0.094	11.524	1.385	0.5285	0.207		0.0115	
435		1.378	0.521	0.193	-0.094	11.556	1.392	0.53175	0.2065	440	0.010 7 5 0.010	
440		1.371 1.378	0.524 0.524	0.196 0.196	-0.091 -0.091	11.510 11.516	1.384 1.390	0.534 0.53325	0.209 0.20825	440	0.00925	
445 450		1.384	0.524	0.190	-0.088	11.560	1.396	0.5385	0.20025		0.0085	
450		1.304	0.53	0.203	-0.088	11.591	1.401	0.53775	0.21375		0.00775	
460		1.384	0.53	0.2	-0.085	11.577	1.394	0.537	0.21	460	0.007	
465		1.384	0.533	0.203	-0.085	11.570	1.393	0.53925	0.21175		0.00625	0.00875
470	11.586	1.39	0.533	0.203	-0.082	11.594	1.398	0.5385	0.2105		0.0055	
475		1.39	0.536	0.206	-0.082	11.554	1.396	0.54075	0.21225		0.00475	
480		1.39	0.54	0.206	-0.079	11.585	1.395	0.544	0.211	480	0.004	
485		1.397	0.54	0.209	-0.079	11.596	1.401	0.543 0.545	0.21325 0.2125		0.003 0.002	
490		1.397 1.397	0.543 0.546	0.209 0.212	-0.075 -0.072	11.584 11.614	1.401 1.400	0.545	0.2125		0.002	
495 500		1.403	0.546	0.212	-0.072	11.582	1.405	0.546	0.217	500	0.000	
505		1.409	0.546	0.212	-0.069	11.671	1.411	0.546	0.2135		0.000	

Table B-3 36-Hour Constant Rate Discharge Data for MWBP-05B (Flow Rate = 16 gpm)

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Elapsed			т	ransducer	Readings of	Drawdown (ft	•			Elapsed	ckground Rea	Relative
Time of	MWBP-05B	P-3(B)	P-4(A)	P-5(B)	HFMW-05D	MWBP-05B (corrected)	P-3(B)	P-4(A) (corrected)	P-5(B) (corrected)	Time (minutes)	Fluctuation in MWBP-09A	Fluctuation in MWBP-09B
510	11.618	1.403	0.549	0.215	-0.066	11.619	1.404	0.549	0.216	(minutes)	0.000	
515	11.637	1.409	0.549	0.212	-0.066	11.638	1.410	0.549	0.2125		0.000	
520	11.669	1.409	0.552	0.215	-0.06	11.669	1.409	0.552	0.215	520	0.000	0.000
525	11.643	1.409	0.552	0.215	-0.06	11.642	1.408	0.55125	0.214		-0.00075	
530	11.656	1.409	0.552	0.215	-0.06	11.654	1.407	0.5505	0.213		-0.0015	
535	11.681	1.409	0.555	0.219	-0.053	11.678	1.406	0.55275	0.216		-0.00225	
540	11.688	1.416	0.558	0.219	-0.053	11.684	1.412	0.555	0.215	540		
545	11.669	1.416	0.558	0.222	-0.053	11.665	1.412	0.55575	0.21775		-0.00225	
550	11.63	1.416	0.558	0.222	-0.053	11.626	1.412 1.411	0.5565 0.55725	0.2175 0.21425		-0.0015 -0.00075	
555 560	11.688 11.624	1.416 1.409	0.558 0.558	0.219 0.222	-0.05 -0.05	11.683 11.619	1.404	0.55725	0.21423	560		
565	11.605	1.403	0.558	0.222	-0.044	11.600	1.398	0.55725	0.2135	500	-0.00075	
570	11.611	1.409	0.558	0.219	-0.044	11.605	1.403	0.5565	0.213		-0.0015	
575	11.592	1.409	0.562	0.222	-0.044	11.586	1.403	0.55975	0.2155		-0.00225	
580	11.662	1.416	0.562	0.222	-0.044	11.655	1.409	0.559	0.215	580	-0.003	
585	11.649	1.416	0.562	0.222	-0.037	11.643	1.410	0.56075	0.2155		-0.00125	-0.0065
590	11.675	1.416	0.562	0.222	-0.037	11.669	1.410	0.5625	0.216		0.0005	-0.0060
595	11.656	1.416	0.562	0.222	-0.037	11.651	1.411	0.56425	0.2165		0.00225	
600	11.656	1.409	0.562	0.219	-0.037	11.651	1.404	0.566	0.214	600	0.004	-0.005
605	11.649	1.416	0.562	0.222	-0.034	11.645	1.412	0.56675	0.21775		0.00475	
610	11.681	1.409	0.562	0.219	-0.031	11.678	1.406	0.5675	0.2155		0.0055	
615	11.643	1.409	0.562	0.215	-0.031	11.640	1.406	0.56825	0.21225	600	0.00625	-0.00275
620	11.688	1.416	0.562	0.222	-0.031	11.686	1.414	0.569	0.22 0.216	620	0.007 0.00625	-0.002 -0.003
625	11.649 11.611	1.409 1.416	0.565 0.565	0.219 0.219	-0.028 -0.028	11.646 11.607	1.406 1.412	0.57125 0.5705	0.215		0.00525	-0.003
630 635	11.643	1.416	0.565	0.219	-0.026	11.638	1.412	0.56975	0.214		0.00330	
640	11.662	1.416	0.568	0.219	-0.025	11.656	1.410	0.572	0.213	640	0.004	-0.006
645	11.656	1.416	0.571	0.222	-0.022	11.650	1.410	0.574	0.21575	• • • • • • • • • • • • • • • • • • • •	0.003	-0.00625
650	11.649 ;	1.422	0.571	0.225	-0.018	11.643	1.416	0.573	0.2185		0.002	-0.0065
655	11.669	1.422	0.574	0.225	-0.018	11.662	1.415	0.575	0.21825		0.001	-0.00675
660	11.681	1.422	0.574	0.222	-0.022	11.674	1.415	0.574	0.215	660	0.000	-0.007
665	11.675	1.422	0.571	0.222	-0.018	11.668	1.415	0.572	0.21525		0.001	-0.00675
670	11.611	1.416	0.571	0.222	-0.018	11.605	1.410	0.573	0.2155		0.002	-0.00650
675	11.649	1.416	0.574	0.222	-0.018	11.643	1.410	0.577	0.21575		0.003	-0.00625
680	11.681	1.422	0.574	0.222	-0.015	11.675	1.416	0.578	0.216	680	0.004	-0.006
685	11.694	1.422	0.577	0.225	-0.015	11.687	1.415	0.58	0.218		0.003 0.002	-0.007 -0.008
690	11.611 11.63	1.416 1.422	0.574 0.581	0.222 0.228	-0.015 -0.012	11.603 11.621	1.408 1.413	0.576 0.582	0.214		0.002	-0.009
695 700	11.675	1.422	0.581	0.223	-0.012	11.665	1.412	0.581	0.213	700	0.000	-0.010
705	11.63	1.428	0.587	0.234	-0.009	11.620	1.418	0.58625	0.2235		-0.00075	-0.0105
710	11.675	1.428	0.584	0.231	-0.009	11.664	1.417	0.5825	0.22		-0.0015	-0.0110
715	11.643	1.428	0.584	0.231	-0.012	11.632	1.417	0.58175	0.2195		-0.00225	-0.0115
720	11.649	1.428	0.584	0.234	-0.009	11.637	1.416	0.581	0.222	720	-0.003	-0.012
725	11.669	1.428	0.584	0.231	-0.009	11.657	1.416	0.58175	0.21925		-0.00225	
730	11.669	1.428	0.584	0.231	-0.009	11.658	1.417	0.5825	0.2195		-0.0015	
735	11.643	1.422	0.584	0.231	-0.009	11.632	1,411	0.58325	0.21975	740	-0.00075	-0.01125
740	11.656	1.428	0.587	0.231	-0.009	11.645	1.417	0.587	0.22	740	0.000	-0.011
745	11.669	1.428	0.59	0.231	-0.009	11.658	1.417	0.58925	0.2195		-0.00075 -0.0015	
750 755	11.63 11.662	1.435 1.428	0.59 0.59	0.238 0.234	-0.009 -0.009	11.618 11.650	1.423 1.416	0.5885 0.58775	0.226 0.2215		-0.0015	
760	11.643	1.435	0.59	0.238	-0.009	11.630	1.422	0.587	0.2215	760	-0.00223	-0.0123
765	11.618	1.435	0.593	0.234	-0.009	11.605	1.422	0.59	0.221	700	-0.003	-0.013
770	11.669	1.435	0.593	0.238	-0.009	11.656	1.422	0.59	0.225		-0.003	-0.013
775	11.675	1.435	0.593	0.238	-0.012	11.662	1.422	0.59	0.225		-0.003	-0.013
780	11.675	1.435	0.593	0.238	-0.012	11.662	1.422	0.59	0.225	780	-0.003	-0.013
785	11.649	1.435	0.596	0.241	-0.009	11.636	1.422	0.59225	0.2275		-0.00375	-0.0135
790	11.624	1.435	0.596	0.241	-0.009	11.610	1.421	0.5915	0.227		-0.0045	
795	11.675	1.441	0.596	0.241	-0.012	11.661	1.427	0.59075	0.2265		-0.00525	-0.0145
800	11.694	1.441	0.599	0.241	-0.012	11.679	1.426	0.593	0.226	800	-0.006	-0.015
805	11.669	1.441	0.603	0.244	-0.012	11.655	1.427	0.59775	0.2295		-0.00525	-0.0145
810	11.618	1.441	0.603	0.244	-0.012	11.604	1.427	0.5985	0.23		-0.0045	-0.014
815	11.681	1.441	0.603	0.244	-0.012	11.668	1.428	0.59925	0.2305	920	-0.00375	-0.0135
820	11.681	1.441	0.599	0.244	-0.015	11.668	1.428	0.596	0.231	820	-0.003	-0.013

Table B-3 36-Hour Constant Rate Discharge Data for MWBP-05B (Flow Rate = 16 gpm)

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1050 11.688 1.454 0.618 0. 1055 11.726 1.454 0.622 0. 1060 11.694 1.447 0.618 0. 1065 11.745 1.454 0.618 0. 1070 11.719 1.454 0.622 0. 1075 11.751 1.454 0.622 0. 1080 11.77 1.46 0.622 0. 1085 11.745 1.454 0.625 0. 1090 11.745 1.454 0.622		MWBP-05B				Elapsed	Relative	Relative
825	LIENNA OFF		P-3(B) (corrected)	P-4(A) (corrected)	P-5(B)		Fluctuation in MWBP-09A	Fluctuation in MWBP-09B
830	1 -0.01		1.424	0.59775	0.22975	(minutes)	-0.00125	-0.01125
835			1.426	0.5995	0.2315		0.0005	
840 11.713 1.435 0.593 0. 845 11.707 1.435 0.593 0. 850 11.713 1.435 0.593 0. 855 11.688 1.428 0.593 0. 866 11.669 1.435 0.593 0. 870 11.7 1.435 0.593 0. 880 11.726 1.428 0.593 0. 881 11.688 1.428 0.593 0. 882 11.656 1.422 0.587 0. 883 11.732 1.435 0.593 0. 895 11.732 1.435 0.593 0. 900 11.662 1.428 0.593 0. 905 11.669 1.435 0.593 0. 915 11.745 1.435 0.596 0. 920 11.681 1.435 0.596 0. 920 11.681 1.435 0.596 0. 921 11.713 1.425 0.596 0. 922 11.681 1.435 0.596 0. 933 11.713 1.435 0.596 0. 935 11.713 1.435 0.596 0. 945 11.719 1.435 0.596 0. 945 11.719 1.435 0.596 0. 955 11.713 1.435 0.596 0. 955 11.662 1.435 0.596 0. 955 11.675 1.435 0.596 0. 955 11.713 1.435 0.596 0. 955 11.714 1.435 0.596 0. 955 11.715 1.435 0.596 0. 955 11.717 1.447 0.609 0. 1005 11.686 1.428 0.599 0. 1005 11.686 1.428 0.599 0. 1005 11.686 1.428 0.599 0. 1005 11.686 1.428 0.599 0. 1005 11.686 1.428 0.599 0. 1005 11.686 1.428 0.599 0. 1006 11.687 1.447 0.618 0. 1007 1.719 1.447 0.618 0. 1008 11.775 1.447 0.618 0. 1055 11.726 1.454 0.622 0. 1080 11.745 1.454 0.622 0. 1085 11.745 1.454 0.622 0. 1080 11.745 1.454 0.622 0. 1080 11.745 1.454 0.622 0. 1080 11.745 1.454 0.622 0. 1080 11.745 1.454 0.622 0. 1080 11.745 1.454 0.622 0. 1085 11.745 1.454 0.622 0. 1085 11.745 1.454 0.622			1.427	0.59825	0.23025		0.00225	
845 11.707 1.435 0.593 0. 850 11.713 1.435 0.593 0. 855 11.688 1.428 0.593 0. 860 11.669 1.435 0.593 0. 865 11.662 1.435 0.593 0. 870 11.7 1.435 0.593 0. 875 11.688 1.428 0.593 0. 880 11.726 1.428 0.593 0. 890 11.713 1.422 0.587 0. 890 11.713 1.422 0.587 0. 895 11.732 1.435 0.596 0. 905 11.669 1.435 0.596 0. 905 11.669 1.435 0.596 0. 915 11.745 1.435 0.596 0. 920 11.681 1.435 0.599 0. 925 11.713 1.435 0.596 </td <td></td> <td></td> <td>1.429</td> <td>0.597</td> <td>0.228</td> <td>840</td> <td>0.004</td> <td>-0.006</td>			1.429	0.597	0.228	840	0.004	-0.006
850	4 -0.01	8 11.702	1.430	0.59775	0.229		0.00475	-0.005
860 11.669 1.435 0.593 0.865 865 11.662 1.435 0.593 0.870 870 11.7 1.435 0.593 0.871 875 11.688 1.428 0.593 0.888 880 11.726 1.428 0.593 0.8885 885 11.656 1.422 0.587 0.8885 890 11.713 1.432 0.587 0.909 900 11.662 1.428 0.593 0.909 905 11.669 1.435 0.596 0.909 915 11.745 1.435 0.596 0.909 915 11.745 1.435 0.596 0.909 920 11.681 1.435 0.596 0.909 925 11.771 1.435 0.596 0.909 925 11.771 1.435 0.596 0.909 935 11.669 1.435 0.596 0.909 940 11.669<	1 -0.01	8 11.709	1.431	0.5985	0.227		0.0055	
865 11.662 1.435 0.593 0. 870 11.7 1.435 0.593 0. 875 11.688 1.428 0.593 0. 880 11.726 1.428 0.593 0. 885 11.656 1.422 0.587 0. 890 11.713 1.422 0.587 0. 895 11.732 1.435 0.599 0. 900 11.662 1.428 0.593 0. 905 11.669 1.435 0.596 0. 915 11.745 1.435 0.596 0. 915 11.745 1.435 0.596 0. 920 11.681 1.435 0.599 0. 925 11.719 1.435 0.596 0. 935 11.675 1.435 0.596 0. 940 11.669 1.435 0.596 0. 945 11.713 1.435 0.596 </td <td></td> <td></td> <td>1.425</td> <td>0.59925</td> <td>0.231</td> <td></td> <td>0.00625</td> <td>-0.003</td>			1.425	0.59925	0.231		0.00625	-0.003
870 11.7 1.435 0.593 0. 875 11.688 1.428 0.593 0. 880 11.726 1.428 0.59 0. 885 11.656 1.422 0.587 0. 890 11.713 1.422 0.587 0. 895 11.732 1.435 0.599 0. 900 11.662 1.428 0.593 0. 905 11.669 1.435 0.596 0. 910 11.732 1.435 0.596 0. 915 11.745 1.435 0.596 0. 915 11.745 1.435 0.599 0. 920 11.681 1.435 0.599 0. 925 11.713 1.435 0.596 0. 935 11.675 1.435 0.596 0. 940 11.669 1.435 0.596 0. 945 11.713 1.428 0.593 <td></td> <td></td> <td>1.433</td> <td>0.6</td> <td>0.232</td> <td>860</td> <td>0.007</td> <td>-0.002</td>			1.433	0.6	0.232	860	0.007	-0.002
875			1.435	0.60225	0.23425		0.00925	
880			1.438	0.6045	0.2335		0.0115	
885			1.433	0.60675	0.23575	880	0.01375 0.016	
890 11.713 1.422 0.587 0. 895 11.732 1.435 0.59 0. 900 11.662 1.428 0.593 0. 905 11.669 1.435 0.596 0. 910 11.732 1.435 0.596 0. 915 11.745 1.435 0.596 0. 920 11.681 1.435 0.599 0. 925 11.719 1.435 0.599 0. 930 11.713 1.435 0.596 0. 940 11.669 1.435 0.596 0. 941 11.713 1.435 0.596 0. 941 11.719 1.428 0.593 0. 942 11.719 1.428 0.593 0. 943 11.713 1.435 0.596 0. 945 11.713 1.435 0.596 0. 955 11.713 1.435 0.596 0. 955 11.713 1.435 0.596 0. 955 11.688 1.435 0.596 0. 960 11.643 1.428 0.593 0. 961 11.643 1.428 0.593 0. 970 11.707 1.435 0.599 0. 988 11.745 1.435 0.596 0. 988 11.745 1.435 0.596 0. 995 11.738 1.435 0.596 0. 995 11.738 1.428 0.596 0. 995 11.738 1.428 0.596 0. 1005 11.665 1.428 0.599 0. 1010 11.662 1.435 0.596 0. 1015 11.738 1.441 0.606 0. 1015 11.738 1.441 0.606 0. 1025 11.707 1.447 0.609 0. 1030 11.7 1.447 0.612 0. 1035 11.719 1.447 0.612 0. 1036 11.719 1.454 0.618 0. 1045 11.732 1.454 0.622 0. 1050 11.688 1.454 0.618 0. 1051 11.751 1.454 0.622 0. 1075 11.776 1.454 0.622 0. 1075 11.776 1.454 0.622 0. 1075 11.776 1.454 0.622 0. 1075 11.776 1.454 0.622 0. 1076 11.779 1.454 0.622 0. 1077 11.719 1.454 0.622 0. 1078 11.771 1.466 0.622 0. 1079 11.771 1.454 0.622 0. 1075 11.775 1.454 0.622 0. 1080 11.77 1.466 0.622 0. 1085 11.745 1.454 0.622			1.435	0.606 0.60225	0.235 0.2315	000	0.01525	
895 11.732 1.435 0.593 0. 900 11.662 1.428 0.593 0. 905 11.669 1.435 0.596 0. 910 11.732 1.435 0.596 0. 915 11.745 1.435 0.596 0. 920 11.681 1.435 0.599 0. 925 11.719 1.435 0.599 0. 930 11.713 1.435 0.596 0. 935 11.675 1.435 0.596 0. 940 11.669 1.435 0.596 0. 945 11.719 1.428 0.593 0. 945 11.713 1.435 0.596 0. 950 11.662 1.435 0.596 0. 955 11.713 1.435 0.599 0. 970 11.707 1.435 0.599 0. 975 11.675 1.435 0.596			1.429 1.428	0.60225	0.2313		0.01323	
900			1.441	0.60375	0.2335		0.01375	
905			1.433	0.606	0.236	900	0.013	
910			1.440	0.609	0.23625		0.013	
915			1.441	0.609	0.2365		0.013	
920			1.441	0.609	0.23675		0.013	0.00575
925			1.441	0.612	0.24	920	0.013	
935	4 -0.04	1 11.725	1.441	0.61275	0.24		0.01375	
940 11.669 1.435 0.596 0. 945 11.719 1.428 0.593 0. 950 11.662 1.435 0.596 0. 955 11.713 1.435 0.596 0. 960 11.643 1.428 0.593 0. 965 11.688; 1.435 0.599 0. 970 11.707 1.435 0.599 0. 975 11.675 1.435 0.596 0. 980 11.745 1.435 0.596 0. 985 11.713 1.435 0.596 0. 985 11.73 1.435 0.596 0. 990 11.751 1.435 0.596 0. 995 11.738 1.428 0.596 0. 995 11.738 1.428 0.596 0. 1005 11.656 1.428 0.596 0. 1015 11.738 1.441 0.606 0. 1015 11.738 1.441 0.606 0. 1020 11.738 1.441 0.609 0. 1025 11.707 1.447 0.609 0. 1030 11.7 1.447 0.612 0. 1030 11.719 1.447 0.615 0. 1040 11.719 1.454 0.618 0. 1055 11.726 1.454 0.622 0. 1060 11.694 1.447 0.618 0. 1070 11.719 1.454 0.622 0. 1075 11.751 1.454 0.622 0. 1080 11.77 1.46 0.622 0. 1080 11.77 1.46 0.622 1. 1080 11.77 1.454 0.622 1. 1080 11.77 1.454 0.622 1. 1080 11.77 1.454 0.622 1. 1080 11.77 1.454 0.622 1. 1080 11.77 1.454 0.622 1. 1080 11.77 1.454 0.622 1. 1080 11.77 1.454 0.622 1. 1080 11.77 1.454 0.622 1. 1080 11.77 1.466 0.622 1. 1080 11.77 1.454 0.622 1. 1080 11.77 1.466 0.622 1. 1080 11.77 1.466 0.622 1. 1080 11.77 1.466 0.622 1. 1080 11.77 1.454 0.622 1. 1080 11.775 1.454 0.622 1. 1080 11.775 1.454 0.622 1.	1 -0.04		1.441	0.6105	0.237		0.0145	
945 11.719 1.428 0.593 0.950 11.662 1.435 0.596 0.955 11.713 1.435 0.596 0.960 11.643 1.428 0.593 0.965 11.688; 1.435 0.599 0.970 11.707 1.435 0.599 0.975 11.675 1.435 0.596 0.985 11.745 1.435 0.596 0.985 11.745 1.435 0.596 0.985 11.773 1.435 0.596 0.995 11.738 1.428 0.596 0.995 11.738 1.428 0.596 0.995 11.738 1.428 0.596 0.995 11.656 1.428 0.596 0.1005 11.656 1.428 0.599 0.1015 11.738 1.441 0.606 0.1015 11.738 1.441 0.606 0.1020 11.738 1.441 0.609 0.1025 11.707 1.447 0.609 0.1025 11.707 1.447 0.612 0.1030 11.7 1.447 0.612 0.1035 11.719 1.454 0.618 0.1045 11.732 1.454 0.618 0.1055 11.726 1.454 0.622 0.1050 11.694 1.447 0.618 0.1055 11.726 1.454 0.622 0.1075 11.751 1.454 0.622 0.1075 11.751 1.454 0.622 0.1085 11.775 1.454 0.622 0.1080 11.775 1.454 0.622 0.1085 11.775 1.454 0.622 0.1085 11.775 1.454 0.622 0.1080 11.775 1.454 0.622 0.1085 11.775 1.454 0.622 0.1085 11.775 1.454 0.622 0.1080 11.775 1.454 0.622 0.1080 11.775 1.454 0.622 0.1080 11.775 1.454 0.622 0.1080 11.775 1.454 0.622 0.1080 11.775 1.454 0.622 0.1080 11.775 1.454 0.622 0.1080 11.775 1.454 0.622 0.1080 11.775 1.454 0.622 0.1080 11.775 1.454 0.622 0.1080 11.775 1.454 0.622 0.1080 11.775 1.454 0.622 0.1080 11.775 1.454 0.622 0.1080 11.775 1.454 0.622 0.1080 11.775 1.454 0.622 0.1080 11.775 1.454 0.622 0.1080 11.775 1.454 0.622 0.1080 11			1.441	0.61125	0.237		0.01525	
950			1.441	0.612	0.234	940	0.016	
955 11.713 1.435 0.596 0.960 11.643 1.428 0.593 0.965 11.688; 1.435 0.599 0.970 11.707 1.435 0.599 0.975 11.675 1.435 0.596 0.985 11.745 1.435 0.596 0.985 11.713 1.435 0.596 0.995 11.751 1.435 0.596 0.995 11.738 1.428 0.596 0.995 11.738 1.428 0.596 0.995 11.738 1.428 0.596 0.995 11.656 1.428 0.596 0.995 11.656 1.428 0.599 0.905 11.662 1.435 0.603 0.905 11.738 1.441 0.606 0.905 11.738 1.441 0.606 0.905 11.738 1.441 0.609 0.905 11.778 1.447 0.612 0.905 11.779 1.447 0.612 0.905 11.719 1.447 0.615 0.905 11.719 1.447 0.618 0.905 11.726 1.454 0.618 0.905 11.726 1.454 0.622 0.905 11.726 1.454 0.622 0.905 11.751 1.454 0.622 0.905 11.751 1.454 0.622 0.905 11.751 1.454 0.622 0.905 11.751 1.454 0.622 0.905 11.751 1.454 0.622 0.905 11.751 1.454 0.622 0.905 11.775 11.751 1.454 0.622 0.905 11.775 11.751 1.454 0.622 0.905 11.775 11.751 1.454 0.622 0.905 11.775 11.751 1.454 0.622 0.905 11.775 11.751 1.454 0.622 0.905 11.775 11.751 1.454 0.622 0.905 11.775 11.751 1.454 0.622 0.905 11.775 11.751 1.454 0.622 0.905 11.775 11.751 1.454 0.622 0.905 11.775 11.751 1.454 0.622 0.905 11.775 11.751 1.454 0.622 0.905 11.775 11.775 1.454 0.622 0.905 11.775 11.7751 1.454 0.622 0.905 11.775 11.454 0.622 0.905 11.775 11.7751 1.454 0.622 0.905 11.775 11.7751 1.454 0.			1.435	0.60975	0.235		0.01675	
960 11.643 1.428 0.593 0. 965 11.688; 1.435 0.599 0. 970 11.707 1.435 0.599 0. 975 11.675 1.435 0.596 0. 980 11.745 1.435 0.596 0. 985 11.713 1.435 0.596 0. 995 11.738 1.428 0.596 0. 995 11.738 1.428 0.596 0. 1000 11.688 1.435 0.596 0. 1005 11.656 1.428 0.599 0. 1015 11.738 1.441 0.606 0. 1015 11.738 1.441 0.606 0. 1020 11.738 1.441 0.609 0. 1025 11.707 1.447 0.609 0. 1030 11.7 1.447 0.612 0. 1035 11.719 1.454 0.618 0. 1045 11.732 1.454 0.622 0. 1060 11.694 1.447 0.618 0. 1070 11.719 1.454 0.622 0. 1075 11.751 1.454 0.622 0. 1075 11.751 1.454 0.622 0. 1080 11.77 1.46 0.622 0. 1080 11.77 1.46 0.622 1. 1080 11.77 1.46 0.622 1. 1080 11.77 1.46 0.622 1. 1080 11.77 1.454 0.625 1. 1080 11.77 1.454 0.625 1. 1080 11.77 1.46 0.622			1.443	0.6135	0.239 0.237		0.0175 0.01825	
965 11.688; 1.435 0.599 0. 970 11.707 1.435 0.599 0. 975 11.675 1.435 0.596 0. 980 11.745 1.435 0.596 0. 985 11.713 1.435 0.596 0. 990 11.751 1.435 0.596 0. 995 11.738 1.428 0.596 0. 1000 11.688 1.435 0.596 0. 1005 11.656 1.428 0.599 0. 1010 11.662 1.435 0.603 0. 1015 11.738 1.441 0.606 0. 1020 11.738 1.441 0.609 0. 1025 11.707 1.447 0.609 0. 1030 11.7 1.447 0.612 0. 1035 11.719 1.454 0.618 0. 1040 11.719 1.454 0.618 0. 1055 11.726 1.454 0.622 0. 1060 11.694 1.447 0.618 0. 1075 11.719 1.454 0.622 0. 1075 11.719 1.454 0.622 0. 1075 11.719 1.454 0.622 0. 1075 11.751 1.454 0.622 0. 1080 11.77 1.46 0.622 1. 1080 11.77 1.46 0.622 1. 1080 11.77 1.46 0.622 1. 1085 11.745 1.454 0.625 1. 1090 11.745 1.454 0.622			1.444 1.438	0.61425 0.612	0.237	960	0.01023	
970 11.707 1.435 0.599 0. 975 11.675 1.435 0.596 0. 980 11.745 1.435 0.596 0. 985 11.713 1.435 0.596 0. 990 11.751 1.435 0.596 0. 995 11.738 1.428 0.596 0. 1000 11.688 1.435 0.596 0. 1005 11.656 1.428 0.599 0. 1010 11.662 1.435 0.603 0. 1015 11.738 1.441 0.606 0. 1020 11.738 1.441 0.609 0. 1025 11.707 1.447 0.609 0. 1030 11.7 1.447 0.612 0. 1035 11.719 1.447 0.615 0. 1040 11.719 1.454 0.618 0. 1055 11.726 1.454 0.622 0. 1060 11.694 1.447 0.618 0. 1065 11.745 1.454 0.622 0. 1075 11.719 1.454 0.622 0. 1075 11.751 1.454 0.622 0. 1080 11.77 1.46 0.622 0. 1080 11.77 1.46 0.622 0. 1085 11.745 1.454 0.625 0. 1085 11.745 1.454 0.625 0. 1085 11.745 1.454 0.625 0. 1080 11.775 1.454 0.625 0. 1080 11.775 1.454 0.625 0. 1085 11.745 1.454 0.625			1.446	0.612	0.24175	300	0.020	
975 11.675 1.435 0.596 0. 980 11.745 1.435 0.596 0. 985 11.713 1.435 0.596 0. 990 11.751 1.435 0.596 0. 995 11.738 1.428 0.596 0. 1000 11.688 1.435 0.596 0. 1005 11.656 1.428 0.599 0. 1010 11.662 1.435 0.603 0. 1015 11.738 1.441 0.606 0. 1020 11.738 1.441 0.609 0. 1025 11.707 1.447 0.609 0. 1030 11.7 1.447 0.612 0. 1035 11.719 1.447 0.615 0. 1040 11.719 1.454 0.618 0. 1050 11.688 1.454 0.618 0. 1055 11.726 1.454			1.447	0.62	0.2455		0.021	0.0115
980 11.745 1.435 0.596 0. 985 11.713 1.435 0.596 0. 990 11.751 1.435 0.596 0. 995 11.738 1.428 0.596 0. 1000 11.688 1.435 0.596 0. 1005 11.656 1.428 0.599 0. 1010 11.662 1.435 0.603 0. 1015 11.738 1.441 0.606 0. 1020 11.738 1.441 0.609 0. 1025 11.707 1.447 0.609 0. 1030 11.7 1.447 0.612 0. 1035 11.719 1.447 0.615 0. 1040 11.719 1.454 0.618 0. 1055 11.726 1.454 0.618 0. 1055 11.726 1.454 0.618 0. 1060 11.694 1.447 0.618 0. 1065 11.745 1.454 0.622 0. 1070 11.719 1.454 0.622 0. 1070 11.719 1.454 0.622 0. 1071 11.719 1.454 0.618 0. 1072 11.719 1.454 0.618 0. 1073 11.719 1.454 0.618 0. 1074 11.719 1.454 0.618 0. 1075 11.751 1.454 0.622 0. 1080 11.77 1.46 0.622 0. 1080 11.77 1.46 0.622 0. 1080 11.77 1.46 0.622 0. 1085 11.745 1.454 0.625 0.			1.447	0.618	0.24325		0.022	
985 11.713 1.435 0.596 0. 990 11.751 1.435 0.596 0. 995 11.738 1.428 0.596 0. 1000 11.688 1.435 0.596 0. 1005 11.656 1.428 0.599 0. 1010 11.662 1.435 0.603 0. 1015 11.738 1.441 0.606 0. 1020 11.738 1.441 0.609 0. 1025 11.707 1.447 0.609 0. 1030 11.7 1.447 0.612 0. 1035 11.719 1.447 0.615 0. 1040 11.719 1.454 0.618 0. 1050 11.688 1.454 0.618 0. 1055 11.726 1.454 0.622 0. 1060 11.694 1.447 0.618 0. 1075 11.751 1.454			1.448	0.619	0.244	980	0.023	
990 11.751 1.435 0.596 0. 995 11.738 1.428 0.596 0. 1000 11.688 1.435 0.596 0. 1005 11.656 1.428 0.599 0. 1010 11.662 1.435 0.603 0. 1015 11.738 1.441 0.606 0. 1020 11.738 1.441 0.609 0. 1025 11.707 1.447 0.609 0. 1030 11.7 1.447 0.612 0. 1035 11.719 1.447 0.615 0. 1040 11.719 1.454 0.618 0. 1055 11.726 1.454 0.622 0. 1060 11.694 1.447 0.618 0. 1065 11.745 1.454 0.618 0. 1070 11.719 1.454 0.618 0. 1070 11.719 1.454 0.618 0. 1070 11.719 1.454 0.622 0. 1080 11.77 1.454 0.622 0. 1080 11.77 1.46 0.622 0. 1080 11.77 1.46 0.622 1. 1080 11.77 1.46 0.622 1. 1080 11.77 1.46 0.622 1. 1080 11.745 1.454 0.625 1. 1090 11.745 1.454 0.625 1.			1.449	0.619	0.2415		0.023	
995 11.738 1.428 0.596 0. 1000 11.688 1.435 0.596 0. 1005 11.656 1.428 0.599 0. 1010 11.662 1.435 0.603 0. 1015 11.738 1.441 0.606 0. 1020 11.738 1.441 0.609 0. 1025 11.707 1.447 0.609 0. 1030 11.7 1.447 0.612 0. 1035 11.719 1.447 0.615 0. 1040 11.719 1.454 0.618 0. 1045 11.732 1.454 0.622 0. 1050 11.688 1.454 0.618 0. 1055 11.726 1.454 0.622 0. 1060 11.694 1.447 0.618 0. 1075 11.719 1.454 0.622 0. 1075 11.771 1.454			1.449	0.619	0.242		0.023	0.014
1000 11.688 1.435 0.596 0. 1005 11.656 1.428 0.599 0. 1010 11.662 1.435 0.603 0. 1015 11.738 1.441 0.606 0. 1020 11.738 1.441 0.609 0. 1025 11.707 1.447 0.609 0. 1030 11.7 1.447 0.612 0. 1035 11.719 1.447 0.615 0. 1040 11.719 1.454 0.618 0. 1045 11.732 1.454 0.622 0. 1050 11.688 1.454 0.622 0. 1050 11.688 1.454 0.622 0. 1060 11.694 1.447 0.618 0. 1065 11.745 1.454 0.622 0. 1075 11.751 1.454 0.622 0. 1075 11.751 1.454	8 -0.0	6 11.753	1.443	0.619	0.2425		0.023	
1005 11.656 1.428 0.599 0. 1010 11.662 1.435 0.603 0. 1015 11.738 1.441 0.606 0. 1020 11.738 1.441 0.609 0. 1025 11.707 1.447 0.609 0. 1030 11.7 1.447 0.612 0. 1035 11.719 1.447 0.615 0. 1040 11.719 1.454 0.618 0. 1045 11.732 1.454 0.622 0. 1050 11.688 1.454 0.622 0. 1055 11.726 1.454 0.622 0. 1060 11.694 1.447 0.618 0. 1070 11.719 1.454 0.622 0. 1075 11.751 1.454 0.622 0. 1080 11.77 1.454 0.622 0. 1085 11.745 1.454	8 -0.06	3 11.703	1.450	0.619	0.243	1000	0.023	
1015 11.738 1.441 0.606 0. 1020 11.738 1.441 0.609 0. 1025 11.707 1.447 0.609 0. 1030 11.7 1.447 0.612 0. 1035 11.719 1.447 0.615 0. 1040 11.719 1.454 0.618 0. 1045 11.732 1.454 0.622 0. 1050 11.688 1.454 0.618 0. 1055 11.726 1.454 0.622 0. 1060 11.694 1.447 0.618 0. 1070 11.745 1.454 0.622 0. 1075 11.751 1.454 0.622 0. 1080 11.77 1.46 0.622 0. 1085 11.745 1.454 0.625 0. 1090 11.745 1.454 0.622 0.	1 -0.06	3 11.670	1.442	0.62025	0.2445		0.02125	
1020 11.738 1.441 0.609 0. 1025 11.707 1.447 0.609 0. 1030 11.7 1.447 0.612 0. 1035 11.719 1.447 0.615 0. 1040 11.719 1.454 0.618 0. 1045 11.732 1.454 0.622 0. 1050 11.688 1.454 0.618 0. 1055 11.726 1.454 0.622 0. 1060 11.694 1.447 0.618 0. 1065 11.745 1.454 0.622 0. 1070 11.719 1.454 0.622 0. 1075 11.751 1.454 0.622 0. 1080 11.77 1.46 0.622 0. 1085 11.745 1.454 0.625 0. 1090 11.745 1.454 0.622 0.		3 11.674	1.447	0.6225	0.246		0.0195	
1025 11.707 1.447 0.609 0. 1030 11.7 1.447 0.612 0. 1035 11.719 1.447 0.615 0. 1040 11.719 1.454 0.618 0. 1045 11.732 1.454 0.622 0. 1050 11.688 1.454 0.618 0. 1055 11.726 1.454 0.622 0. 1060 11.694 1.447 0.618 0. 1065 11.745 1.454 0.618 0. 1070 11.719 1.454 0.622 0. 1075 11.751 1.454 0.622 0. 1080 11.77 1.46 0.622 0. 1085 11.745 1.454 0.625 0. 1090 11.745 1.454 0.622 0.			1.452	0.62375	0.2445		0.01775	
1030 11.7 1.447 0.612 0. 1035 11.719 1.447 0.615 0. 1040 11.719 1.454 0.618 0. 1045 11.732 1.454 0.622 0. 1050 11.688 1.454 0.618 0. 1055 11.726 1.454 0.622 0. 1060 11.694 1.447 0.618 0. 1065 11.745 1.454 0.618 0. 1070 11.719 1.454 0.622 0. 1075 11.751 1.454 0.622 0. 1080 11.77 1.46 0.622 0. 1085 11.745 1.454 0.625 0. 1090 11.745 1.454 0.622 0.			1.450	0.625	0.247	1020	0.016	
1035 11.719 1.447 0.615 0. 1040 11.719 1.454 0.618 0. 1045 11.732 1.454 0.622 0. 1050 11.688 1.454 0.618 0. 1055 11.726 1.454 0.622 0. 1060 11.694 1.447 0.618 0. 1065 11.745 1.454 0.618 0. 1070 11.719 1.454 0.622 0. 1075 11.751 1.454 0.622 0. 1080 11.77 1.46 0.622 0. 1085 11.745 1.454 0.625 0. 1090 11.745 1.454 0.622 0.			1.454	0.62275	0.24775		0.01375	
1040 11.719 1.454 0.618 0. 1045 11.732 1.454 0.622 0 1050 11.688 1.454 0.618 0 1055 11.726 1.454 0.622 0 1060 11.694 1.447 0.618 0 1065 11.745 1.454 0.618 0 1070 11.719 1.454 0.622 0 1075 11.751 1.454 0.622 0 1080 11.77 1.46 0.622 0 1085 11.745 1.454 0.625 0 1090 11.745 1.454 0.622 0			1.452 1.449	0.6235 0.62425	0.2485 0.24625		0.0115 0.00925	
1045 11.732 1.454 0.622 0 1050 11.688 1.454 0.618 0 1055 11.726 1.454 0.622 0 1060 11.694 1.447 0.618 0 1065 11.745 1.454 0.618 0 1070 11.719 1.454 0.622 0 1075 11.751 1.454 0.622 0 1080 11.77 1.46 0.622 0 1085 11.745 1.454 0.625 0 1090 11.745 1.454 0.622 0				0.625	0.24023	1040		
1050 11.688 1.454 0.618 0. 1055 11.726 1.454 0.622 0. 1060 11.694 1.447 0.618 0. 1065 11.745 1.454 0.618 0. 1070 11.719 1.454 0.622 0. 1075 11.751 1.454 0.622 0. 1080 11.77 1.46 0.622 0. 1085 11.745 1.454 0.625 0. 1090 11.745 1.454 0.622	5 -0.06			0.629	0.2495	1040	0.007	
1055 11.726 1.454 0.622 0. 1060 11.694 1.447 0.618 0. 1065 11.745 1.454 0.618 0. 1070 11.719 1.454 0.622 0. 1075 11.751 1.454 0.622 0. 1080 11.77 1.46 0.622 0. 1085 11.745 1.454 0.625 0. 1090 11.745 1.454 0.622				0.625	0.246		0.007	
1060 11.694 1.447 0.618 0. 1065 11.745 1.454 0.618 0. 1070 11.719 1.454 0.622 0. 1075 11.751 1.454 0.622 0. 1080 11.77 1.46 0.622 0. 1085 11.745 1.454 0.625 0. 1090 11.745 1.454 0.622				0.629	0.2455		0.007	
1065 11.745 1.454 0.618 0. 1070 11.719 1.454 0.622 0. 1075 11.751 1.454 0.622 0. 1080 11.77 1.46 0.622 0. 1085 11.745 1.454 0.625 0. 1090 11.745 1.454 0.622				0.625	0.245	1060	0.007	-0.002
1070 11.719 1.454 0.622 0. 1075 11.751 1.454 0.622 0. 1080 11.77 1.46 0.622 0. 1085 11.745 1.454 0.625 0. 1090 11.745 1.454 0.622				0.625	0.245		0.007	
1080 11.77 1.46 0.622 1085 11.745 1.454 0.625 1090 11.745 1.454 0.622	7 -0.07	5 11.717		0.629	0.245		0.007	
1085 11.745 1.454 0.625 1090 11.745 1.454 0.622				0.629	0.245		0.007	
1090 11.745 1.454 0.622	-0.07			0.629	0.248	1080		
	5 -0.07			0.63275	0.249		0.00775	
	5 -0.07			0.6305	0.25		0.0085 0.00925	
	5 -0.07			0.63125	0.251	1100		
1100 11.656 1.454 0.625 0.				0.635 0.63425	0.249 0.2515	1100	0.00925	
	25 -0.07 25 -0.07			0.6335	0.2515		0.00925	
1110 11.719 1.454 0.625 1115 11.745 1.46 0.628 0.				0.63575	0.2545		0.00775	
1115 11.745 1.46 0.626 0. 1120 11.719 1.46 0.628 0.				0.635	0.254	1120		
	7 -0.07 7 -0.07			0.63725	0.256	0	0.00625	
	77 -0.07 57 -0.07			0.6365	0.255		0.0055	
1135 11.751 1.466 0.634 0.				0.63875	0.254		0.00475	

Table B-3
36-Hour Constant Rate Discharge Data for MWBP-05B
(Flow Rate = 16 gpm)

(Page 7 of 10)

1						, ,			í	Pa	ckground Rea	adinge
Elapsed			т	ransducer	Readings of [Drawdown (ff)			Elapsed	Relative	Relative
Time of				Tarisducci	•	MWBP-05B	P-3(B)	P-4(A)	P-5(B)	Time		Fluctuation in
	MWBP-05B	P-3(B)	P-4(A)	P-5(B)	HFMW-05D	(corrected)		(corrected)			MWBP-09A	MWBP-09B
1140	11.681	1.46	0.634	0.26	-0.072	11.677	1.456	0.638	0.256	1140	0.004	-0.004
1145	11.719	1.46	0.637	0.257	-0.072	11.714	1.455	0.63925	0.25175 0.2535		0.00225 0.0005	-0.00525 -0.0065
1150	11.7 11.669	1.46 1.466	0.637 0.641	0.26 0.263	-0.072 -0.072	11.694 11.661	1.454 1.458	0.6375 0.63975	0.25525		-0.00125	
1155 1160	11.757	1.466	0.641	0.263	-0.072	11.748	1.457	0.638	0.254	1160	-0.003	
1165	11.713	1.466	0.641	0.263	-0.072	11.704	1.457	0.63875	0.25375		-0.00225	
1170	11.7	1.466	0.641	0.263	-0.072	11.691	1.457	0.6395	0.2535		-0.0015	
1175	11.675	1.472	0.644	0.263	-0.072	11.665	1.462	0.64325	0.25325	4400	-0.00075	-0.00975 -0.010
1180	11.916	1.491	0.647	0.266 0.269	-0.072 -0.069	11.906 11.793	1.481 1.476	0.647 0.648	0.256 0.26	1180	0.000 0.001	-0.010
1185 1190	11.802 11.834	1.485 1.479	0.647 0.647	0.269	-0.069	11.793	1.471	0.649	0.258		0.002	-0.008
1195	11.802	1.479	0.647	0.266	-0.069	11.795	1.472	0.65	0.259		0.003	-0.007
1200	11.77	1.479	0.644	0.266	-0.072	11.764	1.473	0.648	0.26	1200	0.004	-0.006
1205	11.802	1.479	0.647	0.266	-0.069	11.795	1.472	0.65	0.25925		0.003	-0.00675
1210	11.694	1.472	0.644	0.266	-0.069	11.687	1.465	0.646 0.648	0.2585 0.25775		0.002 0.001	-0.0075 -0.00825
1215 1220	11.707 11.7	1.472 1.472	0.647 0.647	0.266 0.266	-0.069 -0.069	11.699 11.691	1.464 1.463	0.647	0.25775	1220	0.000	-0.009
1225	11.726	1.472	0.65	0.269	-0.069	11.717	1.463	0.65	0.25975		0.000	-0.00925
1230	11.688	1.479	0.65	0.269	-0.066	11.679	1.470	0.65	0.2595		0.000	
1235	11.707	1.472	0.647	0.269	-0.066	11.697	1.462	0.647	0.25925		0.000	
1240	11.656	1.472	0.647	0.266	-0.066	11.646	1.462	0.647	0.256 0.25575	1240	0.000 0.000	-0.010 -0.01025
1245 1250	11.719 11.726	1.472 1.479	0.65 0.65	0.266 0.269	-0.066 -0.066	11.709 11.716	1.462 1.469	0.65 0.65	0.2585		0.000	-0.01025
1255	11.726	1.479	0.647	0.273	-0.069	11.715	1.461	0.647	0.26225		0.000	-0.01075
1260	11.77	1.479	0.65	0.273	-0.069	11.759	1.468	0.65	0.262	1260	0.000	
1265	11.713	1.479	0.653	0.273	-0.063	11.702	1.468	0.65225	0.26175		-0.00075	
1270	11.669	1.472	0.65	0.273	-0.066	11.658	1.461	0.6485	0.2615		-0.0015	
1275	11.675	1.479	0.653	0.266	-0.063	11.663 11.676	1.467 1.467	0.65075 0.647	0.25425 0.251	1280	-0.00225 -0.003	
1280 1285	11.688 11.649	1.479 1.472	0.65 0.653	0.263 0.26	-0.066 -0.066	11.637	1.460	0.65	0.24775	1200	-0.003	
1290	11.63	1.479	0.653	0.273	-0.066	11.618	1.467	0.65	0.2605		-0.003	
1295	11.688	1.479	0.653	0.269	-0.063	11.675	1.466	0.65	0.25625		-0.003	
1300	11.745	1.485	0.656	0.273	-0.06	11.732	1.472	0.653	0.26	1300	-0.003	
1305	11.726	1.479	0.656	0.273	-0.063 -0.063	11.713 11.732	1.466 1.466	0.653 0.65	0.26 0.253		-0.003 -0.003	
1310 1315	11.745 11.713	1.479 1.479	0.653 0.656	0.266 0.276	-0.063	11.732	1.466	0.653	0.263		-0.003	
1320	11.662	1.485	0.656	0.282	-0.06	11.649	1.472	0.653	0.269	1320	-0.003	
1325	11.719	1.485	0.656	0.276	-0.06	11.708	1.474	0.65375	0.26475		-0.00225	
1330	11.656	1.479	0.656	0.273	-0.06	11.647	1.470	0.6545	0.2635		-0.0015	
1335	11.719	1.485	0.656	0.273	-0.06	11.711 11.682	1.477 1.479	0.65525 0.656	0.26525 0.273	1340	-0.00075 0.000	
1340 1345	11.688 11.707	1.485 1.485	0.656 0.656	0.279 0.273	-0.056 -0.06	11.701	1.479	0.657	0.267	1540	0.001	-0.006
1350	11.713	1.479	0.656	0.273	-0.056	11.707	1.473	0.658	0.267		0.002	
1355	11.713	1.485	0.656	0.276	-0.053	11.707	1.479	0.659	0.27		0.003	
1360	11.764	1.485	0.653	0.269	-0.053	11.758	1.479	0.657	0.263	1360		
1365	11.751	1.479	0.653	0.269	-0.053	11.746	1.474	0.65775	0.264 0.269		0.00475 0.0055	
1370 1375	11.745 11.726	1.479 1.479	0.653 0.647	0.273 0.266	-0.053 -0.056	11.741 11.723	1.475 1.476	0.6585 0.65325	0.263		0.00625	
1373	11.720	1.479	0.647	0.263	-0.056	11.717	1.477	0.654	0.261	1380		
1385	11.738	1.485	0.653	0.266	-0.05	11.737	1.484	0.66075	0.26525		0.00775	
1390	11.745	1.472	0.65	0.263	-0.053	11.746	1.473	0.6585	0.2635		0.0085	
1395	11.738	1.479	0.65	0.266	-0.05	11.740	1.481	0.65925	0.26775	4400	0.00925	
1400	11.732	1.479 1.485	0.653 0.653	0.269 0.266	-0.05 -0.05	11.735 11.755	1.482 1.489	0.663 0.66225	0.272 0.2695	1400	0.01 0.00925	
1405 1410	11.751 11.764	1.485	0.653	0.263	-0.05	11.755	1.483	0.6615	0.265		0.00925	
1415	11.726	1.479	0.65	0.26	-0.05	11.731	1.484	0.65775	0.2645		0.00775	0.0045
1420	11.688	1.479	0.65	0.273	-0.047	11.693	1.484	0.657	0.278	1420		
1425	11.688	1.479	0.647	0.263	-0.047	11.694	1.485	0.65625	0.26875		0.00925	
1430	11.738	1.479	0.65	0.266	-0.047	11.745	1.486 1.486	0.6615 0.66075	0.2725 0.27625		0.0115 0.01375	
1435 1440	11.713 11.745	1.479 1.472	0.647 0.644	0.269 0.269	-0.047 -0.047	11.720 11.753	1.486	0.66075	0.27625	1440		
1440	11.745	1.472	0.647	0.269	-0.047	11.761	1.489	0.66475	0.27575		0.01775	
1450	11.707	1.466	0.644	0.257		11.719	1.478		0.2685		0.0195	0.0115

Table B-3 36-Hour Constant Rate Discharge Data for MWBP-05B (Flow Rate = 16 gpm)

(Page 8 of 10)

							•		1	Ra	ckground Rea	ndinas
Elapsed			т	ransducer	Readings of	Drawdown (ft)			Elapsed	Relative	Relative
Time of						MWBP-05B	P-3(B)	P-4(A)	P-5(B)	Time		Fluctuation in
	MWBP-05B	P-3(B)	P-4(A)	P-5(B)	HFMW-05D	(corrected)		(corrected)		(minutes)		MWBP-09B
1455		1.466	0.644	0.266	-0.047 -0.044	11.764 11.722	1.479 1.487	0.66525 0.667	0.27925 0.288	1460	0.02125 0.023	0.01325 0.015
1460 1465		1.472 1.466	0.644 0.641	0.273 0.26	-0.044	11.722	1.484	0.66625	0.2775	1400	0.02525	0.0175
1470		1.472	0.644	0.257	-0.041	11.733	1.492	0.6715	0.277		0.0275	0.02
1475		1.472	0.637	0.266	-0.044	11.761	1.495	0.66675	0.2885		0.02975	0.0225
1480		1.466	0.631	0.247	-0.041	11.808	1.491	0.663	0.272	1480	0.032	0.025
1485		1.46	0.631	0.257	-0.041	11.726	1.486	0.6655	0.283		0.0345	0.026
1490		1.454	0.625	0.241	-0.044	11.816	1.481	0.662	0.268		0.037	0.027
1495		1.46	0.622	0.238	-0.041	12.018	1.740 1.476	0.6615 0.664	0.518 0.273	1500	0.0395 0.042	0.280 0.029
1500 1505		1.447 1.454	0.622 0.618	0.244 0.231	-0.044 -0.044	11.748 11.776	1.485	0.66075	0.262	1300	0.04275	0.023
1510		1.454	0.622	0.241	-0.037	11.778	1.487	0.6655	0.274		0.0435	0.033
1515		1.447	0.622	0.238	-0.037	11.710	1.482	0.66625	0.273		0.04425	0.035
1520		1.454	0.625	0.241	-0.034	11.769	1.491	0.67	0.278	1520	0.045	0.037
1525		1.46	0.625	0.244	-0.034	11.852	1.498	0.6715	0.282		0.0465	0.038
1530		1.447	0.625	0.244	-0.034	11.777	1.486	0.673	0.283		0.048 0.0495	0.039 0.040
1535 1540		1.454 1.454	0.622 0.622	0.241 0.234	-0.031 -0.031	11.766 11.779	1.494 1.495	0.6715 0.673	0.281 0.275	1540	0.0493	0.041
1540		1.454	0.622	0.234	-0.028	11.774	1.496	0.673	0.2825	1010	0.051	0.0415
1550		1.441	0.615	0.225	-0.034	11.780	1.483	0.666	0.267		0.051	0.0420
1555		1.454	0.622	0.234	-0.025	11.800	1.497	0.673	0.2765		0.051	0.0425
1560		1.46	0.622	0.234	-0.022	11.826	1.503	0.673	0.277	1560	0.051	0.043
1565		1.454	0.622	0.234	-0.025	11.800	1.497	0.673 0.669	0.27675 0.2765		0.051 0.051	0.04275 0.04250
1570		1.454 1.46	0.618 0.625	0.234 0.244	-0.022 -0.018	11.794 11.761	1.497 1.502	0.676	0.28625		0.051	0.04235
1575 1580		1.447	0.623	0.238	-0.018	11.799	1.489	0.673	0.20023	1580	0.051	0.042
1585		1.454	0.625	0.238	-0.015	11.768	1.496	0.676	0.28		0.051	0.042
1590		1.46	0.631	0.247	-0.012	11.806	1.502	0.682	0.289		0.051	0.042
1595			0.618	0.222	-0.025	11.711	1.489	0.669	0.264		0.051	0.042
1600		1.447	0.615	0.222	-0.018	11.761	1.489	0.666	0.264	1600	0.051 0.05175	0.042 0.04275
1605		1.454	0.618 0.628	0.228 0.244	-0.012 -0.003	11.762 11.839	1.497 1.510	0.66975 0.6805	0.27075 0.2875		0.05175	0.04275
1610 1615		1.466 1.46	0.625	0.244	-0.003	11.827	1.504	0.67825	0.28825		0.05325	0.04425
1620		1.46	0.628	0.241	0.000	11.739	1.505	0.682	0.286	1620	0.054	0.045
1625		1.454	0.625	0.238	0	11.820	1.498	0.67825	0.282		0.05325	0.044
1630		1.46	0.628	0.241	0	11.832	1.503	0.6805	0.284		0.05250	0.043
1635		1.46	0.634	0.244	0.006	11.806	1.502	0.68575	0.286	4040	0.05175	0.042
1640		1.466	0.628	0.238	0.009	11.817	1.507	0.679 0.679	0.279 0.285	1640	0.051 0.051	0.041 0.041
1645 1650		1.46 1.466	0.628 0.634	0.244 0.247	0.006 0.015	11.817 11.817	1.501 1.507	0.685	0.288		0.051	0.041
1655		1.46	0.631	0.241	0.009	11.773	1.501	0.682	0.282		0.051	0.041
1660		1.472	0.637	0.25		11.798	1.513	0.688	0.291	1660	0.051	0.041
1665	11.814	1.466	0.637	0.25	0.022	11.854	1.506	0.68725	0.29025		0.05025	0.04025
1670		1.466	0.634	0.244	0.022	11.766	1.506	0.6835	0.2835		0.0495	0.0395
1675		1.466	0.634	0.241	0.025 0.028	11.784 11.795	1.505 1.504	0.68275 0.685	0.27975 0.282	1680	0.04875 0.048	0.03875 0.038
1680 1685		1.466 1.466	0.637 0.637	0.244 0.247	0.028	11.821	1.504	0.685	0.285	1000	0.048	0.038
1690		1.472	0.637	0.244	0.034	11.827	1.510	0.685	0.282		0.048	0.038
1695		1.472	0.641	0.241	0.037	11.846	1.510	0.689	0.279		0.048	0.038
1700	11.834	1.472	0.641	0.241	0.037	11.872	1.510	0.689	0.279	1700	0.048	0.038
1705		1.472	0.637	0.244	0.037	11.846	1.510	0.685	0.282		0.048	0.038
1710		1.472	0.637	0.244	0.044	11.833	1.510	0.685	0.282		0.048 0.048	0.038 0.038
1715 1720		1.472 1.472	0.637 0.641	0.241 0.247	0.047 0.05	11.808 11.808	1.510 1.510	0.685 0.689	0.279 0.285	1720		0.038
1720		1.472	0.644	0.247	0.053	11.845	1.516	0.6905	0.2935	1720	0.0465	0.0365
1730		1.472	0.644	0.257	0.056	11.799	1.507	0.689	0.292		0.045	0.035
1735		1.479	0.647	0.26	0.063	11.791	1.513	0.6905	0.2935		0.0435	0.0335
1740		1.479	0.647	0.26	0.063	11.808	1.511	0.689	0.292	1740		0.032
1745		1.479	0.641	0.257	0.063	11.820	1.510	0.682	0.288		0.041	0.031
1750		1.479	0.65	0.263	0.066	11.876	1.509	0.69 0.689	0.293 0.286		0.040 0.039	0.030 0.029
1755 1760		1.479 1.479	0.65 0.65	0.257 0.26	0.072 0.075	11.843 11.798	1.508 1.507	0.689	0.288	1760		0.029
1765		1.479	0.65	0.26	0.075	11.803	1.506	0.6865	0.2865		0.0365	
50			0.00	1.20								

Table B-3 36-Hour Constant Rate Discharge Data for MWBP-05B (Flow Rate = 16 gpm)

(Page 9 of 10)

1-1						(-S	,			Ra	ckground Rea	adinas
Elapsed			т	ransducer	Readings of I	Drawdown (ft)			Elapsed	Relative	Relative
Time of			•	i al isoucci	readings of t	MWBP-05B	P-3(B)	P-4(A)	P-5(B)	Time		Fluctuation in
	MWBP-05B	P-3(B)	P-4(A)	P-5(B)	HFMW-05D			(corrected)			MWBP-09A	MWBP-09B
1770	11.732	1.479	0.653	0.26	0.082	11.757	1.504	0.688	0.285		0.035	0.025
1775	11.713	1.485	0.653	0.263		11.737	1.509	0.6865	0.2865		0.0335	0.0235
1780	11.783	1.485	0.656	0.266	0.088	11.805		0.688	0.288	1780	0.032	0.022
1785	11.789	1.485	0.653	0.26	0.091	11.811	1.507	0.685	0.282		0.032	0.022
1790	11.713	1.479	0.656	0.266	0.094	11.735		0.688	0.288		0.032	0.022
1795	11.776	1.479	0.653	0.266	0.094	11.798		0.685	0.288		0.032	0.022
1800	11.656	1.479	0.656	0.266	0.101	11.678		0.688	0.288	1800	0.032	0.022
1805	11.77	1.485	0.659	0.269	0.104	11.792		0.691	0.291		0.032	0.022
1810	11.738	1.485	0.659	0.269	0.107	11.760		0.691	0.291		0.032 0.032	0.022 0.022
1815	11.757	1.485	0.659	0.273 0.269	0.11 0.11	11.779 11.817	1.507 1.513	0.691 0.691	0.295 0.291	1820	0.032	0.022
1820 1825	11.795 11.764	1.491 1.491	0.659 0.659	0.269	0.117	11.786		0.6895	0.29075	1020	0.0305	0.02175
1830	11.754	1.491	0.663	0.203	0.117	11.773	1.513	0.692	0.2945		0.029	0.0215
1835	11.719	1.491	0.663	0.279	0.12	11.740		0.6905	0.30025		0.0275	0.02125
1840	11.764	1.491	0.666	0.276	0.126	11.785	1.512	0.692	0.297	1840	0.026	0.021
1845	11.764	1.491	0.666	0.276	0.129	11.784	1.511	0.69125	0.29575		0.02525	0.01975
1850	11.745	1.491	0.669	0.279	0.132	11.764	1.510	0.6935	0.2975		0.0245	0.0185
1855	11.745	1.498	0.669	0.279	0.136	11.762		0.69275	0.29625		0.02375	0.01725
1860	11.783	1.498	0.672	0.282	0.139	11.799	1.514	0.695	0.298	1860	0.023	0.016
1865	11.783	1.498	0.675	0.285	0.142	11.798		0.69625	0.3		0.02125	0.015
1870	11.776	1.504	0.678	0.288	0.145	11.790	1.518	0.6975	0.302		0.0195	0.014
1875	11.77	1.51	0.678	0.288	0.148	11.783	1.523	0.69575	0.301	1880	0.01775 0.016	0.013 0.012
1880	11.814	1.51	0.682	0.288	0.155	11.826		0.698 0.69875	0.3 0.30225	1000	0.01375	0.012
1885	11.802 11.846	1.51 1.517	0.685 0.688	0.292 0.295	0.158 0.161	11.812 11.855		0.6995	0.30225		0.01375	0.0085
1890 1895	11.776	1.517	0.688	0.298	0.164	11.783	1.517	0.69725	0.30475		0.00925	0.00675
1900	11.834	1.517	0.691	0.298	0.17	11.839	1.522	0.698	0.303	1900	0.007	0.005
1905	11.84	1.523	0.694	0.301	0.174	11.845		0.701	0.3055		0.007	0.0045
1910	11.795 ;	1.517	0.694	0.301	0.177	11.799	1.521	0.701	0.305		0.007	0.0040
1915	11.865	1.523	0.694	0.301	0.18	11.869	1.527	0.701	0.3045		0.007	0.0035
1920	11.814	1.517	0.694	0.301	0.183	11.817	1.520	0.701	0.304	1920	0.007	0.003
1925	11.776	1.517	0.694	0.301	0.186	11.777	1.518	0.70025	0.30175		0.00625	0.00075
1930	11.821	1.517	0.694	0.301	0.189	11.820		0.6995	0.2995		0.0055	-0.0015
1935	11.808	1.517	0.694	0.304	0.193	11.804	1.513	0.69875	0.30025		0.00475	-0.00375
1940	11.776	1.517	0.697	0.304	0.196	11.770	1.511	0.701	0.298	1940	0.004	-0.006
1945	11.84	1.517	0.697	0.304	0.199 0.205	11.834 11.745	1.511 1.511	0.7 0.699	0.298 0.298		0.003 0.002	-0.006 -0.006
1950 1955	11.751 11.808	1.517 1.523	0.697 0.697	0.304 0.308	0.205	11.745		0.698	0.302		0.002	-0.006
1960	11.808	1.523	0.697	0.304	0.208	11.802		0.697	0.298	1960	0.000	-0.006
1965	11.859	1.529	0.701	0.308	0.208	11.852		0.701	0.301		0.000	-0.007
1970	11.859	1.523	0.701	0.308	0.212	11.851	1.515	0.701	0.3		0.000	-0.008
1975	11.834	1.523	0.701	0.308		11.825	1.514	0.701	0.299		0.000	-0.009
1980		1.523	0.701	0.308	0.215	11.760	1.513	0.701	0.298	1980	0.000	-0.010
1985	11.821	1.523	0.701	0.308		11.810		0.70025	0.29725		-0.00075	-0.01075
1990	11.77	1.523	0.701	0.311	0.221	11.759		0.6995	0.2995		-0.0015	-0.0115
1995	11.795	1.523	0.704	0.311	0.221	11.783		0.70175	0.29875		-0.00225	-0.01225
2000		1.529	0.704	0.311	0.224	11.840		0.701	0.298	2000	-0.003 -0.003	-0.013 -0.013
2005	11.846	1.523	0.704	0.311	0.224	11.833		0.701 0.701	0.298 0.298		-0.003	-0.013
2010	11.865	1.529 1.523	0.704 0.704	0.311 0.311	0.227 0.227	11.852 11.814		0.701	0.298		-0.003	-0.013
2015 2020	11.827 11.789	1.523	0.704	0.311	0.227	11.776		0.701	0.298	2020	-0.003	-0.013
2025	11.783	1.523	0.704	0.311	0.227	11.771	1.511	0.70175	0.29925	2020	-0.00225	-0.01175
2030	11.834	1.517	0.701	0.308	0.231	11.824		0.6995	0.2975		-0.0015	-0.0105
2035	11.827	1.523	0.701	0.311	0.234	11.818		0.70025	0.30175		-0.00075	-0.00925
2040		1.517	0.701	0.308		11.813		0.701	0.3	2040		-0.008
2045	11.776	1.523	0.701	0.308	0.234	11.770		0.70275	0.3015		0.00175	-0.0065
2050	11.821	1.517	0.697	0.304	0.234	11.816		0.7005	0.299		0.0035	-0.005
2055	11.808	1.517	0.697	0.304	0.237	11.805		0.70225	0.3005		0.00525	-0.0035
2060	11.751	1.51	0.694	0.301	0.234	11.749		0.701	0.299	2060		-0.002
2065	11.789	1.51	0.691	0.298		11.789		0.70025	0.298		0.00925	0
2070	11.77	1.51	0.691	0.298		11.772		0.7025	0.3		0.0115	0.002
2075	11.789	1.504	0.688	0.295		11.793		0.70175	0.299	2080	0.01375 0.016	0.004 0.006
2080	11.783	1.51	0.688	0.295	0.237	11.789	1.516	0.704	0.301	2000	0.016	0.006

Table B-3
36-Hour Constant Rate Discharge Data for MWBP-05B
(Flow Rate = 16 gpm)

(Page 10 of 10)

											Ba	ckground Rea	adings
	Elapsed			Т	ransducer	Readings of I	Drawdown (ft)			Elapsed	Relative	Relative
	Time of						MWBP-05B	P-3(B)	P-4(A)	P-5(B)	Time	Fluctuation in	Fluctuation in
		MWBP-05B	P-3(B)	P-4(A)	P-5(B)	HFMW-05D	(corrected)	(corrected)	(corrected)	(corrected)	(minutes)	MWBP-09A	MWBP-09B
•	2085		1.504	0.688	0.292	0.234	11.840	1.510	0.704	0.298		0.016	0.006
	2090		1.504	0.685	0.292	0.234	11.801	1.510	0.701	0.298		0.016	
	2095	11.827	1.504	0.685	0.292	0.231	11.833	1.510	0.701	0.298		0.016	
	2100	11.764	1.498	0.685	0.292	0.231	11.770	1.504	0.701	0.298	2100	0.016	
	2105	11.802	1.504	0.688	0.295	0.231	11.810	1.512	0.70475	0.303		0.01675	
	2110	11.834	1.504	0.688	0.292	0.231	11.844	1.514	0.7055	0.302		0.0175	
	2115	11.827	1.504	0.685	0.292	0.227	11.839	1.516	0.70325	0.304		0.01825	0.012
	2120	11.77	1.498	0.685	0.288	0.224	11.784	1.512	0.704	0.302	2120	0.019	0.014
	2125	11.726	1.498	0.682	0.288	0.224	11.741	1.513	0.70275	0.303		0.02075	
	2130		1.498	0.682	0.285	0.221	11.761	1.514	0.7045	0.301		0.0225	0.016
	2135	11.808	1.498	0.682	0.288	0.221	11.825	1.515	0.70625	0.305		0.02425	0.017
	2140	11.783	1.498	0.682	0.285	0.218	11.801	1.516	0.708	0.303	2140	0.026	0.018
	2145	11.764	1.498	0.682	0.285	0.218	11.783	1.517	0.70875	0.30375		0.02675	
	2150	11.776	1.498	0.682	0.282	0.215	11.796	1.518	0.7095	0.3015		0.0275	0.0195
	2155		1.498	0.678	0.282	0.212	11.841	1.518	0.70625	0.30225		0.02825	
	2160	11.814	1.498	0.678	0.285	0.212	11.835	1.519	0.707	0.306	2160	0.029	0.021

Table B-4
Recovery Data for 36-Hour Constant Rate Discharge Test in MWBP-05B

(Page 1 of 4)

Elapsed	Total Test		Drawdown I	Measureme	nts (feet)	
Time	Time	MWBP-05B	P-3(B)	P-4(A)	P-5(B)	HFMW-05D
(minute)	(minute)	LECTED PUM				111 10100 000
0.1	0.1	5.209	0.284	0.003	0.022	0
1	1	9.212	0.897	0.022	0.066	0
10	10	10.259	1.131	0.186	0.085	-0.012
100	100	11.415	1.277	0.356	0.107	-0.028
1000	1000	11.688	1.435	0.596	0.228	-0.063
2000	2000	11.853	1.529	0.704	0.311	0.224
2100	2100	11.764	1.498	0.685	0.292	0.231
2120	2120	11.77	1.498	0.685	0.288	0.224
2140	2140	11.783	1.498	0.682	0.285	0.218
2160	2160	11.814	1.498	0.678	0.285	0.212
			OVERY DA			
0.0083	2160.008	11.237	1.498	0.678	0.282	0.208
0.0166	2160.017	11.104	1.491	0.678	0.282	0.208
0.025	2160.025	10.958	1.491	0.678	0.285	0.205
0.0333	2160.033	10.818	1.491	0.678	0.285	0.208
0.0416	2160.042	10.691	1.491	0.678	0.282	0.205
0.05	2160.05	10.564	1.485	0.678	0.285	0.208
0.0583	2160.058	10.412	1.479	0.678	0.285	0.208
0.0666	2160.067	10.298	1.479	0.678	0.282	0.208
0.075	2160.075	10.158	1.472	0.678	0.282	0.205
0.0833	2160.083	10.037	1.472	0.675	0.282	0.208
0.0916	2160.092	9.917	1.466	0.678	0.285	0.208
0.1	2160.1	9.783	1.46	0.678	0.279	0.208
0.1083	2160.108	9.656	1.46	0.678	0.285	0.208
0.1166	2160.117	9.536	1.454	0.675	0.285	0.212
0.125	2160.125	9.415	1.447	0.678	0.285	0.212
0.1333	2160.133	9.294	1.441	0.678	0.282	0.212
0.1416	2160.142	9.18	1.435	0.678	0.282	0.212
0.15	2160.15	9.059	1.428	0.678	0.285	0.212
0.1583	2160.158	8.951	1.422	0.678	0.285	0.212
0.1666	2160.167	8.837	1.416	0.678	0.285	0.212
0.175	2160.175	8.723	1.409	0.678	0.288	0.208
0.1833	2160.183	8.615	1.403	0.678	0.285	0.208 0.208
0.1916	2160.192	8.507	1.397	0.678	0.285	0.208
0.2	2160.2	8.399	1.384	0.675	0.282	
0.2083	2160.208	8.291	1.378	0.678	0.285 0.285	0.208
0.2166	2160.217	8.183	1.371	0.678	0.285	0.208
0.225	2160.225	8.081 7.98	1.365 1.359	0.678 0.675	0.283	0.212
0.2333	2160.233	7.878	1.339	0.678	0.282	0.212
0.2416 0.25	2160.242 2160.25	7.776	1.340	0.678	0.282	0.212
	2160.25	7.776	1.333	0.678	0.282	
0.2583 0.2666	2160.256	7.586	1.333	0.675	0.232	
0.2666	2160.267	7.565	1.314	0.675	0.279	0.212
0.275	2160.275	7.491	1.308	0.678	0.282	
0.2033	2160.203	7.393	1.302	0.675	0.282	
0.2910	2100.202	7.500	1,002	0.070	0.202	

Table B-4
Recovery Data for 36-Hour Constant Rate Discharge Test in MWBP-05B

(Page 2 of 4)

Elapsed	Total Test	1	Drawdown I	Measureme	nts (feet)	
Time (minute)	Time (minute)	MWBP-05B	P-3(B)	P-4(A)	P-5(B)	HFMW-05D
0.3	2160.3	7.211	1.296	0.678	0.285	0.212
0.3083	2160.308	7.116	1.283	0.675	0.282	0.212
0.3166	2160.317	7.027	1.277	0.675	0.282	0.208
0.325	2160.325	6.944	1.27	0.675	0.282	0.208
0.3333	2160.333	6.855	1.264	0.675	0.282	0.208
0.35	2160.35	6.684	1.245	0.675	0.279	0.205
0.3666	2160.367	6.518	1.232	0.675	0.282	0.208
0.3833	2160.383	6.353	1.213	0.675	0.282	0.208
0.4	2160.4	6.194	1.201	0.675	0.282	0.208
0.4166	2160.417	6.042	1.182	0.675	0.279	0.208
0.4333	2160.433	5.889	1.169	0.675	0.279	0.208
0.45	2160.45	5.743	1.156	0.675	0.279	0.208
0.4666	2160.467	5.603	1.137	0.672	0.279	0.208
0.4833	2160.483	5.463	1.119	0.672	0.276	0.208
0.5	2160.5	5.324	1.106	0.672	0.276	0.208
0.5166	2160.517	5.19	1.093	0.672	0.276	0.208
0.5333	2160.533	5.069	1.081	0.672	0.276	0.208
0.55	2160.55	4.942	1.062	0.672	0.276	0.205
0.5666	2160.567	4.815	1.049	0.672	0.276	0.205
0.5833	2160.583	4.701	1.036	0.669	0.273	0.205
0.6	2160.6	4.586	1.017	0.669	0.276	0.205
0.6166	2160.617	4.465	1.005	0.669	0.273	0.205
0.6333	2160.633	4.364	0.992	0.669	0.273	0.208
0.65	2160.65	4.256	0.979	0.669	0.273	0.205
0.6666	2160.667	4.147	0.967	0.666	0.269	0.205
0.6833	2160.683	4.046	0.954	0.666	0.269	0.205
0.7	2160.7	3.95	0.942	0.666	0.269	0.205
0.7166	2160.717	3.855	0.929	0.666	0.269	0.205
0.7333	2160.733	3.76	0.916	0.663	0.269	0.205
0.75	2160.75	3.671	0.904	0.666	0.266	0.208
0.7666	2160.767	3.582	0.891	0.663	0.266	0.208
0.7833	2160.783	3.492	0.878	0.663	0.266	0.205
0.8	2160.8	3.41	0.866	0.663	0.266	0.208
0.8166	2160.817	3.327	0.859	0.659	0.263	0.208
0.8333	2160.833	3.244	0.847	0.659	0.26	0.205
0.85	2160.85	3.168	0.834	0.659	0.263	0.205
0.8666	2160.867	3.092	0.821	0.659	0.26	0.205
0.8833	2160.883	3.022	0.815	0.656	0.257	0.205
0.9	2160.9	2.946	0.802	0.656	0.26	0.205
0.9166	2160.917	2.882	0.79	0.656	0.26	0.205
0.9333	2160.933	2.812	0.783	0.656	0.257	0.208
0.95	2160.95	2.742	0.771	0.656	0.257	0.205
0.9666	2160.967	2.678	0.765	0.653	0.254	0.205
0.9833	2160.983	2.615	0.752	0.653	0.25	0.205
1	2161	2.558	0.746	0.653	0.254	0.208
1.2	2161.2	1.934	0.644	0.641	0.241	0.205
1.4	2161.4	1.495	0.569	0.631	0.231	0.208

Table B-4
Recovery Data for 36-Hour Constant Rate Discharge Test in MWBP-05B

(Page 3 of 4)

Time (minute) Time (minute) MWBP-05B P-3(B) P-4(A) P-5(B) HFMW-05D 1.6 2161.6 1.171 0.505 0.618 0.222 0.205 1.8 2161.8 0.941 0.461 0.606 0.209 0.205 2 2162 0.776 0.423 0.593 0.2 0.205 2.2 2162.2 0.655 0.392 0.584 0.196 0.205 2.4 2162.6 0.502 0.354 0.562 0.177 0.205 2.8 2162.8 0.458 0.341 0.552 0.18 0.205 3.2 2163.2 0.394 0.322 0.536 0.165 0.205 3.4 2163.4 0.369 0.316 0.527 0.165 0.205 3.4 2163.6 0.362 0.309 0.521 0.161 0.205 3.8 2163.6 0.362 0.309 0.524 0.161 0.205 3.8 2163.6
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8 2168 0.299 0.278 0.438 0.133 0.205 8.2 2168.2 0.299 0.278 0.438 0.139 0.205 8.4 2168.4 0.299 0.278 0.435 0.133 0.205
8.2 2168.2 0.299 0.278 0.438 0.139 0.205 8.4 2168.4 0.299 0.278 0.435 0.133 0.205
8.4 2168.4 0.299 0.278 0.435 0.133 0.205
8.6 2168.6 0.299 0.278 0.435 0.139 0.205
8.8 2168.8 0.292 0.271 0.435 0.139 0.205
9 2169 0.299 0.271 0.432 0.139 0.202
9.2 2169.2 0.292 0.271 0.429 0.133 0.202
9.4 2169.4 0.292 0.271 0.429 0.139 0.205
9.6 2169.6 0.292 0.271 0.429 0.136 0.202
9.8 2169.8 0.292 0.271 0.426 0.13 0.202
10 2170 0.292 0.271 0.426 0.117 0.205
12 2172 0.286 0.265 0.416 0.13 0.2 02
14 2174 0.28 0.265 0.407 0.127 0.202
16 2176 0.28 0.259 0.401 0.127 0.199
18 2178 0.273 0.252 0.397 0.12 0.202

BP5BQ36R.XLS: Sheet1(11/15/96)sai

Table B-4
Recovery Data for 36-Hour Constant Rate Discharge Test in MWBP-05B

(Page 4 of 4)

Elapsed	Total Test		Drawdown N	Measureme	rements (feet)			
Time (minute)	Time (minute)	MWBP-05B	P-3(B)	P-4(A)	P-5(B)	HFMW-05D		
20	2180	0.267	0.252	0.391	0.117	0.199		
22	2182	0.267	0.246	0.385	0.117	0.196		
24	2184	0.267	0.246	0.382	0.114	0.196		
26	2186	0.26	0.246	0.378	0.114	0.196		
28	2188	0.26	0.246	0.375	0.114	0.196		
30	2190	0.26	0.24	0.372	0.114	0.193		
32	2192	0.254	0.24	0.369	0.111	0.189		
34	2194	0.254	0.24	0.366	0.111	0.193		
36	2196	0.254	0.233	0.363	0.107	0.189		
38	2198	0.248	0.233	0.36	0.104	0.189		
40	2200	0.248	0.227	0.356	0.104	0.189		
42	2202	0.248	0.227	0.353	0.104	0.186		
44	2204	0.241	0.227	0.35	0.104	0.186		
46	2206	0.241	0.227	0.35	0.098	0.183		
48	2208	0.241	0.227	0.347	0.101	0.183		
50	2210	0.241	0.221	0.344	0.101	0.183		
52	2212	0.241	0.221	0.344	0.101	0.183		
54	2214	0.235	0.221	0.341	0.101	0.18		
56	2216	0.235	0.214	0.337	0.095	0.18		
58	2218	0.229	0.214	0.334	0.095	0.177		
60	2220	0.229	0.214	0.334	0.095	0.177		
÷ 62	2222	0.229	0.214	0.331	0.095	0.177		
64	2224	0.229	0.208	0.331	0.092	0.174		
66	2226	0.229	0.208	0.328	0.092	0.174		
68	2228	0.222	0.208	0.325	0.092	0.17		
70	2230	0.222	0.208	0.325	0.088	0.17		
72	2232	0.222	0.202	0.322	0.092	0.17		
74	2234	0.222	0.202	0.322	0.088	0.17		
76	2236	0.216	0.202	0.318	0.088	0.167		
78	2238	0.216	0.202	0.315	0.085	0.164		
80	2240	0.216	0.202	0.312	0.082	0.164		
82	2242	0.21	0.196	0.309	0.082	0.161		
84	2244	0.21	0.196	0.309	0.082	0.161		
86	2246	0.21	0.196	0.306	0.082	0.161		
88	2248	0.21	0.196	0.306	0.079	0.161		
90	2250	0.21	0.189	0.303	0.082	0.158		
92	2252	0.203	0.189	0.303	0.079	0.158		
94	2254	0.203	0.189	0.3	0.076	0.155		
96	2256	0.203	0.189	0.3	0.076	0.155		
98	2258	0.203	0.189	0.3	0.076	0.155		
100	2260	0.203	0.189	0.296	0.076	0.151		
105	2265	0.197	0.183	0.293	0.073	0.148		
110	2270	0.197	0.183	0.293	0.076	0.145		
115	2275	0.197	0.183	0.29	0.076	0.142		
120	2280	0.19	0.177	0.287	0.069	0.139		

Table B-5
Water Level Measurements in MWBP-05(A) During 36-Hour Test in MWBP-05B

(Page 1 of 2)

			(1 ago 1 o. z)				
Initial Depth to	Water	80.48 1	ft	Back	ground Read	ings	
				Relative		Absolute	
			Corrected	MWBP-09A		MWBP-09A	
Elapsed Time	Depth to	Drawdown	Drawdown	Xd Reading	Test Elapsed	Xd Reading	
(min)	Water (ft)	(ft)	(ft)	(ft)	Time (min)	(ft)	
0	80.44	-0.04	-0.04	0.000	1	0.124	
65	80.53	0.05	0.069	0.019	60	0.143	
95	80.53	0.05	0.079	0.029	100	0.153	
125	80.54	0.06	0.092	0.032	120	0.156	
155	80.55	0.07	0.108	0.038	160	0.162	
185	80.56	0.08	0.122	0.042	180	0.166	
215	80.57	0.09	0.132	0.042	220	0.166	
245	80.58	0.1	0.142	0.042	240	0.166	
275	80.6	0.12	0.158	0.038	280	0.162	
305	80.61	0.13	0.165	0.035	300	0.159	
335	80.62	0.14	0.169	0.029	340	0.153	
365	80.64	0.16	0.186	0.026	360	0.150	
395	80.65	0.17	0.186	0.016	400	0.140	
425	80.67	0.19	0.203	0.013	420	0.137	
455	80.68	0.2	0.207	0.007	460	0.131	
485	80.68	0.2	0.204	0.004	480	0.128	
515	80.7	0.22	0.220	0.000	520	0.124	
545	80.71	0.23	0.227	-0.003	540	0.121	
575	80.71	0.23	0.227	-0.003	580	0.121	
÷ 605	80.71	0.23	0.234	0.004	600	0.128	
635	80.71	0.23	0.234	0.004	640	0.128	
665	80.72	0.24	0.240	0.000	660	0.124	
695	80.73	0.25	0.250	0.000	700	0.124	
725	80.73	0.25	0.247	-0.003	720	0.121	
755	80.74	0.26	0.257	-0.003	760	0.121	
785	80.74	0.26	0.257	-0.003	780	0.121	
815	80.76	0.28	0.277	-0.003	820	0.121	
845	80.75	0.27	0.274	0.004	840	0.128	
875	80.75	0.27	0.286	0.016	880	0.140	
905	80.75	0.27	0.283	0.013	900	0.137	
935	80.74	0.26	0.276	0.016	940	0.140	
965	80.74	0.26	0.279	0.019	960	0.143	
995	80.74	0.26	0.283	0.023	1000	0.147	
1025	80.75	0.27	0.286	0.016	1020	0.140	
1055	80.76	0.28	0.287	0.007	1060	0.131	
1085	80.78	0.3	0.307	0.007	1080	0.131	
1115	80.78	0.3	0.307	0.007	1120	0.131	
1145	80.77	0.29	0.294	0.004	1140	0.128	
1175	80.78	0.3	0.300	0.000	1180	0.124	
1205	80.77	0.29	0.294	0.004	1200	0.128	
1235	80.78	0.3	0.300	0.000	1240	0.124	
1265	80.78	0.3	0.300	0.000	1260	0.124	
1295	80.78	0.3	0.297	-0.003	1300	0.121	
1325	80.78	0.3	0.297	-0.003	1320	0.121	

Table B-5
Water Level Measurements in MWBP-05(A) During 36-Hour Test in MWBP-05B

(Page 2 of 2)

1. 20 of Broads 4 of	18/-4	00.40.4	(, Lgc L c, L _j	Background Readings				
Initial Depth to	vvater	80.48 f	ι	Relative	ground Read	Absolute		
			Corrected	MWBP-09A		MWBP-09A		
Clansed Time	Donth to	Droudown	Drawdown	Xd Reading	Test Elapsed			
Elapsed Time (min)	Depth to Water (ft)	Drawdown (ft)	(ft)	(ft)	Time (min)	(ft)		
1355	80.78	0.3	0.304	0.004	1360	0.128		
1385	80.78	0.3	0.307	0.007	1380	0.123		
1415	80.78	0.3	0.307	0.007	1420	0.131		
1445	80.77	0.29	0.306	0.007	1440	0.140		
1475	80.76	0.28	0.312	0.032	1480	0.156		
1505	80.75	0.27	0.312	0.042	1500	0.166		
1535	80.75	0.27	0.321	0.051	1540	0.175		
1565	80.76	0.28	0.331	0.051	1560	0.175		
1595	80.76	0.28	0.331	0.051	1600	0.175		
1625	80.76	0.28	0.334	0.054	1620	0.178		
1655	80.77	0.29	0.341	0.051	1660	0.175		
1685	80.78	0.3	0.348	0.048	1680	0.172		
1715	80.78	0.3	0.348	0.048	1720	0.172		
1745	80.79	0.31	0.352	0.042	1740	0.166		
1775	80.81	0.33	0.362	0.032	1780	0.156		
1805	80.81	0.33	0.362	0.032	1800	0.156		
1835	80.83	0.35	0.376	0.026	1840	0.150		
1865	80.84	0.36	0.383	0.023	1860	0.147		
1895	80.85	0.37	0.377	0.007	1900	0.131		
⁺ 1925	80.85	0.37	0.377	0.007	1920	0.131		
1955	80.85	0.37	0.370	0.000	1960	0.124		
1985	80.87	0.39	0.390	0.000	1980	0.124		
2015	80.87	0.39	0.387	-0.003	2020	0.121		
2045	80.87	0.39	0.390	0.000	2040	0.124		
2075	80.85	0.37	0.386	0.016	2080	0.140		
2105	80.84	0.36	0.376	0.016	2100	0.140		
2135	80.84	0.36	0.386	0.026	2140	0.150		
2160	80.83	0.35	0.379	0.029	2160	0.153		
Recovery Data								
2162	80.81	0.33						
2165	80.8							
2167	80.79	0.31						
2169	80.78							
2170	80.77	0.29						
2173	80.76	0.28						
2176	80.75	0.27			2490	0.156		
2179	80.74	0.26			2180	0.156		
2187	80.73	0.25			2200	0.153		
2202	80.72				2200	0.153		
2209	80.71	0.23			2220	0.156		
2220	80.7	0.22		1	2220	0.130		

Table B-6
Water Level Measurements in MWBP-05C During 36-Hour Test in MWBP-05B

Initial Depth to	Water .	80.75 ft		d Fluctuations VBP-09B Relative
Elapsed Time	Depth to	Fluctuation		Change from
(min)	Water (ft)	(ft)		Time 0 (ft)
5	80.72	-0.03	5	0.001
65	80.72	-0.03	65	0.01
125	80.71	-0.04	125	0.0285
185	80.70	-0.05	185	0.0365
245	80.69	-0.06	245	0.0405
305	80.70	-0.05	305	0.0325
365	80.71	-0.04	365	0.01975
425	80.74	-0.01	425	0.0145
485	80.73	-0.02	485	0.00425
545	80.76	0.01	545	-0.00425
605	80.76	0.01	605	-0.00425
665	80.76	0.01	665	-0.00675
725	80.77	0.02	725	-0.01175
785	80.77	0.02	785	-0.0135
845	80.77	0.02	845	-0.005
905	80.77	0.02	905	0.00525
965	80.75	0	965	0.01075
1025	80.75	0	1025	0.00675
, 1085	80.76	0.01	1085	-0.001
1145	80.75	0	1145	-0.00525
1205	80.76	0.01	1205	-0.00675
1265	80.74	-0.01	1265	-0.01125
1325	80.74	-0.01	1325	-0.01125
1385	80.74	-0.01	1385	-0.00075
1445	80.74	-0.01	1445	0.00975
1505	80.72	-0.03	1505	0.031
1565	80.72	-0.03	1565	0.04275
1625	80.72	-0.03	1625	0.044
1685	80.74	-0.01	1685	0.038
1745	80.75	0	1745	0.031
1805	80.77	0.02	1805	0.022
1865	80.81	0.06	1865	0.015
1925	80.82	0.07	1925	0.00075
1985	80.83	0.08	1985	-0.01075
2045	80.83	0.08	2045	-0.0065
2105	80.81	0.06	2105	0.008
2160	80.80	0.05	2160	0.021

Table B-7
Background Monitoring Well Fluctuations During Pumping Test Activities

(Page 1 of 14)

				MWBP-09		MWBP-09B		1
	Data	Elapsed	Transducer	Cumulative	Water Level	Cumulative	Water Level	
	Logger	Time	Reading	Xd Reading	Fluctuation	Xd Reading	Fluctuation	
	Time	(min)	(ft)	(ft)	(ft)	(ft)	(ft)	Comments
_	0	0	-0.003	-0.003	0.003	-0.009	0.009	3/17, 14:00
	20	20	-0.006	-0.006	0.006	-0.016	0.016	
	40	40	-0.009	-0.009	0.009	-0.022	0.022	
	60	60	-0.009	-0.009	0.009	-0.022	0.022	
	80	80	-0.012	-0.012	0.012	-0.025	0.025	
	100	100	-0.012	-0.012	0.012	-0.025	0.025	
	120	120	-0.019	-0.019	0.019	-0.035	0.035	
	140	140	-0.015	-0.015	0.015	-0.031	0.031	
	160	160	-0.022	-0.022	0.022	-0.038	0.038	
	180	180	-0.022	-0.022	0.022	-0.038	0.038	
	200	200	-0.015	-0.015	0.015	-0.031	0.031	
	220	220	0.012	0.012	-0.012	-0.006	0.006	
	240	240	0.047	0.047	-0.047	0.031	-0.031	
	260	260	0.063	0.063	-0.063	0.05	-0.05	
	280	280	0.073	0.073	-0.073	0.06	-0.06	
	300	300	0.082	0.082	-0.082		-0.069	
	320	320	0.092	0.092	-0.092		-0.076	
	340	340	0.095	0.095	-0.095		-0.082	
	360	360	0.089	0.089	-0.089	0.076	-0.076	
	380	380	0.079	0.079	-0.079		-0.066	
	400	400	0.063	0.063	-0.063		-0.05	
	420	420	0.05	0.05	-0.05		-0.038	
	440	440	0.066	0.066	-0.066		-0.054	
	460	460	0.066	0.066	-0.066		-0.05	
	480	480	0.057	0.057	-0.057	0.041	-0.041	
	500	500	0.06	0.06	-0.06		-0.044	
	520	520	0.06	0.06	-0.06	0.047	-0.047	
	540	540	0.054	0.054	-0.054		-0.038	
	560	560	0.047	0.047	-0.047	0.031	-0.031	
	580	580	0.073	0.073	-0.073		-0.054	
	600	600	0.073	0.073	-0.073		-0.06	
	620	620	0.086	0.086	-0.086	1	-0.066	
	640	640	0.089	0.089	-0.089		-0.073	
	660	660	0.076	0.076	-0.076		-0.057	
	680	680	0.082	0.082	-0.082 -0.07		-0.063 -0.047	
	700	700	0.07	0.07	-0.04	0.047	-0.025	
	720	720 740	0.044 0.028	0.044 0.028	-0.044		-0.025	
	740	760	0.028	0.028	-0.028		0.003	
	760 780			0.019	-0.019	-0.003	0.003	
	780 800	780 800	0.022 0.019	0.022	-0.022		0.003	
	800 820	820	0.019	0.019	-0.019		0.003	
	840	840	0.006	0.000	-0.000		0.010	
	860	860	0.012	0.012	-0.012		0.012	
	880	880	0.025	0.023	-0.023		0.006	
	900	900	0.019	0.019	-0.019		-0.006	
	300	300	0.033	0.000	-0.000	0.000	3.000	

Table B-7
Background Monitoring Well Fluctuations During Pumping Test Activities

(Page 2 of 14)

				MWBP-09		MWBP-09B		
	Data	Elapsed	Transducer	Cumulative	Water Level	Cumulative	Water Level	
	Logger	Time	Reading	Xd Reading	Fluctuation	Xd Reading	Fluctuation	
	Time	(min)	(ft)	(ft)	(ft)	(ft)	(ft)	Comments
_	920	920	0.019	0.019	-0.019	-0.006	0.006	
	940	940	0.031	0.031	-0.031	0.006	-0.006	
	960	960	0.041	0.041	-0.041	0.015	-0.015	
	980	980	0.041	0.041	-0.041	0.015	-0.015	
	1000	1000	0.054	0.054	-0.054	0.028	-0.028	
	1020	1020	0.057	0.057	-0.057	0.028	-0.028	
	1040	1040	0.06	0.06	-0.06	0.034	-0.034	
	1060	1060	0.082	0.082	-0.082	0.054	-0.054	
	1080	1080	0.076	0.076	-0.076	0.047	-0.047	
	1100	1100	0.082	0.082	-0.082	0.054	-0.054	·
	1120	1120	0.079	0.079	-0.079	0.05	-0.05	
	1140	1140	0.07	0.07	-0.07	0.041	-0.041	
	1160	1160	0.066	0.066	-0.066	0.041	-0.041	
	1180	1180	0.054	0.054	-0.054	0.025	-0.025	
	1200	1200	0.038	0.038	-0.038	0.012	-0.012	
	1220	1220	0.038	0.038	-0.038	0.009	-0.009	
	1240	1240	0.028	0.028	-0.028	0	0	
	1260	1260	0.012	0.012	-0.012	-0.016	0.016	
	1280	1280	0.006	0.006	-0.006	-0.019	0.019	
	1300	1300	0.003	0.003	-0.003	-0.025	0.025	
	1320	1320	0.009	0.009	-0.009	-0.022	0.022	
	1340	1340	0.006	0.006	-0.006	-0.022	0.022	
	1360	1360	0	0	0	-0.028	0.028	
	1380	1380	-0.009	-0.009	0.009	-0.035	0.035	
	1400	1400	-0.009	-0.009	0.009	-0.038	0.038	
	1420	1420	-0.006	-0.006	0.006	-0.035	0.035	
	1440	1440	-0.012	-0.012	0.012	-0.038	0.038	3/18, 14:00
	1460	1460	-0.009	-0.009	0.009	-0.035	0.035	
	1480	1480	0	0	0	-0.028	0.028	
	1500	1500	0.003	0.003	-0.003	-0.019	0.019	
	1520	1520	0.003	0.003	-0.003	-0.022	0.022	
	1540	1540	0.009	0.009	-0.009	-0.016	0.016	
	1560	1560	0.006	0.006	-0.006	-0.016	0.016	
	1580	1580	-0.006	-0.006	0.006	-0.025	0.025	
	1600	1600	-0.012	-0.012	0.012	-0.035	0.035	
	1620	1620	-0.019	-0.019	0.019		0.041	•
	1640	1640	-0.025	-0.025	0.025	-0.051	0.051	
	1660	1660	-0.025	-0.025	0.025	-0.047	0.047	
	1680	1680	-0.028	-0.028	0.028	1	0.051	
	1700	1700	-0.038	-0.038	0.038	1	0.06	1
	1720	1720	-0.028	-0.028	0.028		0.054	
	1740	1740	-0.022	-0.022	0.022		0.044	
	1760	1760	-0.019	-0.019	0.019		0.041	
	1780	1780	-0.012	-0.012	0.012		0.035	
	1800	1800	0.006	0.006	-0.006		0.016	
	1820	1820	0	0	0	-0.019	0.019	

Table B-7
Background Monitoring Well Fluctuations During Pumping Test Activities

(Page 3 of 14)

				(i ago o o	•,		
			MWBP-09		MWBP-09B		
Data	Elapsed	Transducer	Cumulative	Water Level	Cumulative	Water Level	
Logger	Time	Reading	Xd Reading		Xd Reading		
Time	(min)	(ft)	(ft)	(ft)	(ft)	(ft)	Comments
 1840	1840	-0.012	-0.012	0.012	-0.031	0.031	
1860	1860	0.003	0.003	-0.003		0.019	
1880	1880	0.009	0.009	-0.009		0.012	
1900	1900	0.015	0.015	-0.015		0.006	l e e e e e e e e e e e e e e e e e e e
1920	1920	-0.003	-0.003	0.003		0.022	
1940	1940	-0.009	-0.009	0.009	-0.031	0.031	
1960	1960	-0.015	-0.015	0.015	-0.038	0.038	
1980	1980	-0.019	-0.019	0.019		0.041	
2000	2000	-0.025	-0.025	0.025		0.047	
2020	2020	-0.019	-0.019	0.019		0.044	
2040	2040	-0.019	-0.019	0.019		0.044	
2040	2060	-0.016	-0.006	0.006	-0.031	0.031	
2080	2080	-0.009	-0.009	0.009	-0.035	0.035	
2100	2100	-0.009	-0.009	0.009	l .	0.031	
2120	2120	-0.009	-0.009	0.009		0.035	
2140	2140	-0.009	-0.022	0.003	-0.044	0.044	
2160	2160	-0.022	-0.022	0.022		0.06	
	2180	-0.055	-0.055	0.055	-0.076	0.076	
2180		-0.051	-0.051	0.031	-0.070	0.070	
2200	2200			0.066		0.009	
2220	2220	-0.066	-0.066	0.000	-0.095	0.093	
2240	2240	-0.07	-0.07		l .	0.098	
2260	2260	-0.054	-0.054	0.054	-0.082		
2280	2280	-0.044	-0.044	0.044	-0.073	0.073	
2300	2300	-0.035	-0.035	0.035	-0.066	0.066 0.063	
2320	2320	-0.038	-0.038	0.038		0.063	
2340	2340	-0.035	-0.035	0.035		0.003	
2360	2360	-0.019	-0.019	0.019 0.009	-0.047 -0.038	0.047	
2380	2380	-0.009	-0.009 -0.003	0.009	-0.036	0.030	
2400	2400	-0.003			i	0.031	
2420	2420	-0.009	-0.009	0.009	1	0.055	
2440	2440	-0.025	-0.025	0.025	1	0.031	
2460	2460	-0.019	-0.019	0.019		0.047	
2480	2480	-0.012	-0.012	0.012		0.041	
2500	2500	-0.012	-0.012	0.012		0.041	
2520	2520	-0.015	-0.015	0.015		0.041	
2540	2540	-0.006	-0.006	0.006	1		
2560	2560	-0.009	-0.009	0.009		0.038 0.035	•
2580	2580	-0.006	-0.006	0.006			
2600	2600	-0.022	-0.022	0.022		0.047	
2620	2620	-0.015	-0.015	0.015		0.041	
2640	2640	-0.019	-0.019	0.019		0.044	
2660	2660	-0.012	-0.012	0.012		0.041	
2680	2680	-0.015	-0.015	0.015		0.041	
2700	2700	-0.025	-0.025	0.025		0.051	
2720	2720	-0.022	-0.022	0.022	t e	0.051	
2740	2740	-0.038	-0.038	0.038	-0.063	0.063	1

Table B-7
Background Monitoring Well Fluctuations During Pumping Test Activities

(Page 4 of 14)

					(. aga . a	• /		
				MWBP-09		MWBP-09B		
	Data	Elapsed	Transducer	Cumulative	Water Level	Cumulative	Water Level	
	Logger	Time	Reading		Fluctuation			
	Time	(min)	(ft)	(ft)	(ft)	(ft)	(ft)	Comments
_	2760	2760	-0.047	-0.047	0.047	-0.07	0.07	
	2780	2780	-0.051	-0.051	0.051	-0.076	0.076	
	2800	2800	-0.057	-0.057	0.057		0.082	
	2820	2820	-0.073	-0.073	0.073		0.092	
	2840	2840	-0.086	-0.086	0.086		0.108	
	2860	2860	-0.095	-0.095	0.095	1	0.117	
	2880	2880	-0.098	-0.098	0.098	1		3/19, 14:00
	2900	2900	-0.095	-0.095	0.095	1	0.117	
	2920	2920	-0.098	-0.098	0.098	1	0.121	ľ
	2940	2940	-0.095	-0.095	0.095	5	0.117	
	2960	2960	-0.098	-0.098	0.098	1	0.121	
	2980	2980	-0.095	-0.095	0.095		0.114	
	3000	3000	-0.098	-0.098	0.098		0.117	
	3020	3020	-0.105		0.105		0.121	
	3040	3040	-0.101	-0.101	0.101		0.121	
	3060	3060	-0.092	-0.092	0.092		0.111	
	3080	3080	-0.092	-0.095	0.095	B .	0.111	
	3100	3100	-0.095	-0.095	0.095	P .	0.111	
	3120	3120	-0.093	-0.093	0.033		0.095	
		3140	-0.079	-0.079 -0.076	0.076		0.092	
	3140	3140	-0.076	-0.076	0.076		0.092	
	3160				0.073		0.032	
	3180	3180	-0.073 -0.06	-0.073 -0.06	0.073		0.000	
	3200	3200			0.06		0.073	
	3220	3220	-0.06		0.00	1	0.073	
	3240	3240	-0.07 -0.124		0.07	1	0.073	1
	3260	3260	-0.124		0.124	i .	0.168	
	3280	3280			0.130		0.13	
	3300	3300 3320	-0.114 -0.101	-0.114	0.114		0.114	
	3320		-0.101	-0.101	0.079		0.092	
	3340	3340	-0.079		0.079		0.098	P .
	3360 3380	3360 3380	-0.085				0.108	ı
	3400	3400	-0.093			2	0.095	1
	3420	3420	-0.082			1	0.082	
	3440	3440	-0.075			1	0.076	
		3460	-0.076			1	0.076	1
	3460	3480	-0.076			1	0.086	i
	3480	3500	-0.076			1	0.086	1
	3500	3520	-0.073				0.082	1
	3520 3540	3540	-0.073				0.002	
		3560	-0.009				0.108	1
	3560 3580	3580	-0.095		0.093	l	0.103	1
	3600	3600	-0.101					I .
	3620	3620	-0.101 -0.095					1
	3640	3640	-0.095			1		
	3640 3660	3660	-0.100		0.100			
	3000	3000	-0.111	-0.111	0.111	1 -0.124	0.124	ı

Table B-7
Background Monitoring Well Fluctuations During Pumping Test Activities

(Page 5 of 14)

					-			1
				MWBP-09		MWBP-09B		
	Data	Elapsed	Transducer	Cumulative				
	Logger	Time	Reading	Xd Reading	Fluctuation			
_	Time	(min)	(ft)	(ft)	(ft)	(ft)	(ft)	Comments
	3680	3680	-0.121	-0.121	0.121		0.133	
	3700	3700	-0.111	-0.111	0.111		0.127	
	3720	3720	-0.114	-0.114	0.114		0.13	
	3740	3740	-0.117	-0.117	0.117	-0.137	0.137	
	3760	3760	-0.13	-0.13	0.13	-0.149	0.149	
	3780	3780	-0.117	-0.117	0.117	-0.14	0.14	
	3800	3800	-0.114	-0.114	0.114	-0.133	0.133	
	3820	3820	-0.111	-0.111	0.111	-0.13	0.13	
	3840	3840	-0.111	-0.111	0.111	-0.133	0.133	
	3860	3860	-0.111	-0.111	0.111	-0.13	0.13	
	3880	3880	-0.108	-0.108	0.108	-0.13	0.13	
	3900	3900	-0.101	-0.101	0.101	-0.124	0.124	
	3920	3920	-0.092	-0.092	0.092	-0.114	0.114	
	3940	3940	-0.086	-0.086	0.086	-0.108	0.108	
	3960	3960	-0.076	-0.076	0.076	-0.095	0.095	
	3980	3980	-0.066	-0.066	0.066	-0.086	0.086	
	4000	4000	-0.066	-0.066	0.066	-0.086	0.086	
	4020	4020	-0.066		0.066	-0.086	0.086	
	4040	4040	-0.073	-0.073	0.073	-0.095	0.095	
	4060	4060	-0.076	-0.076	0.076	-0.098	0.098	
	4080	4080	-0.073	-0.073	0.073	-0.092	0.092	
	4100	4100	-0.073	-0.073	0.073	-0.092	0.092	
	4120	4120	-0.079	-0.079	0.079	-0.098	0.098	
	4140	4140	-0.082	-0.082	0.082	-0.101	0.101	
	4160	4160	-0.098	-0.098	0.098	-0.117	0.117	
	4180	4180	-0.101	-0.101	0.101	-0.121	0.121	
	4200	4200	-0.105	-0.105	0.105	-0.124	0.124	
	4220	4220	-0.111	-0.111	0.111	-0.13	0.13	
	4240	4240	-0.114	-0.114	0.114	-0.133	0.133	
	4260	4260	-0.121	-0.121	0.121	-0.137	0.137	
	4280	4280	-0.121	-0.121	0.121	-0.137	0.137	
	0	4360	-0.07	-0.191	0.191	-0.2	0.2	
	20	4380	-0.057	-0.178	0.178	-0.187	0.187	
	40	4400	-0.044	-0.165	0.165	-0.175	0.175	
	60	4420	-0.035	-0.156	0.156	-0.171	0.171	3/20, 15:00
	80	4440	-0.028		0.149	-0.165	0.165	
	100	4460	-0.028	-0.149	0.149	-0.165	0.165	
	120	4480	-0.035	-0.156	0.156	-0.171	0.171	
	140	4500	-0.038	-0.159	0.159	-0.175	0.175	
	160	4520	-0.044	-0.165	0.165	-0.178	0.178	
	180	4540	-0.038		0.159		0.171	
	200	4560	-0.044	-0.165	0.165		0.178	
	220	4580	-0.041	-0.162	0.162		0.178	
	240	4600	-0.044		0.165		0.181	
	260	4620	-0.048		0.169		0.181	
	280	4640	-0.048		0.169		0.184	i
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Table B-7
Background Monitoring Well Fluctuations During Pumping Test Activities

(Page 6 of 14)

			MWBP-09		MWBP-09B		
Data	Elapsed	Transducer	Cumulative	Water Level	Cumulative	Water Level	
Logger	Time	Reading	Xd Reading	Fluctuation	Xd Reading	Fluctuation	
Time	(min)	(ft)	(ft)	(ft)	(ft)	(ft)	Comments
300	4660	-0.038	-0.159	0.159	-0.171	0.171	
320	4680	-0.041	-0.162	0.162	-0.175	0.175	
340	4700	-0.025	-0.146	0.146	-0.162	0.162	
360	4720	-0.025	-0.146	0.146	-0.162	0.162	
380	4740	-0.032	-0.153	0.153	-0.168	0.168	
400	4760	-0.032	-0.153	0.153	-0.165	0.165	
420	4780	-0.028	-0.149	0.149	-0.165	0.165	
440	4800	-0.032	-0.153	0.153	-0.168	0.168	
460	4820	-0.032	-0.153	0.153	-0.165	0.165	
480	4840	-0.032	-0.153	0.153	-0.168	0.168	
500	4860	-0.038	-0.159	0.159	-0.175	0.175	
520	4880	-0.035	-0.156	0.156	-0.171	0.171	
540	4900	-0.028	-0.149	0.149	-0.165	0.165	
560	4920	-0.044	-0.165	0.165	-0.181	0.181	
580	4940	-0.035	-0.156	0.156	-0.171	0.171	
600	4960	-0.038	-0.159	0.159	-0.175	0.175	
620	4980	-0.044	-0.165	0.165	-0.181	0.181	
640	5000	-0.038	-0.159	0.159	-0.171	0.171	
660	5020	-0.028	-0.149	0.149	-0.162	0.162	
680	5040	-0.035	-0.156	0.156	-0.171	0.171	
700	5060	-0.032	-0.153	0.153	-0.168	0.168	
720	5080	-0.041	-0.162	0.162	-0.178	0.178	
740	5100	-0.054	-0.175	0.175	-0.19	0.19	
760	5120	-0.057	-0.178	0.178	-0.194	0.194	
780	5140	-0.064	-0.185	0.185	-0.2	0.2	
800	5160	-0.051	-0.172	0.172	-0.187	0.187	
820	5180	-0.051	-0.172	0.172	-0.184	0.184	
840	5200	-0.048	-0.169	0.169	-0.181	0.181	
860	5220	-0.041	-0.162	0.162	-0.175	0.175	
880	5240	-0.032	-0.153	0.153	-0.165	0.165	
900	5260	-0.025	-0.146	0.146	-0.162	0.162	
920	5280	-0.019	-0.14	0.14	-0.152	0.152	
940	5300	-0.009	-0.13	0.13	-0.146	0.146	
960	5320	-0.003	-0.124	0.124	-0.14	0.14	
980	5340	-0.003	-0.124	0.124	-0.14	0.14	
1000	5360	-0.003	-0.124	0.124	-0.14	0.14	
1020	5380	-0.006	-0.127	0.127	-0.14	0.14	
0	5400	0	-0.127	0.127	-0.14		3/21, 08:00
20	5420	0.009	-0.118	0.118	-0.134	0.134	
40	5440	0.006	-0.121	0.121	-0.137	0.137	
60	5460	0.015	-0.112	0.112	-0.125	0.125	
80	5480	0.019	-0.108	0.108	-0.121	0.121	
100	5500	0.019	-0.108	0.108	-0.125	0.125	
120	5520	0.015	-0.112	0.112	-0.128	0.128	
140	5540	0.022	-0.105	0.105	-0.121	0.121	
160	5560	0.019	-0.108	0.108	-0.125	0.125	

Table B-7
Background Monitoring Well Fluctuations During Pumping Test Activities

(Page 7 of 14)

			MWBP-09		MWBP-09B		1
Data	Elapsed	Transducer	Cumulative	Water Level	Cumulative	Water Level	
Logger	Time	Reading	Xd Reading	Fluctuation	Xd Reading	Fluctuation	
Time	(min)	(ft)	(ft)	(ft)	(ft)	(ft)	Comments
180	5580	0.012	-0.115	0.115	-0.131	0.131	
200	5600	0.015	-0.112	0.112	-0.131	0.131	
220	5620	0.015	-0.112	0.112	-0.131	0.131	
240	5640	0.006	-0.121	0.121	-0.14	0.14	
260	5660	0	-0.127	0.127	-0.146		Begin step-drawdown test in
280	5680	-0.009	-0.136	0.136	-0.155	0.155	MWBP-12 @1230 (5670 min)
300	5700	-0.016	-0.143	0.143	-0.162	0.162	
320	5720	-0.009	-0.136	0.136	-0.159	0.159	
340	5740	-0.019	-0.146	0.146	-0.165	0.165	
360	5760	-0.032	-0.159	0.159	-0.178	0.178	
380	5780	-0.035	-0.162	0.162	-0.181	0.181	
400	5800	-0.035	-0.162	0.162	-0.181	0.181	
420	5820	-0.032	-0.159	0.159	-0.178	0.178	
440	5840	-0.038	-0.165	0.165	-0.187	0.187	
460	5860	-0.038	-0.165	0.165	-0.184	0.184	
480	5880	-0.051	-0.178	0.178	-0.197	0.197	
500	5900	-0.048	-0.175	0.175	-0.193	0.193	End step-drawdown test in
520	5920	-0.038	-0.165	0.165	-0.184	0.184	MWBP-12 @1600 (5910 min)
540	5940	-0.025	-0.152	0.152	-0.171	0.171	
560	5960	-0.006	-0.133	0.133	-0.149	0.149	
580	5980	-0.009	-0.136	0.136	-0.155	0.155	
600	6000	-0.016	-0.143	0.143	-0.159	0.159	
620	6020	-0.009	-0.136	0.136	-0.152	0.152	
640	6040	-0.009	-0.136	0.136	-0.152	0.152	
660	6060	0.003	-0.124	0.124	-0.14	0.14	
680	6080	0.006	-0.121	0.121	-0.137	0.137	
700	6100	0.009	-0.118	0.118	-0.134	0.134	
720	6120	0.019	-0.108	0.108	-0.125	0.125	
740	6140	0.025	-0.102	0.102	-0.121	0.121	
760	6160	0.031	-0.096	0.096	-0.112	0.112	
780	6180	0.031	-0.096	0.096	-0.112	0.112	
800	6200	0.031	-0.096	0.096	-0.115	0.115	
820	6220	0.028	-0.099	0.099	-0.118	0.118	
840	6240	0.019	-0.108	0.108	-0.125	0.125	
860	6260	0.019	-0.108	0.108	-0.125	0.125	
880	6280	0.022	-0.105	0.105	-0.121	0.121	
900	6300	0.015	-0.112	0.112	-0.128	0.128	
920	6320	0.019	-0.108	0.108	-0.125	0.125	
940	6340	0.022	-0.105	0.105	-0.121	0.121	
960	6360	0.025	-0.102	0.102	-0.118	0.118	
980	6380	0.028	-0.099	0.099	-0.115	0.115	
1000	6400	0.025	-0.102	0.102	-0.118	0.118	
1020	6420	0.025	-0.102	0.102	-0.118	0.118	
1040	6440	0.019	-0.108	0.108	-0.125	0.125	
1060	6460	0.006	-0.121	0.121	-0.14	0.14	
1080	6480	-0.009	-0.136	0.136	-0.152	0.152	
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Table B-7
Background Monitoring Well Fluctuations During Pumping Test Activities

(Page 8 of 14)

				MWBP-09		MWBP-09B		
	Data	Elapsed	Transducer	Cumulative	Water Level	Cumulative	Water Level	
	Logger	Time	Reading	Xd Reading	Fluctuation	Xd Reading	Fluctuation	
	Time	(min)	(ft)	(ft)	(ft)	(ft)	(ft)	Comments
	1100	6500	-0.012	-0.139	0.139	-0.155	0.155	
	1120	6520	-0.019	-0.146	0.146	-0.162	0.162	
	1140	6540	-0.032	-0.159	0.159	-0.174	0.174	
	1160	6560	-0.038	-0.165	0.165	-0.178	0.178	
	1180	6580	-0.041	-0.168	0.168	-0.184	0.184	
	1200	6600	-0.051	-0.178	0.178	-0.193	0.193	
	1220	6620	-0.057	-0.184	0.184	-0.197	0.197	
	1240	6640	-0.054	-0.181	0.181	-0.197	0.197	
	1260	6660	-0.054	-0.181	0.181	-0.193	0.193	
	1280	6680	-0.057	-0.184	0.184	-0.2	0.2	
	1300	6700	-0.06	-0.187	0.187	-0.2	0.2	
	1320	6720	-0.057	-0.184	0.184	-0.2	0.2	
	1340	6740	-0.057	-0.184	0.184	-0.197	0.197	
	1360	6760	-0.064	-0.191	0.191	-0.206	0.206	
	1380	6780	-0.07	-0.197	0.197	-0.212	0.212	
	1400	6800	-0.064	-0.191	0.191	-0.206	0.206	
	1420	6820	-0.064	-0.191	0.191	-0.203	0.203	
	1440	6840	-0.07	-0.197	0.197	-0.209		3/22, 08:00
	1460	6860	-0.064	-0.191	0.191	-0.206	0.206	
	1480	6880	-0.07	-0.197	0.197	-0.212	0.212	
	1500	6900	-0.073	-0.2	0.2	-0.212	0.212	
	1520	6920	-0.076	-0.203	0.203	-0.216	0.216	
	1540	6940	-0.073	-0.2	0.2	-0.216	0.216	
	1560	6960	-0.086	-0.213	0.213	-0.225	0.225	
	1580	6980	-0.089	-0.216	0.216	-0.231	0.231	
	1600	7000	-0.099	-0.226	0.226	-0.238	0.238	
	1620	7020	-0.102	-0.229	0.229	-0.244		Begin step-drawdown test in
	1640	7040	-0.108	-0.235	0.235	-0.247		BP-05B @1050 (7010 min)
	1660	7060	-0.115	-0.242	0.242	-0.254	0.254	
	1680	7080	-0.118	-0.245	0.245	-0.257	0.257	
	1700	7100	-0.134	-0.261	0.261	-0.276	0.276	
	1720	7120	-0.137	-0.264	0.264	-0.276	0.276	
	1740	7140	-0.144	-0.271	0.271	-0.285	0.285	
	1760	7160	-0.147	-0.274 -0.28	0.274	-0.285	0.285	
	1780 1800	7180 7200	-0.153 -0.156	-0.283	0.28 0.283	-0.295	0.295	
	1820	7200	-0.163	-0.263	0.283	-0.298 -0.304	0.298 0.304	
	1840	7240	-0.163 -0.156		0.283	-0.304	0.304	
	1860	7240	-0.15	-0.283 -0.277	0.263	-0.298	0.298	
	1880	7280	-0.163	-0.29	0.27	-0.292	0.292	
	1900	7300	-0.169	-0.29	0.29	-0.304	0.304	
	1900	7300	-0.175	-0.296	0.296	-0.306		End step-drawdown test in
	1940	7340	-0.173	-0.302	0.302	-0.317		BP-05B @1615 (7335 min)
	1960	7340	-0.188	-0.309	0.309	-0.323	0.323	Dr-030 (#1013 (7333 Hill)
	1980	7380	-0.182	-0.309	0.319	-0.32	0.33	
	0	7440	0.003	-0.309	0.306		0.32	
DIC	CBDI UC AI 6			3.000	0.000	-0.02	0.02	

Table B-7
Background Monitoring Well Fluctuations During Pumping Test Activities

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				MWBP-09		MWBP-09B		
	Data	Elapsed	Transducer		Water Level	Cumulative	Water Level	
	Logger	Time	Reading		Fluctuation			
	Time	(min)	(ft)	(ft)	(ft)	(ft)	(ft)	Comments
-	20	7460	0.022	-0.287	0.287	-0.305	0.305	
	40	7480	0.028	-0.281	0.281	-0.295	0.295	
	60	7500	0.031	-0.278	0.278	-0.295	0.295	
	80	7520	0.035	-0.274	0.274	-0.292	0.292	
	100	7540	0.031	-0.278	0.278	-0.292	0.292	
	120	7560	0.035	-0.274	0.274	-0.292	0.292	
	140	7580	0.038	-0.271	0.271	-0.285	0.285	1
	160	7600	0.038	-0.271	0.271	-0.285	0.285	4
	180	7620	0.044	-0.265	0.265	-0.276	0.276	•
	200	7640	0.035	-0.274	0.274	-0.285	0.285	1
	220	7660	0.031	-0.278	0.278	-0.295	0.295	
	240	7680	0.044	-0.265	0.265		0.279	
	260	7700	0.044	-0.265	0.265		0.279	
	280	7720	0.038	-0.271	0.271	-0.282	0.282	
	300	7740	0.044	-0.265	0.265		0.276	
	320	7760	0.047	-0.262	0.262		0.273	
	340	7780		-0.271	0.271	-0.282	0.282	1
	360	7800	0.031	-0.278	0.278	i e	0.289	
	380	7820	0.019	-0.29	0.29	1	0.301	•
	400	7840	0.035		0.274		0.289	
	420	7860	0.028		0.281	-0.295	0.295	
	440	7880	0.028		0.281	-0.292	0.292	1
	460	7900	0.047		0.262		0.276 0.238	
	480	7920	0.079	-0.23	0.23	i	0.238	
	500	7940	0.092		0.217 0.217		0.225	I .
	520	7960	0.092 0.076		0.217		0.223	I .
	540	7980 8000	0.078		0.233	1	0.235	I .
	560 580	8020	0.002	-0.239	0.239	1	0.247	
	600	8040	0.089	-0.239	0.23		0.235	I .
	620	8040	0.003	-0.214	0.214		0.222	1
	640	8080			0.214		0.209	I .
	660	8100		-0.198			0.209	1
	680	8120					0.196	1
	700	8140		-0.188		i	0.199	
	720	8160		-0.198			0.206	I .
	740	8180					0.193	I .
	760	8200				1	0.177	1
	780	8220				t	0.171	
	800	8240				1	0.171	1
	820	8260					0.174	
	840	8280					0.18	3/23, 08:00
	860	8300					0.177	
	880	8320				•	0.177	
	900	8340					0.177	
	920	8360				-0.171	0.171	
						•		-

Table B-7
Background Monitoring Well Fluctuations During Pumping Test Activities

(Page 10 of 14)

				(* ***)	. *		_
			MWBP-09		MWBP-09B		
Data	Elapsed	Transducer	Cumulative	Water Level	Cumulative	Water Level	
Logger	Time	Reading	Xd Reading	Fluctuation	Xd Reading	Fluctuation	
Time	(min)	(ft)	(ft)	(ft)	(ft)	(ft)	Comments
 940	8380	0.149	-0.16	0.16	-0.171	0.171	
960	8400	0.146	-0.163	0.163	-0.171	0.171	Begin constant Q test in
980	8420	0.146	-0.163	0.163	-0.171	0.171	BP-12 @1000 (8400 min)
1000	8440	0.14	-0.169	0.169	-0.177	0.177	
1020	8460	0.13	-0.179	0.179	-0.184	0.184	
1040	8480	0.13	-0.179	0.179	-0.187	0.187	
1060	8500	0.117	-0.192	0.192		0.196	·
1080	8520	0.117	-0.192	0.192		0.199	
1100	8540	0.117	-0.192	0.192	1	0.196	
1120	8560	0.117	-0.192	0.192		0.196	
1140	8580	0.111	-0.198	0.198	1	0.199	
1160	8600	0.102	-0.207	0.207	-0.209	0.209	
1180	8620	0.098	-0.211	0.211	-0.215	0.215	
1200	8640	0.092	-0.217	0.217		0.222	
1220	8660	0.092	-0.217	0.217		0.219	
1240	8680	0.082	-0.227	0.227	-0.228	0.228	
1260	8700	0.089	-0.22	0.22	-0.225	0.225	4
1280	8720	0.079	-0.23	0.23	1	0.228	1
1300	8740	0.076	-0.233	0.233		0.231	
1320	8760	0.082	-0.227	0.227	-0.228	0.228	
1340	* 8780	0.095	-0.214	0.214		0.215	
1360	8800	0.108	-0.201	0.201	-0.203	0.203	
1380	8820	0.105	-0.204	0.204		0.206	
1400	8840	0.117	-0.192	0.192		0.19	
1420	8860	0.108	-0.201	0.201	-0.196	0.196	
1440	8880	0.098		0.211	-0.209	0.209	
1460	8900	0.098		0.211	-0.209	0.209	5
1480	8920	0.114	-0.195	0.195		0.193	
1500	8940	0.114	-0.195	0.195		0.193	
1520	8960	0.137		0.172		0.171	
1540	8980	0.149		0.16		0.158	1
1560	9000						1
1580	9020						
1600	9040					0.158	
1620	9060	0.146				0.158	
1640	9080					0.165	
1660	9100				1	0.161	
1680	9120					0.155	
1700	9140	0.149			t e	0.155	
1720	9160	0.149		0.16		0.158	
1740	9180	0.146		0.163		0.158	
1760	9200	0.146				0.161	
1780	9220				•	0.161	
1800	9240					0.165	
1820	9260					0.171	i
1840	9280						
							•

Table B-7
Background Monitoring Well Fluctuations During Pumping Test Activities

(Page 11 of 14)

	MWBP-09 MWBP-09B							
	Data	Elapsed	Transducer	Cumulative	Water Level	Cumulative	Water Level	
	Logger	Time	Reading	Xd Reading	Fluctuation	Xd Reading	Fluctuation	
	Time	(min)	(ft)	(ft)	(ft)	(ft)	(ft)	Comments
_	1860	9300	0.13	-0.179	0.179	-0.177	0.177	
	1880	9320	0.127	-0.182	0.182		0.177	
	1900	9340	0.124	-0.185	0.185		0.184	
	1920	9360	0.111	-0.198	0.198		0.193	
	1940	9380	0.105	-0.204	0.204		0.199	
	1960	9400	0.102	-0.207	0.207	-0.203	0.203	
	1980	9420	0.098	-0.211	0.211	-0.206	0.206	Programme and the second secon
	2000	9440	0.095	-0.214	0.214		0.209	
	2020	9460	0.098	-0.211	0.211	-0.209	0.209	
	2040	9480	0.098	-0.211	0.211	-0.209	0.209	
	2060	9500	0.102	-0.207	0.207	-0.206	0.206	
	2080	9520	0.108	-0.201	0.201	-0.199	0.199	
	2100	9540	0.105	-0.204	0.204		0.203	1
	2120	9560	0.102	-0.207	0.207	-0.206	0.206	I .
	2140	9580	0.105	-0.204	0.204		0.203	
	2160	9600	0.098	-0.211	0.211	-0.209		End constant Q test in
	2180	9620	0.102	-0.207	0.207	-0.206		BP-12 @0600 (9600 min)
	2200	9640	0.102	-0.207	0.207	-0.206	0.206	
	2220	9660	0.105	-0.204	0.204		0.203	1
	2240	9680	0.108	-0.201	0.201	-0.199	0.199	
	2260	9700	0.111	-0.198	0.198		0.196	
	2280	9720	0.114	-0.195	0.195			3/24, 08:00
	2300	9740	0.114	-0.195	0.195			End recovery monitoring at
	2320	9760	0.114	-0.195	0.195		0.196	
	0	14040	0	-0.09	0.09	1		3/27, 08:00
	20	14060	0	-0.09	0.09		0.091	
	40	14080	0	-0.09	0.09	1	0.091	
	60	14100	0	-0.09	0.09		0.091	
	80	14120	-0.003	-0.093	0.093		0.094	
	100	14140	0	-0.09	0.09		0.091	
	120	14160	-0.009	-0.099	0.099 0.102		0.1 0.103	1
	140	14180	-0.012	-0.102 -0.109	0.102		0.103	
	160	14200	-0.019 -0.028	-0.109	0.109		0.119	
	180	14220	-0.026	-0.110	0.110		0.113	
	200 220	14240 14260	-0.031	-0.121	0.121			Begin constant Q test in
	240	14280	-0.034	-0.124	0.124			BP-05B @1140 (14260 min)
	260	14300	-0.041	-0.134	0.131		0.135	
	280	14300	-0.044	-0.134	0.134		0.144	1
	300	14340	-0.057	-0.143	0.143	1	0.148	
	320	14340	-0.057	-0.153	0.147		0.154	
	340	14380	-0.065	-0.156	0.156		0.157	
	360	14400	-0.069	-0.159	0.159		0.137	
	380	14420	-0.069		0.162		0.163	
	400	14440	-0.072	-0.162	0.162		0.167	3
	400	14460	-0.076		0.166		0.167	
	420	14400	-0.070	-0.100	0.100	1 -0.107	0.107	I

Table B-7
Background Monitoring Well Fluctuations During Pumping Test Activities

(Page 12 of 14)

Data Elapsed Transducer Cumulative Water Level Cumulative Cumul	
Logger Time (min) (h)	
Time (min) (ft) (ft) (ft) (ft) (ft) Comments 440 14480 -0.076 -0.166 0.166 -0.167 0.167 480 14520 -0.076 -0.166 0.166 -0.167 0.167 500 14540 -0.072 -0.162 0.162 -0.163 0.163 520 14560 -0.069 -0.159 0.159 -0.16 0.16 540 14580 -0.066 -0.156 0.156 -0.157 0.157 560 14600 -0.063 -0.153 0.153 -0.154 0.154 600 14640 -0.053 -0.143 0.143 -0.144 0.144 620 14660 -0.05 -0.14 0.14 -0.141 0.144 640 14880 -0.047 -0.137 0.133 0.135 0.135 660 14700 -0.044 -0.131 0.131 -0.132 0.125 700 <t< td=""><td></td></t<>	
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Table B-7
Background Monitoring Well Fluctuations During Pumping Test Activities

(Page 13 of 14)

				MWBP-09		MWBP-09B		
	Data	Elapsed	Transducer		Water Level		Water Level	
	Logger	Time	Reading		Fluctuation			
	Time	(min)	(ft)	(ft)	(ft)	(ft)	(ft)	Comments
_	1360	15400	-0.038	-0.128	0.128		0.129	
	1380	15420	-0.033	-0.121	0.121		0.122	
	1400	15440	-0.034	-0.124	0.124		0.125	
	1420	15460	-0.038	-0.128	0.128	8	0.129	
	1440	15480	-0.034	-0.124	0.124	P .		3/28, 08:00
	1460	15500	-0.034	-0.124	0.124		0.125	
	1480	15520	-0.034	-0.124	0.124		0.125	
	1500	15540	-0.031	-0.121	0.121	-0.122	0.122	
	1520	15560	-0.031	-0.121	0.121	-0.122	0.122	
	1540	15580	-0.031	-0.121	0.121		0.122	
	1560	15600	-0.034	-0.124	0.124		0.125	
	1580	15620	-0.038	-0.128	0.128		0.129	
	1600	15640	-0.041	-0.131	0.131	-0.132	0.132	
	1620	15660	-0.044	-0.134	0.134	-0.135	0.135	
	1640	15680	-0.041	-0.131	0.131	Į.	0.132	
	1660	15700	-0.05	-0.14	0.14		0.141	
	1680	15720	-0.057	-0.147	0.147		0.148	
	1700	15740	-0.066	-0.156	0.156		0.157	
	1720	15760	-0.076	-0.166	0.166		0.167	
	1740	15780	-0.079	-0.169	0.169		0.17	
	1760	15800	-0.085	-0.175	0.175	1	0.176	
	1780	15820	-0.085	-0.175	0.175	-0.176	0.176	
	1800	15840	-0.085	-0.175	0.175	-0.176	0.176	
	1820	15860	-0.085	-0.175	0.175	-0.176	0.176	
	1840	15880	-0.088	-0.178	0.178	-0.179	0.179	
	1860	15900	-0.085	-0.175	0.175	-0.176	0.176	
	1880	15920	-0.085	-0.175	0.175	-0.176	0.176	
	1900	15940	-0.082	-0.172	0.172	-0.173	0.173	
	1920	15960	-0.082	-0.172	0.172	-0.173	0.173	
	1940	15980	-0.082	-0.172	0.172		0.173	
	1960	16000	-0.076	-0.166	0.166		0.167	
	1980	16020	-0.072	-0.162		1		
	2000	16040				1	0.157	
	2020	16060						
	2040	16080			0.156	1		
	2060	16100					0.151	
	2080	16120				1	0.148	
	2100	16140			0.14	1	0.141	
	2120	16160		-0.131	0.131		0.132	
	2140	16180		-0.131	0.131		0.132	
	2160	16200	-0.038	-0.128	0.128		0.129	1
	2180	16220	-0.034		0.124		0.125	
	2200	16240					0.125	
	2220	16260		-0.121	0.121			l e
	2240	16280				1		
	2260	16300	-0.034	-0.124	0.124	-0.125	0.125	

Table B-7
Background Monitoring Well Fluctuations During Pumping Test Activities

(Page 14 of 14)

					MWBP-09B			
	Data	Elapsed	Transducer	Cumulative				
	Logger	Time	Reading	Xd Reading	Fluctuation	Xd Reading		
	Time	(min)	(ft)	(ft)	(ft)	(ft)	(ft)	Comments
_	2280	16320	-0.041	-0.131	0.131	-0.132	0.132	
	2300	16340	-0.05	-0.14	0.14		0.141	
	2320	16360	-0.05	-0.14	0.14		0.141	
	2340	16380	-0.053	-0.143	0.143		0.144	
	2360	16400	-0.06	-0.15	0.15		0.151	
	2380	16420	-0.063	- 0.153	0.153	-0.154	0.154	End constant Q test in
	2400	16440	-0.066	-0.156	0.156	-0.157	0.157	BP-05B @2340 (16420 min)
	2420	16460	-0.063	-0.153	0.153	-0.154	0.154	
	2440	16480	-0.066	-0.156	0.156	-0.157	0.157	
	2460	16500	-0.066	-0.156	0.156	-0.157	0.157	
	2480	16520	-0.069	-0.159	0.159	-0.16	0.16	
	2500	16540	-0.066	-0.156	0.156	-0.157		End recovery monitoring
	2520	16560	-0.063	-0.153	0.153	-0.154	0.154	at 01:45
	2540	16580	-0.063	-0.153	0.153	-0.154	0.154	
	2560	16600	-0.063	-0.153	0.153	-0.154	0.154	
	2580	16620	-0.063	-0.153	0.153	-0.154	0.154	
	2600	16640	-0.057	-0.147	0.147	-0.148	0.148	
	2620	16660	-0.057	-0.147	0.147	-0.148	0.148	
	2640	16680	-0.057	-0.147	0.147	-0.148	0.148	
	2660	16700	-0.057	-0.147	0.147	-0.148	0.148	
	2680	16720	-0.057	-0.147	0.147	-0.148	0.148	
	2700	16740	-0.053	-0.143	0.143	-0.144	0.144	
	2720	16760	-0.05	-0.14	0.14	-0.141	0.141	
	2740	16780	-0.047	-0.137	0.137	-0.138	0.138	1
	2760	16800	-0.044	-0.134	0.134	-0.135	0.135	
	2780	16820	-0.038	-0.128	0.128	-0.129	0.129	
	2800	16840	-0.031	-0.121	0.121	-0.122	0.122	
	2820	16860	-0.028	-0.118	0.118	-0.119	0.119	
	2840	16880	-0.028	-0.118	0.118	-0.119	0.119	
	2860	16900	-0.031	-0.121	0.121	-0.122	0.122	
	2880	16920	-0.028	-0.118	0.118	-0.119		3/29, 08:00
	2900	16940	-0.025	-0.115	0.115	-0.116	0.116	

Table B-8
Barometric Pressure Observations
(From the National Weather Service at Fresno Air Terminal)

(Page 1 of 6)

Date/Time Date/Time Date/Time Cimin Hy Pressure Reading (in. Hy) Pressure Reading (fit. HyO) Absolute Comments 3/17/95, 1400 0 29.695 33.644 0 60 29.685 33.633 -0.01133 120 29.675 33.692 -0.02266 180 29.655 33.599 -0.04532 240 29.755 33.712 0.06798 360 29.775 33.735 0.09064 420 29.755 33.712 0.06798 3/17, 2300 540 29.785 33.735 0.09064 480 29.775 33.735 0.09064 3/18, 0100 660 29.805 33.769 0.1197 720 29.815 33.780 0.1133 840 29.795 33.758 0.1133 900 29.800 33.763 0.11896 960 29.830 33.763 0.11896 960 29.845 33.814 0.16995 1020 29.885 33.80			, 5	,		
Date/Time (min) (in. Hg) (ft. H ₂ O) (ft. H ₂ O) Comments		Elapsed	Pressure	Pressure	Absolute	
3/17/95, 1400 0 29.695 33.644 0 60 29.685 33.633 -0.01133 120 29.675 33.599 -0.04532 240 29.705 33.656 0.01133 300 29.755 33.712 0.06798 420 29.775 33.735 0.09064 420 29.755 33.712 0.06798 480 29.775 33.736 0.10197 600 29.805 33.769 0.12463 3/18, 0100 660 29.805 33.769 0.12463 3/18, 0100 660 29.805 33.769 0.13596 780 29.795 33.758 0.1133 840 29.795 33.758 0.1133 840 29.795 33.758 0.1133 840 29.795 33.768 0.1133 840 29.795 33.769 0.12463 3/18, 0100 29.800 33.763 0.118965 960 29.800 33.763 0.118965 1020 29.845 33.814 0.16995 1020 29.885 33.860 0.21527 1260 29.875 33.848 0.20394 1320 29.886 33.837 0.19261 1380 29.865 33.837 0.19261 1380 29.865 33.837 0.19261 1380 29.865 33.837 0.19261 1380 29.865 33.837 0.19261 1380 29.865 33.837 0.186945 1440 29.855 33.826 0.18128 1500 29.855 33.826 0.18128 1600 29.875 33.848 0.20394 1320 29.865 33.837 0.19261 1380 29.865 33.837 0.19261 1380 29.865 33.837 0.19261 1380 29.865 33.830 0.15862 1800 29.835 33.803 0.15862 1800 29.835 33.803 0.15862 1800 29.835 33.803 0.15862 2040 29.835 33.803 0.15862 2220 29.795 33.758 0.1133 2280 29.855 33.803 0.15862 2220 29.795 33.758 0.1133 2280 29.855 33.803 0.15862 2400 29.835 33.803 0.15862 2220 29.795 33.758 0.1133 2280 29.805 33.775 0.130295 2400 29.835 33.803 0.15862 2400 29.835 33.803 0.15862 2400 29.835 33.803 0.15862 2400 29.835 33.803 0.15862 2400 29.835 33.803 0.15862 2400 29.835 33.803 0.15862 2400 29.835 33.803 0.15862 2400 29.835 33.803 0.15862 2400 29.835 33.803 0.15862 2400 29.835 33.803 0.15862 2400 29.835 33.803 0.15862 2400 29.835 33.803 0.15862 2400 29.835 33.803 0.15862 2400 29.835 33.809 0.164285 2400 29.835 33.809 0.164285 2400 29.835 33.809 0.164285 2500 29.845 33.809 0.164285 2500 29.845 33.809 0.164285 2500 29.845 33.809 0.16995						
60 29.685 33.633 -0.01133 120 29.675 33.622 -0.02266 180 29.655 33.599 -0.04532 240 29.705 33.656 0.01133 300 29.7755 33.712 0.06798 420 29.755 33.712 0.06798 480 29.775 33.735 0.09064 420 29.805 33.769 0.12463 3/17, 2300 660 29.805 33.769 0.12463 3/18, 0100 660 29.805 33.769 0.12463 3/18, 0100 660 29.805 33.758 0.1133 840 29.795 33.758 0.1133 900 29.800 33.768 0.1133 900 29.801 33.758 0.1133 900 29.805 33.814 0.16995 1020 29.845 33.814 0.16995 1080 29.805 33.871 0.12266 1200		(min)	(in. Hg)	(ft. H ₂ O)	(ft. H ₂ O)	Comments
120	3/17/95, 1400	0	29.695	33.644	0	
180		60	29.685	33.633	-0.01133	
240 29.705 33.656 0.01133 300 29.775 33.712 0.06798 360 29.775 33.735 0.09064 420 29.755 33.712 0.06798 480 29.775 33.735 0.09064 3/17, 2300 540 29.805 33.746 0.10197 600 29.805 33.769 0.12463 3/18, 0100 660 29.825 33.789 0.14729 720 29.815 33.780 0.13596 780 29.795 33.758 0.1133 840 29.795 33.758 0.1133 840 29.795 33.758 0.1133 900 29.800 33.763 0.118965 960 29.800 33.763 0.118965 1020 29.845 33.814 0.16995 1080 29.895 33.864 0.209605 1140 29.895 33.861 0.2266 1140 29.895 33.881 0.209605 1140 29.895 33.881 0.209605 1140 29.895 33.881 0.2094 1320 29.865 33.826 0.21527 1260 29.875 33.848 0.20394 1320 29.865 33.826 0.18128 1500 29.865 33.826 0.18128 1500 29.865 33.826 0.18128 1500 29.865 33.826 0.18128 1500 29.855 33.826 0.18128 1500 29.855 33.826 0.18128 1680 29.835 33.803 0.15862 1740 29.835 33.803 0.15862 1740 29.835 33.803 0.15862 1860 29.845 33.814 0.16995 1920 29.855 33.826 0.18128 1880 29.835 33.803 0.15862 1740 29.835 33.803 0.15862 1860 29.845 33.814 0.16995 1920 29.855 33.826 0.18128 1890 29.845 33.814 0.16995 1920 29.855 33.803 0.15862 2460 29.835 33.803 0.15862 2460 29.835 33.803 0.15862 2460 29.835 33.803 0.15862 2460 29.855 33.803 0.15862 2460 29.855 33.803 0.15862 2460 29.855 33.803 0.15862 2460 29.855 33.803 0.15862 2460 29.845 33.814 0.16995		120	29.675	33.622	-0.02266	
300 29.755 33.712 0.06798 360 29.775 33.735 0.09064 420 29.755 33.712 0.06798 480 29.775 33.735 0.09064 3/17, 2300 540 29.785 33.746 0.10197 600 29.805 33.769 0.12463 3/18, 0100 660 29.825 33.792 0.14729 720 29.815 33.780 0.13596 780 29.795 33.758 0.1133 840 29.795 33.758 0.1133 900 29.800 33.763 0.118965 960 29.830 33.767 0.152955 1020 29.845 33.814 0.16995 1080 29.893 33.871 0.2266 1140 29.895 33.861 0.209605 1140 29.895 33.861 0.209605 1140 29.895 33.887 0.19261 1380 29.860 33.836 0.21527 1260 29.875 33.848 0.20394 1320 29.865 33.837 0.19261 1380 29.865 33.837 0.19261 1380 29.865 33.837 0.19261 1500 29.855 33.826 0.18128 1500 29.855 33.826 0.18128 1500 29.855 33.826 0.18128 1620 29.855 33.826 0.18128 1620 29.855 33.830 0.15862 1740 29.835 33.803 0.15862 1740 29.835 33.803 0.15862 1800 29.845 33.814 0.16995 1920 29.855 33.826 0.18128 1800 29.845 33.814 0.16995 1920 29.855 33.826 0.18128 1800 29.845 33.814 0.16995 1920 29.855 33.826 0.18128 1800 29.845 33.814 0.16995 1920 29.855 33.826 0.18128 1980 29.845 33.814 0.16995 1920 29.855 33.826 0.18128 1980 29.845 33.814 0.16995 2040 29.835 33.803 0.15862 2220 29.795 33.758 0.1133 2280 29.805 33.769 0.12463 2340 29.816 33.775 0.130295 2400 29.835 33.803 0.15862 2220 29.795 33.758 0.1133 2280 29.805 33.769 0.12463 2340 29.816 33.8175 0.130295 2460 29.835 33.803 0.15862 2460 29.835 33.803 0.15862 2460 29.835 33.803 0.15862 2460 29.835 33.803 0.15862 2460 29.835 33.803 0.15862 2460 29.835 33.803 0.15862		180	29.655	33.599	-0.04532	
360 29.775 33.735 0.09064 420 29.785 33.712 0.06798 480 29.775 33.735 0.09064 3/17, 2300 540 29.785 33.746 0.10197 600 29.805 33.769 0.12463 3/18, 0100 660 29.825 33.790 0.13596 780 29.815 33.780 0.13596 780 29.795 33.758 0.1133 840 29.795 33.758 0.1133 900 29.800 33.763 0.118965 960 29.830 33.797 0.152955 1020 29.845 33.814 0.16995 1080 29.800 33.854 0.209605 1140 29.895 33.871 0.2266 1200 29.885 33.860 0.21527 1260 29.875 33.848 0.20394 1320 29.865 33.837 0.19261 1380 29.860 33.831 0.186945 1440 29.855 33.826 0.18128 1500 29.855 33.848 0.20394 1620 29.855 33.848 0.20394 1620 29.855 33.848 0.20394 1620 29.855 33.848 0.20394 1620 29.855 33.848 0.20394 1620 29.855 33.848 0.20394 1620 29.855 33.830 0.15862 1740 29.835 33.803 0.15862 1740 29.835 33.803 0.15862 1800 29.835 33.803 0.15862 1800 29.835 33.803 0.15862 1800 29.835 33.803 0.15862 1800 29.835 33.803 0.15862 1800 29.835 33.803 0.15862 29.845 33.814 0.16995 2940 29.835 33.803 0.15862 2220 29.795 33.758 0.1133 2280 29.865 33.803 0.15862 2460 29.835 33.803 0.15862		240	29.705	33.656	0.01133	
420		300	29.755	33.712	0.06798	
3/17, 2300 540 29.755 33.735 0.09064 3/17, 2300 540 29.755 33.746 0.10197 600 29.805 33.769 0.12463 3/18, 0100 660 29.825 33.792 0.14729 720 29.815 33.780 0.13596 780 29.795 33.758 0.1133 840 29.795 33.758 0.1133 900 29.800 33.763 0.118965 960 29.830 33.797 0.152955 1020 29.845 33.814 0.16995 1080 29.800 33.854 0.209605 1140 29.895 33.871 0.2266 1200 29.885 33.860 0.21527 1260 29.875 33.848 0.20394 1320 29.865 33.837 0.19261 1380 29.860 33.831 0.186945 1440 29.855 33.826 0.18128 1500 29.865 33.837 0.19261 1560 29.875 33.848 0.20394 1620 29.855 33.826 0.18128 1600 29.855 33.826 0.18128 1600 29.855 33.826 0.18128 1600 29.855 33.803 0.15862 1740 29.835 33.803 0.15862 1800 29.835 33.803 0.15862 1800 29.845 33.814 0.16995 1920 29.855 33.826 0.18128 1980 29.845 33.814 0.16995 1920 29.855 33.826 0.18128 1980 29.845 33.814 0.16995 1920 29.855 33.803 0.15862 2220 29.795 33.758 0.1133 2280 29.845 33.814 0.16995 2400 29.835 33.803 0.15862 2220 29.795 33.775 0.130295 2400 29.835 33.803 0.15862 2220 29.795 33.775 0.130295 2400 29.835 33.803 0.15862 2220 29.795 33.775 0.130295 2400 29.835 33.803 0.15862 2220 29.795 33.775 0.130295 2400 29.835 33.803 0.15862 2220 29.795 33.775 0.130295 2400 29.835 33.803 0.15862 2220 29.795 33.775 0.130295 2400 29.835 33.803 0.15862 2460 29.825 33.779 0.12463 2340 29.810 33.775 0.130295 2400 29.835 33.803 0.15862 2460 29.825 33.792 0.14729 2520 29.845 33.803 0.15862 2460 29.835 33.803 0.15862 2460 29.835 33.803 0.15862 2460 29.835 33.803 0.15862 2460 29.835 33.803 0.15862 2460 29.835 33.803 0.15862 2460 29.835 33.803 0.15862 2460 29.835 33.803 0.15862 2460 29.835 33.803 0.15862 2460 29.835 33.803 0.15862 2460 29.835 33.803 0.15862		360	29.775	33.735	0.09064	
3/17, 2300		420	29.755	33.712	0.06798	
3/18, 0100		480	29.775	33.735	0.09064	
3/18, 0100	3/17, 2300	540	29.785	33.746	0.10197	
3/18, 0100 660 29.825 33.792 0.14729 720 29.815 33.780 0.13596 780 29.795 33.758 0.1133 840 29.795 33.768 0.1133 900 29.800 33.763 0.118965 960 29.830 33.877 0.152955 1020 29.845 33.814 0.16995 1080 29.880 33.854 0.209605 1140 29.895 33.871 0.2266 33.837 0.2266 33.837 0.9266 33.837 0.19261 1380 29.865 33.837 0.19261 1380 29.865 33.837 0.19261 1380 29.865 33.837 0.19261 1380 29.865 33.837 0.19261 1380 29.855 33.826 0.18128 1500 29.875 33.848 0.20394 1620 29.855 33.837 0.19261 1560 29.875 33.848 0.20394 1620 29.855 33.837 0.19261 1560 29.855 33.837 0.19261 1560 29.855 33.830 0.15862 1740 29.835 33.803 0.15862 1800 29.835 33.803 0.15862 1800 29.835 33.803 0.15862 1800 29.845 33.814 0.16995 1920 29.855 33.826 0.18128 1800 29.835 33.803 0.15862 29.845 33.814 0.16995 2040 29.835 33.803 0.15862 2040 29.835 33.803 0.15862 2220 29.845 33.814 0.16995 2160 29.835 33.803 0.15862 2220 29.795 33.758 0.1133 2280 29.805 33.759 0.12463 2340 29.815 33.803 0.15862 2400 29.835 33.803 0.15862 2400 29.835 33.803 0.15862 2400 29.835 33.803 0.15862 2400 29.835 33.803 0.15862 2400 29.835 33.803 0.15862 2400 29.835 33.803 0.15862 2400 29.835 33.803 0.15862 2400 29.835 33.803 0.15862 2400 29.835 33.803 0.15862 2400 29.835 33.803 0.15862 2400 29.835 33.803 0.15862 2400 29.835 33.803 0.15862 2400 29.835 33.803 0.15862 2400 29.835 33.803 0.15862 2400 29.835 33.803 0.15862	,	. 600	29.805	33.769	0.12463	
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2580 29.835 33.803 0.15862 2640 29.845 33.814 0.16995						
2640 29.845 33.814 0.16995						
2700 29.845 33.814 0.16995						
		2700	29.845	33.814	U.16995	

Table B-8

Barometric Pressure Observations
(From the National Weather Service at Fresno Air Terminal)

(Page 2 of 6)

	Elapsed	Pressure	Pressure	Absolute	
	Time	Reading	Reading	Change	
Date/Time	(min)	(in. Hg)	(ft. H ₂ O)	(ft. H ₂ O)	Comments
	2760	29.825	33.792	0.14729	
	2820	29.805	33.769	0.12463	
	2880	29.765	33.724	0.07931	
	2940	29.745	33.701	0.05665	
	3000	29.725	33.678	0.03399	
	3060	29.715	33.667	0.02266	
	3120	29.715	33.667	0.02266	
	3180	29.715	33.667	0.02266	
	3240	29.715	33.667	0.02266	
	3300	29.645	33.588	-0.05665	
	3360	29.665	33.610	-0.03399	
	3420	29.665	33.610	-0.03399	
	3480	29.660	33.605	-0.039655	
3/20, 0100	3540	29.635	33.576	-0.06798	
•	3600	29.615	33.554	-0.09064	
	3660	29.585	33.520	-0.12463	
	3720	29.575	33.508	-0.13596	
	3780	29.555	33.486	-0.15862	
	3840	29.545	33.474	-0.16995	
	3900	29.540	33.469	-0.175615	
÷	3960	29.560	33.491	-0.152955	
	4020	29.570	33.503	-0.141625	
	4080	29.560	33.491	-0.152955	
	4140	29.550	33.480	-0.164285	
	4200	29.520	33.446	-0.198275	
	4260	29.510	33.435	-0.209605	
	4320	29.480	33.401	-0.243595	
	4380	29.480	33.401	-0.243595	
	4440	29.495	33.418	-0.2266	
	4500	29.480	33.401	-0.243595	
	4560	29.470	33.390	-0.254925	
	4620	29.470	33.390	-0.254925	
	4680	29.460	33.378	-0.266255	
	4740	29.475	33.395	-0.24926	
	4800	29.470	33.390	-0.254925	
	4860	29.470	33.390	-0.254925	
	4920	29.455	33.373	-0.27192	
2/24 0400	4980	29.470	33.390	-0.254925	
3/21, 0100		29.470	33.390	-0.254925	
	5040 5100			-0.254925	
	5100 5160	29.450	33.367 33.367	-0.277585	
	5160 5330	29.450		-0.266255	
	5220 5220	29.460	33.378		
	5280	29.480	33.401	-0.243595	
	5340	29.490	33.412	-0.232265	
	5400	29.505	33.429	-0.21527	
	5460	29.525	33.452	-0.19261	

Table B-8
Barometric Pressure Observations
(From the National Weather Service at Fresno Air Terminal)

(Page 3 of 6)

	Elapsed	Pressure	Pressure	Absolute	
Date/Time	Time (min)	Reading (in. Hg)	Reading (ft. H ₂ O)	Change (ft. H ₂ O)	Comments
	5520	29.530	33.457	-0.186945	
	5580	29.545	33.474	-0.16995	
3/21, 1200	5640	29.545	33.474	-0.16995	Begin step-drawdown test
	5700	29.530	33.457	-0.186945	in MWBP-12 @1230
	5760	29.525	33.452	-0.19261	
	5820	29.520	33.446	-0.198275	
3/21, 1600	5880	29.510	33.435	-0.209605	End step-drawdown test
	5940	29.530	33.457	-0.186945	in MWBP-12 @1600
	6000	29.550	33.480	-0.164285	
	6060	29.565	33.497	-0.14729	
	6120	29.590	33.525	-0.118965	
	6180	29.620	33.559	-0.084975	
	6240	29.625	33.565	-0.07931	
	6300	29.645	33.588	-0.05665	
	6360	29.665	33.610	-0.03399	
3/22, 0100	6420	29.685	33.633	-0.01133	
	6480	29.675	33.622	-0.02266	
	6540	29.675	33.622	-0.02266	
	6600	29.665	33.610	-0.03399	
	6660	29.655	33.599	-0.04532	
÷	6720	29.655	33.599	-0.04532	
	6780	29.645	33.588	-0.05665	
	6840	29.655	33.599	-0.04532	
	6900	29.645	33.588	-0.05665	
	6960	29.635	33.576	-0.06798	Begin step-drawdown test
3/22, 1100	7020	29.620	33.559	-0.084975	in MWBP-05B @1050
	7080	29.595	33.531	-0.1133	
	7140	29.570	33.503	-0.141625	
	7200	29.540	33.469	-0.175615	
	7260	29.530	33.457	-0.186945	
3/22, 1600	7320	29.490	33.412	-0.232265	End step-drawdown test
	7380	29.470	33.390	-0.254925	in MWBP-05B @1615
	7440	29.445	33.361	-0.28325	
	7500	29.460	33.378	-0.266255	
	7560	29.450	33.367	-0.277585	
	7620	29.445	33.361	-0.28325	
	7680	29.430	33.344	-0.300245	
	7740	29.425	33.339	-0.30591	
	7800	29.410	33.322	-0.322905	
3/23, 0100	7860	29.390	33.299	-0.345565	
	7920	29.440	33.356	-0.288915	
	7980	29.440	33.356	-0.288915	
	8040	29.420	33.333	-0.311575	
	8100	29.460	33.378	-0.266255	
	8160	29.480	33.401	-0.243595	
	8220	29.520	33.446	-0.198275	

Table B-8

Barometric Pressure Observations
(From the National Weather Service at Fresno Air Terminal)

(Page 4 of 6)

	Elapsed	Pressure	Pressure	Absolute	
Date/Time	Time (min)	Reading (in. Hg)	Reading (ft. H ₂ O)	Change (ft. H ₂ O)	Comments
	8280	29.530	33.457	-0.186945	
	8340	29.530	33.457	-0.186945	
3/23, 1000	8400	29.550	33.480	-0.164285	Begin constant rate test
	8460	29.555	33.486	-0.15862	in MWBP-12 @1000
	8520	29.550	33.480	-0.164285	
	8580	29.560	33.491	-0.152955	
	8640	29.550	33.480	-0.164285	
	8700	29.550	33.480	-0.164285	
	8760	29.550	33.480	-0.164285	
	8820	29.570	33.503	-0.141625	
	8880	29.580	33.514	-0.130295	
	8940	29.600	33.537	-0.107635	
	9000	29.665	33.610	-0.03399	
	9060	29.655	33.599	-0.04532	
	9120	29.675	33.622	-0.02266	
	9180	29.690	33.639	-0.005665	
	9240	29.695	33.644	0	
3/24 0100	9300	29.705	33.656	0.01133	
	9360	29.705	33.656	0.01133	
	9420	29.705	33.656	0.01133	
•	9480	29.705	33.656	0.01133	
	9540	29.725	33.678	0.03399	
3/24 0600	9600	29.735	33.690	0.04532	End constant rate test
	9660	29.745	33.701	0.05665	in MWBP-12 @0600
	9720	29.765	33.724	0.07931	
	9780	29.775	33.735	0.09064	
	9840	29.785	33.746	0.10197	
	9900	29.780	33.741	0.096305	
	9960	29.770	33.729	0.084975	
	10020	29.745	33.701	0.05665	
	10080	29.725	33.678	0.03399	
	10140	29.715	33.667	0.02266	
	10200	29.705	33.656	0.01133	
	10260	29.695	33.644	0	
	10320	29.715	33.667	0.02266	
	10380	29.720	33.673	0.028325	
	10440	29.745	33.701	0.05665	
	10500	29.755	33.712	0.06798	
	10560	29.765	33.724	0.07931	
	10620	29.760	33.718	0.073645	
	10680	29.755	33.712	0.06798	
3/25 0100	10740	29.755	33.712	0.06798	
	10800	29.755	33.712	0.06798	
	10860	29.755	33.712	0.06798	
	10920	29.755	33.712	0.06798	
	10980	29.775	33.735	0.09064	

Table B-8

Barometric Pressure Observations
(From the National Weather Service at Fresno Air Terminal)

(Page 5 of 6)

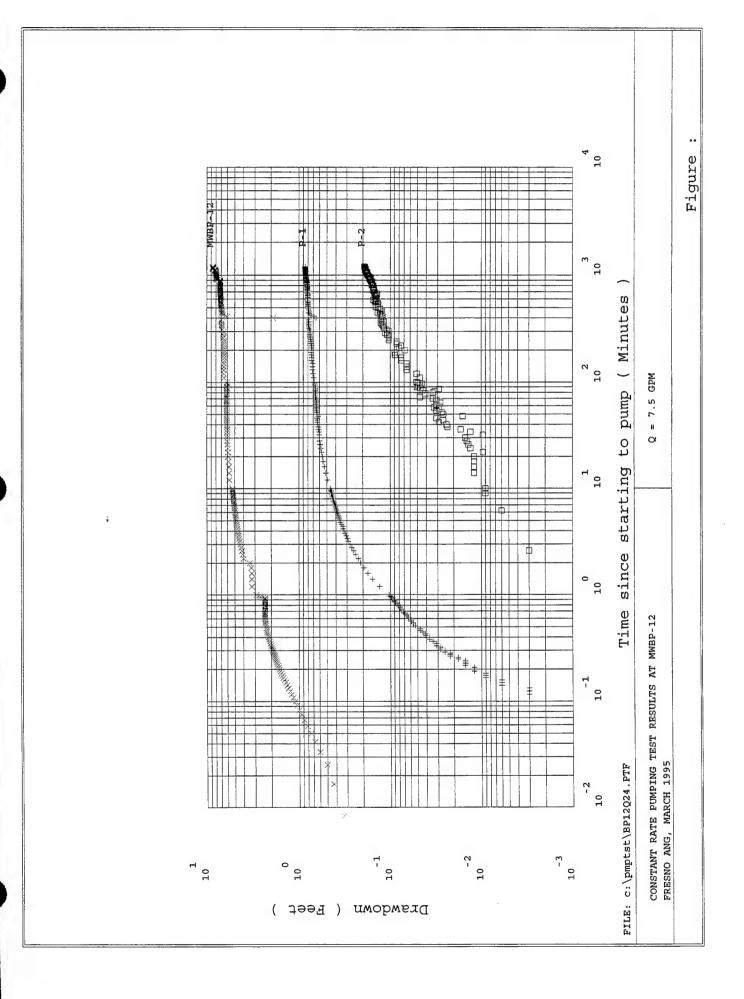
	Elapsed Time	Pressure Reading	Pressure Reading	Absolute Change	
Date/Time	(min)	(in. Hg)	(ft. H ₂ O)	(ft. H ₂ O)	Comments
	11040	29.785	33.746	0.10197	
	11100	29.805	33.769	0.12463	
	11160	29.820	33.786	0.141625	
	11220	29.830	33.797	0.152955	
	11280	29.825	33.792	0.14729	
	11340	29.820	33.786	0.141625	
	11400	29.815	33.780	0.13596	
	11460	29.805	33.769	0.12463	
	11520	29.795	33.758	0.1133	
	11580	29.790	33.752	0.107635	
	11640	29.785	33.746	0.10197	
	11700	29.785	33.746	0.10197	
	11760	29.795	33.758	0.1133	
	11820	29.805	33.769	0.12463	
	11880	29.815	33.780	0.13596	
	11940	29.820	33.786	0.141625	
	12000	29.815	33.780	0.13596	
	12060	29.815	33.780	0.13596	
	12120	29.825	33.792	0.14729	
3/26, 0100	12180	29.825	33.792	0.14729	
·	12240	29.835	33.803	0.15862	
	12300	29.835	33.803	0.15862	
	12360	29.845	33.814	0.16995	
	12420	29.855	33.826	0.18128	
	12480	29.865	33.837	0.19261	
	12540	29.875	33.848	0.20394	
	12600	29.885	33.860	0.21527	
	12660	29.895	33.871	0.2266	
	12720	29.895	33.871	0.2266	
	12780	29.895	33.871	0.2266	
	12840	29.880	33.854	0.209605	
	12900	29.855	33.826	0.18128	
	12960	29.840	33.809	0.164285	
	13020	29.825	33.792	0.14729	
	13080	29.805	33.769	0.12463	
	13140	29.800	33.763	0.118965	
	13200	29.805	33.769	0.12463	
	13260	29.815	33.780	0.13596	
	13320	29.825	33.792	0.14729	
	13380	29.830	33.797	0.152955	
	13440	29.835	33.803	0.15862	
	13500	29.835	33.803	0.15862	
	13560	29.835	33.803	0.15862	
3/27, 0100	13620	29.835	33.803	0.15862	
	13680	29.825	33.792	0.14729	
	13740	29.825	33.792	0.14729	

Table B-8

Barometric Pressure Observations
(From the National Weather Service at Fresno Air Terminal)

(Page 6 of 6)

	Elapsed	Pressure	Pressure	Absolute	
Date/Time	Time (min)	Reading (in. Hg)	Reading (ft. H ₂ O)	Change (ft. H ₂ O)	Comments
	13800	29.815	33.780	0.13596	
	13860	29.815	33.780	0.13596	
	13920	29.815	33.780	0.13596	
	13980	29.825	33.792	0.14729	
	14040	29.835	33.803	0.15862	
	14100	29.835	33.803	0.15862	
	14160	29.835	33.803	0.15862	
	14220	29.815	33.780	0.13596	Begin constant rate test
3/27, 1200	14280	29.800	33.763	0.118965	in MWBP-05B @1140
	14340	29.775	33.735	0.09064	
	14400	29.755	33.712	0.06798	
	14460	29.735	33.690	0.04532	
	14520	29.725	33.678	0.03399	
	14580	29.720	33.673	0.028325	
	14640	29.725	33.678	0.03399	
	14700	29.725	33.678	0.03399	
	14760	29.735	33.690	0.04532	
	14820	29.735	33.690	0.04532	
	14880	29.725	33.678	0.03399	
	14940	29.725	33.678	0.03399	
÷	15000	29.735	33.690	0.04532	
3/28, 0100	15060	29.735	33.690	0.04532	
	15120	29.735	33.690	0.04532	
	15180	29.725	33.678	0.03399	
	15240	29.715	33.667	0.02266	
	15300	29.715	33.667	0.02266	
	15360	29.725	33.678	0.03399	
	15420	29.725	33.678	0.03399	
	15480	29.725	33.678	0.03399	
	15540	29.730	33.684	0.039655	
	15600	29.730	33.684	0.039655	
	15660	29.725	33.678	0.03399	
	15720	29.715	33.667	0.02266	
	15780	29.680	33.627	-0.016995	
	15840	29.665	33.610	-0.03399	
	15900	29.655	33.599	-0.04532	
	15960	29.645	33.588	-0.05665	
	16020	29.645	33.588	-0.05665	
	16080	29.645	33.588	-0.05665	
	16140	29.655	33.599	-0.04532	
	16200	29.665	33.610	-0.03399	
	16260	29.675	33.622	-0.02266	
	16320	29.675	33.622	-0.02266	
	16380	29.665	33.610		End constant rate test
3/29, 0000	16440	29.655	33.599	-0.04532	in MWBP-05B @2340



<pre>Iransmissivity</pre>	= 276.80 $ = 1.4641000$	= 1.00 0.0036127 Hin n = 1.00 0.6830135 FT												
Transmissiv Storativity Stor. [Alfa	1/uw F(uw, Alfa)	Time Orawdown												
	÷				- 4									
7 FOOD 11CG/M:2	0.5000 FT 0.1600 FT	0.10000									B - E	B	8	
: MWBP-12	LC = 1	Alfa =												
Fumping well	Pumping rate y = Radius of casing rc Radius of well bore rw		- 01			(†⊖⊖ <u>-</u>])	nwol	۵.	٦.	·.		

Time since starting to pump (Minutes)

0 01

10

-3

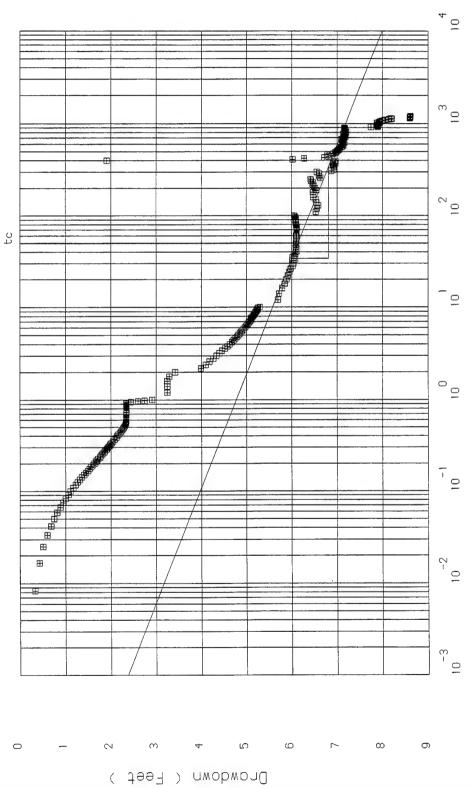
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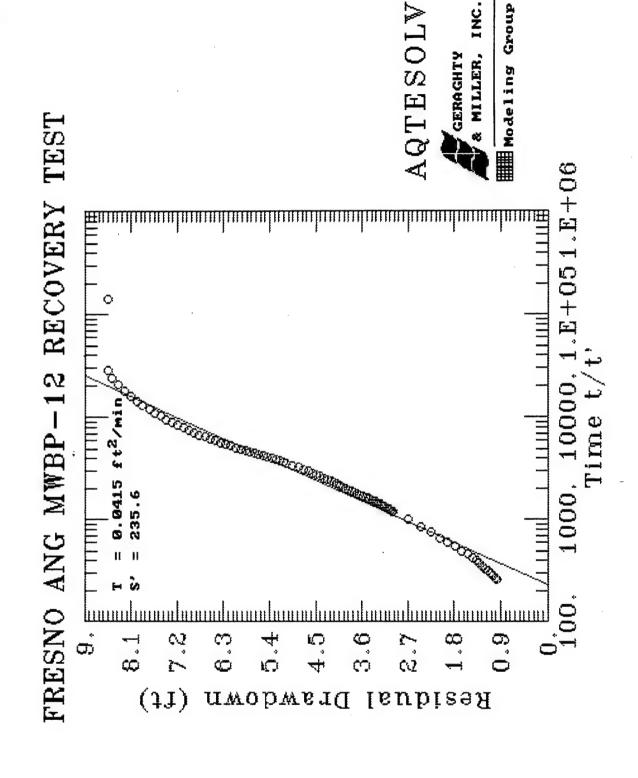
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0.00000115 Min	0.80418110 FT	2458.038 USGPD/FT	0.5000 FT	0.1600 FT	49.298 Min
11	П	Н	11	Ħ	П
£0	sp	—	L C	ď	tc
			7.5000 USG/Min		
		: MWBP-12	11		
		Pumping well	Pumping rate		

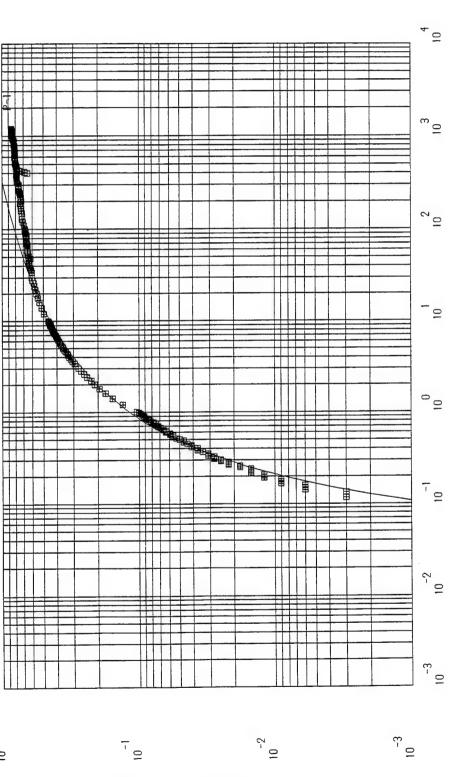


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Time since starting to pump (Minutes)

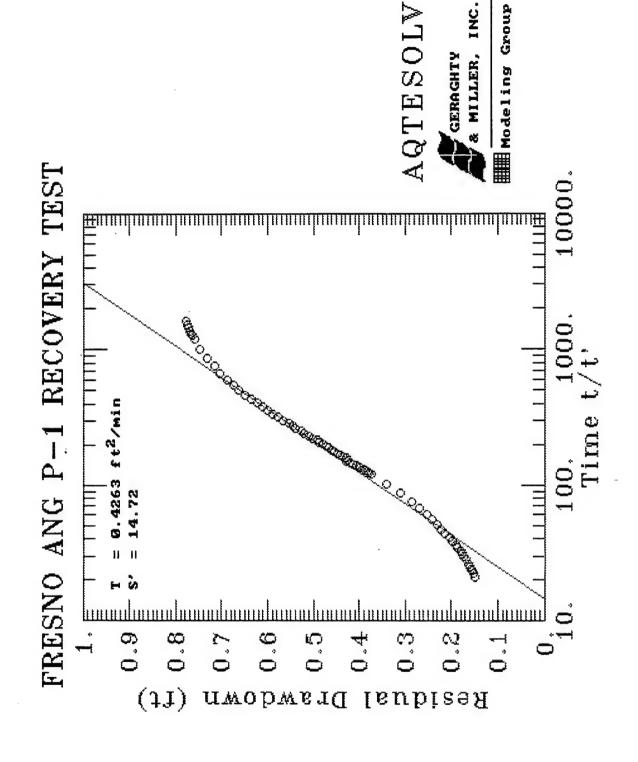


657.078 USGPD/FT^2 5256.624 USGPD/FT 0.00334473 1.00 0.3855433 Min 1.00 0.1635080 FT 1.00 S S ш |-- || |<u>|</u> = 2.5937425= 6.1159090Hydr. conductivity Transmissivity MATCH POINT : Storativity, Drawdown = 1/0 W(u) Time [PUMPING TEST LOG-LOG ANALYSIS : Rtheis TYPE CURVE Confined] 7.5000 USG/Min 8,0000 FT 15.00 FT : MWBP-12 11 __ Pumping rate 0 = Aquifer thickness b = Observation well: P-1 -1 0 01 Pumping well Distance Drawdown (Feet

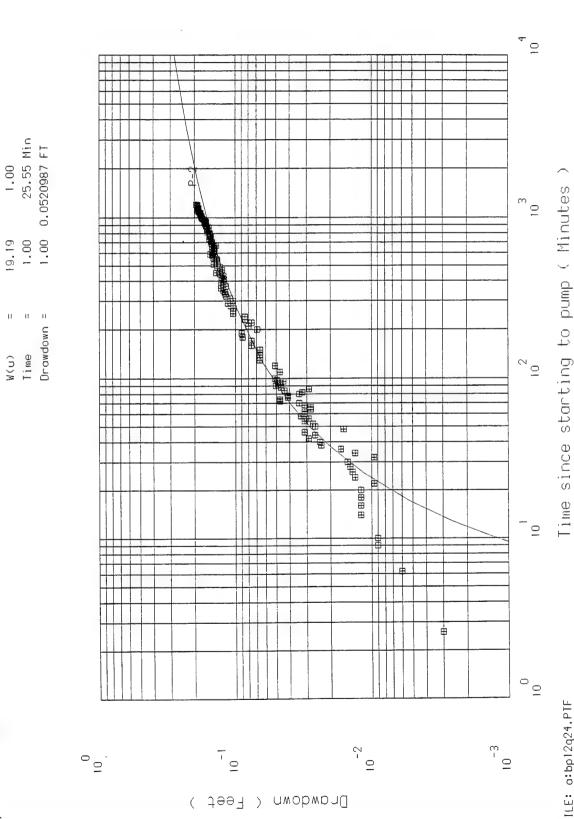


Time since starting to pump (Minutes)

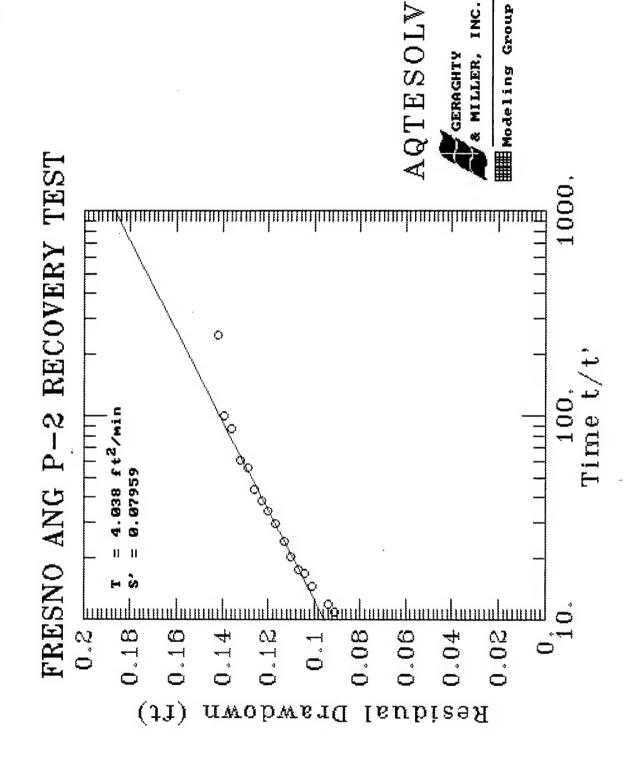
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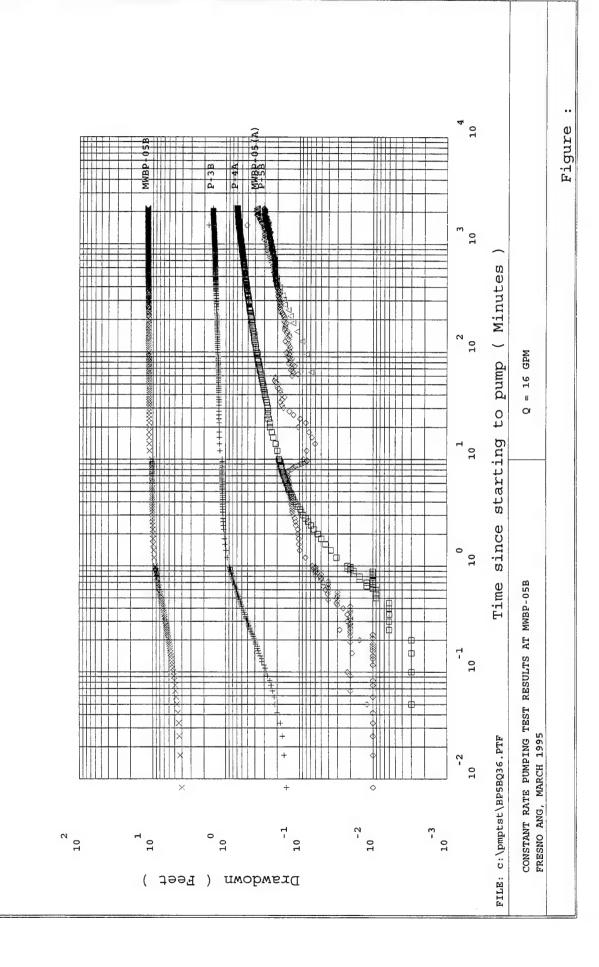


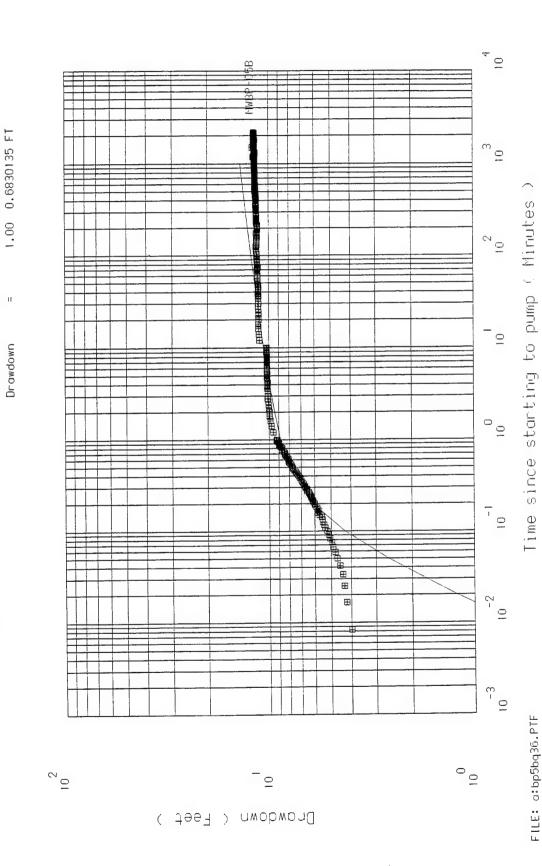
2062.192 USGPD/FT^2 16497,537 USGPD/FT 0.06260284 1.00 Ω ⊼ II II 0.0391425 Hydr. conductivity Transmissivity MATCH POINT : Storativity 11 1/0 [PUMPING TEST LOG-LOG ANALYSIS : Rtheis TYPE CURVE Confined] 7.5000 USG/Min 8,0000 FT 50,00 FT : MWBP-12 Pumping rate 0 = Aquifer thickness b = Observation well: P-2 Pumping well Distance

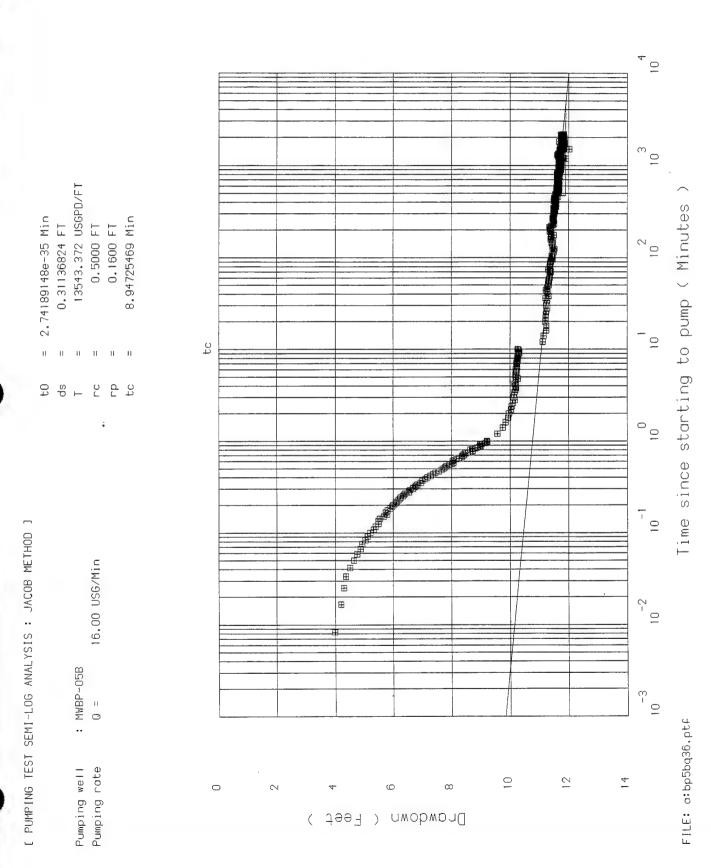


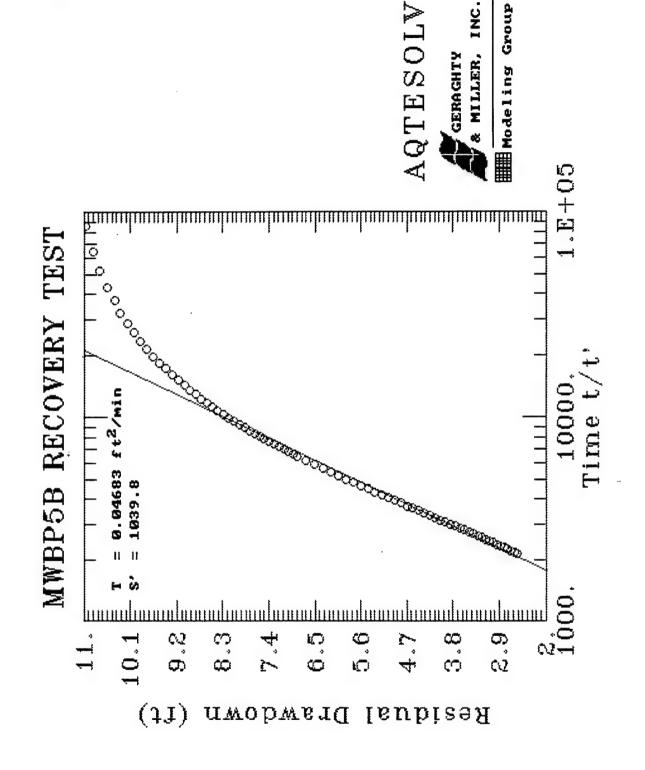
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10
                          2.84853802 USGPD/FT^2
        6330,084 USGPD/FT
                                                                                                                                                                                                                                                                                                                               3
                                                                                                                                                                                     æ
                                                              0.0267349 Min
                 0.00015711
                                                                      0.2896644 FT
                                            1.00
               Storativity S = Vert. conductivity K' =
                                                              1.00
                                            37.40
                                            1/u = 37.40
W(u,r/B) = 3.4522712
        Transmissivity
                                   MATCH POINT:
                                                                      Drawdown =
                                                              Time
                                            1/u
[ PUMPING TEST LOG-LOG ANALYSIS : Jacob & Hantush TYPE CURVE 0.15 ]
                                  16.00 USG/Min
                                                                                                                                                                                                                                                                                             8,0000 FT
                 20.00 FT
                                                     0.15000
                           : MWBP-05B
                                                                                                                                                                                                                                                                                                                              -3
                                             Leaky bed thickness b' =
         Observation well: P-3B
                                                                                                                                                                                                                                                                                                                10
                                     Pumping rate
                                                                                                                                                                                                     0
                           Pumping well
                                                                                            - 01
                  Distance
                                                                                                                                                     Drawdown ( Feet )
```

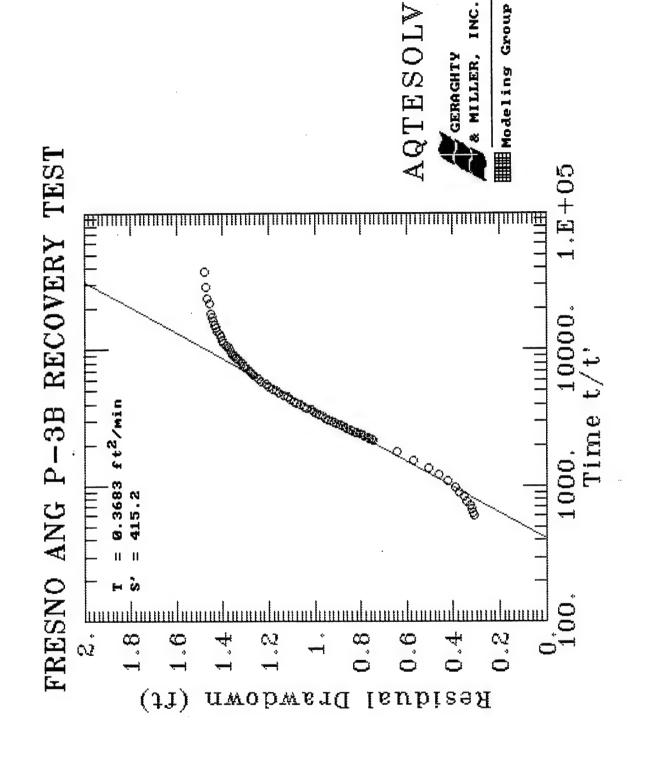
Time since starting to pump (Minutes

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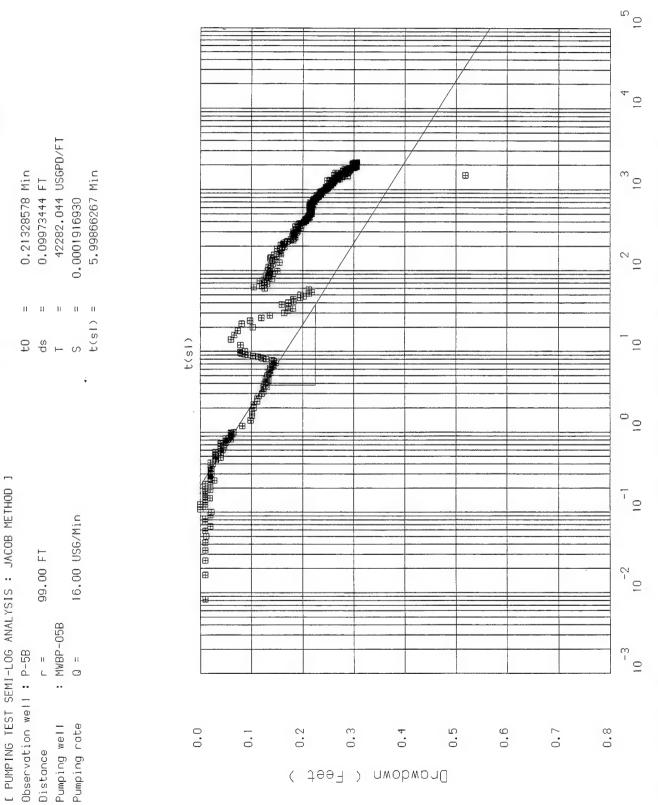
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10
                           1.39261859 USGPD/FT^2
        6963.093 USGPD/FT
                                                                                                                                                                                        ⊞
                                                               0.0243044 Min
                0.00015711
                                                                        0.2633313 FT
               Vert. conductivity K' = MATCH POINT
                                                              1.00
                                            |/u = 41.14
W(u,r/B) = 3.7974983
         Iransmissivity
                                   MATCH POINT :
                                                                       Drawdown =
                                                                Time
[ PUMPING TEST LOG-LOG ANALYSIS : Walton TYPE CURVE 0.1 ]
                                   16.00 USG/Min
                                                                                                                                                                                                                                                                                                  8,0000 FT
                                                                                                                                                                                                                                                                                                                                    10
                 20.00 FT
                                                      0.10000
                            : MWBP-05B
                                             Leaky bed thickness b' =
         Observation well: P-3B
                                     =
()
                            Pumping well
                                                                                                                                                                                                                                                                                                                     10
                                     Pumping rate
                                                                                                                                                                                                         0 01
                                                                                             101
                    Distance
                                                                                                                                                        Drawdown ( Feet )
```

FILE: a:bp5bq36.PTF

Time since starting to pump (Minutes)



INC.



FILE: a:bp5bq36.ptf

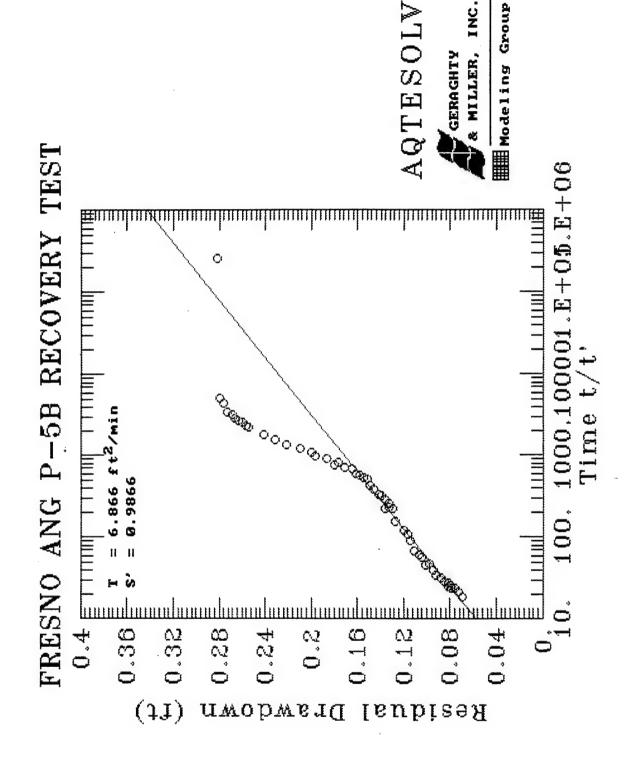
Time since starting to pump (Minutes)

10 860.316 USGPD/FT^2 38714.221 USGPD/FT 3 0.00023886 1.00 0.1628438 Min 1.00 0.0473624 FT 1.00 1.00 II X II 21.11 = 6.1408544 Hydr. conductivity ₩ ⊞ Transmissivity MATCH POINT : Storativity Drawdown = Time W(u) 1/n 16.00 USG/Min 10 45.0 FT 99.00 FT : MWBP-05B Observation well : P-5B п В Aquifer thickness -2. 10 10 Pumping well Pumping rate Distance Drawdown (Feet)

[PUMPING TEST LOG-LOG ANALYSIS : Rtheis TYPE CURVE Confined]

FILE: c:\pmptst\BP5BQ36.PTF

Time since starting to pump (Minutes)



401.216 USGPD/FT^2 18054.726 USGPD/FT 0.00417063 0.9953306 Min 0.1015579 FT 1.00 1.00 II # ¥ 1.00 1.00 = 1.00469139.8466004 Hydr. conductivity Transmissivity Storativity MATCH POINT Drawdown = W(u) Time 1/n [PUMPING TEST LOG-LOG ANALYSIS : Rtheis TYPE CURVE Confined] 16.00 USG/Min 45.0 FT 40.00 FT : MWBP-05B Observation well : P-4A 11 11 O Q Aquifer thickness -2 10 10 -1 Pumping rate Pumping well 10 Distance Drawdown (Feet)

Time since starting to pump (Minutes)

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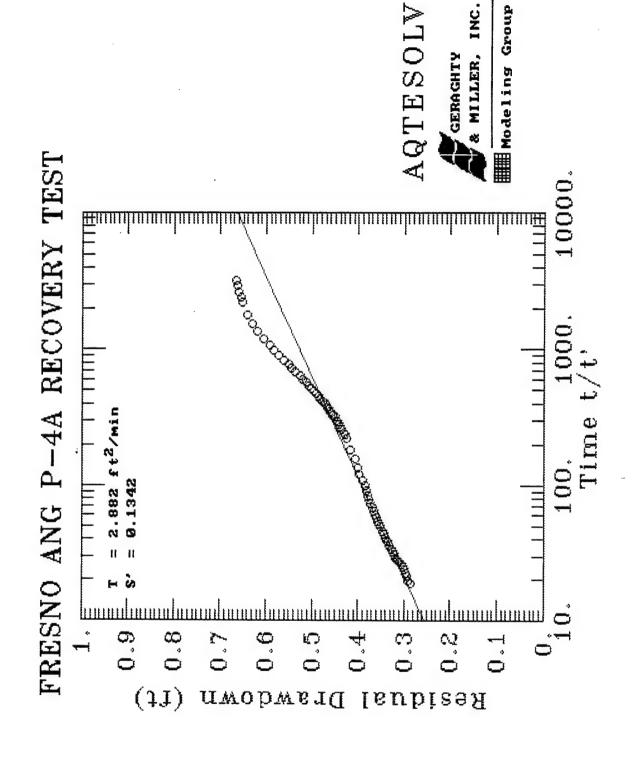
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398.913 USGPD/FT^2 17951.080 USGPD/FT 0.02394794 37.38 Min 1.00 0.1021443 FT 1.00 1.00 ທ ¥ 1.00 = 0.02675389.7900744 Hydr. conductivity Transmissivity MATCH POINT : Storativity Drawdown = Time W (11) 1/n [PUMPING TEST LOG-LOG ANALYSIS : Rtheis TYPE CURVE Confined] 16.00 USG/Min 102.00 FT 45.0 FT Observation well : MWBP-05(A) : MWBP-05B H H Pumping rate Q = Aquifer thickness b = 10 10 Pumping well Distance Drawdown (Feet)

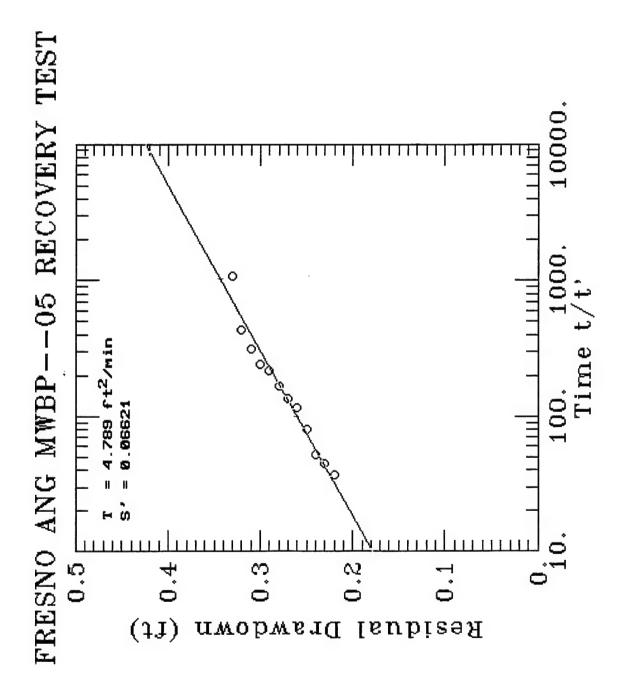
Time since starting to pump (Minutes)

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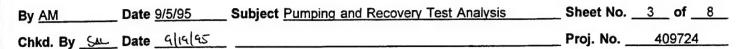
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3.2 In accordance with Theis (1935) recovery method, upon completion of a pumping test, recovery occurs at a constant rate with the residual drawdown given by:

$$s' = \frac{Q}{4\pi T} W(u) - W(u') \tag{4}$$

where
$$u = \frac{r^2S}{4Tt}$$
 and $u' = \frac{r^2S'}{4Tt'}$

s' is the residual drawdown, Q is the rate of well recharge which is equal to the rate of well discharge, S' is the dimensionless storativity of the aquifer during recovery, and t' is the time since the cessation of pumping.

For r small and t' large, equation (4) can be written as

$$s = \frac{2.30Q}{4\pi T} \log \frac{t}{t'} \tag{5}$$

A plot of residual drawdown s' versus t/t' on semi-log paper (t/t' on logarithmic scale) yields a straight line. The slope of the line equals $\frac{2.30Q}{4\pi T}$ so that for Δ s', the residual drawdown per log cycle of t/t', the transmissivity becomes :

$$T = \frac{2.30Q}{4\pi\Delta s'}$$

where Δ s' is the residual drawdown difference per log cycle of t/t'.





By AM Date 9/19/95 Subject Transmissivity Culculations Sheet No. 1 of 2

Chkd. By Su Date 9/19/95 FRESING ANG Proj. No. 409724

The Thiem-Dupuit method was used to calculate transmissivity of geologic materials in the shallow water-bearing zone and the deep water-bearing zone at the Fresno ANG, Fresno, California. The Thiem-Dupuit method is based on the equation:

$$Q=2\pi r K \frac{dh}{dr}$$

after integration between r_1 and r_2 with $(r_2 > r_1)$

$$Q = \frac{\pi K (h_2^2 - h_1^2)}{\ln(\frac{r_2}{r_1})}$$

since h=D-s

$$Q = \frac{2\pi KD(s_1 - s_2)}{\ln(\frac{r_2}{r_1})}$$

T = KD

$$= \frac{2\pi KD(s_1 - s_2)}{2.30\log(\frac{r_2}{r_1})}$$

$$T = \frac{Q}{2\pi(s_1 - s_2)} \ln(\frac{r_1}{r_2})$$

where s' is the corrected drawdown for late time data and s' = $s-(s^2/2D)$

1. Pumping MWBP-12 at 7.5 gpm with observation wells P-1 and P-2:

(i) At
$$t = 1200$$
 minutes $s'_1 = 0.858$ ft $r_1 = 15$ ft $s'_2 = 0.193$ ft $r_2 = 50$ ft



By Am Date 9-19-97 Subject Transmissivity (alwish Sheet No. 2 of 2 Chkd. By Su Date 9/19/95 FREJNO ANG Proj. No. 409 724

$T = \frac{2.30 \times 7.5 \ gpm \times 0.134 \times \log(50 \ ft \ /15 \ ft)}{2\pi(0.853 \ ft - 0.193 \ ft)}$

where $0.134 = \text{conversion factor gpm to } \text{ft}^3/\text{min}$

 $T = 0.292 \text{ ft}^2/\text{min}$

(ii) At t = 450 minutes
$$s'_1 = 0.786 \text{ ft}$$
 $r_1 = 15 \text{ ft}$ $s'_2 = 0.137 \text{ ft}$ $r_2 = 50 \text{ ft}$

 $T = 0.296 \text{ ft}^2/\text{min}$

2. A. Pumping MWBP-05B at 16 gpm with observation wells P-4A and MWBP-05 (Shallow water-bearing Zone)

(i) At
$$t = 2160$$
 minutes $s'_1 = 0.707$ ft $r_1 = 40$ ft $r_2 = 102$ ft

 $T = 0.981 \text{ ft}^2/\text{min}$

(ii) At
$$t = 1205$$
 $s'_1 = 0.65 \text{ ft}$ $r_1 = 40 \text{ ft}$ $s'_2 = 0.294 \text{ ft}$ $r_2 = 102 \text{ ft}$

 $T = 0.902 \text{ ft}^2/\text{min}$

B. Pumping MWBP-05B at 16 gpm with wells P-5B and P-3B as the observation points (deep water bearing zone).

At t = 2160 minutes
$$s'_1 = 0.306 \text{ ft}$$
 $r_1 = 99 \text{ ft}$ $s'_2 = 1.519 \text{ ft}$ $r_2 = 20 \text{ ft}$

 $T = 0.449 \text{ ft}^2/\text{min}$





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Chkd. By Duc Date 12/10/96 Modification to the Theis Method, Fresno ANG Proj. No. 409724

1.0 Objective

To determine the effects of partial penetration on aquifer test results from aquifer test data obtained at the Fresno ANG Base. Hantush's (1961a, 1961b) modification to the Theis method for partially penetrating wells was chosen as being the most applicable among several methods for P-3B.

2.0 Background

A constant rate discharge test was conducted in monitoring well MWBP-05B at the Fresno ANG Base for a period of 36 hours. The discharge rate was maintained at a constant 16 gallons per minute (2.139 ft³/min) for the test duration. The pumping well partially penetrates a semiconfined aquifer which is about 45 feet thick. Drawdown measurements at four monitoring points were collected during the test. The only observation point in which supposed partial penetration effects were noted was in piezometer P-3B. This piezometer is located 20 feet from the pumping well and is screened over the exact screened interval as the pumping well.

Figure 1 shows the configuration of the pump test monitoring network and well geometries in relation to the hydrogeologic setting.

3.0 Method

The following discussion of the Hantush partial penetration method is taken from Kruseman and de Ridder (1991). This method is not applicable for the pumping well.

For a relatively short pumping time, the drawdown in a piezometer at a distance, r, from a partially penetrating well is, according to Hantush (1961a, 1961b):

$$s = \frac{Q}{8\pi K(b-d)} E\left(u, \frac{b}{r}, \frac{d}{r}, \frac{a}{r}\right) \tag{1}$$

where

$$E\left(u, \frac{b}{r}, \frac{d}{r}, \frac{a}{r}\right) = E(u) = M(u, B_1) - M(u, B_2) + M(u, B_3) - M(u, B_4)$$
 (2)

$$u = \frac{r^2 S_s}{4Kt} \tag{3}$$

 $S_s = S/D = Specific storage$

 $B_1 = (b+a)/r$ (for symbols b, d, and a, see Figure 1)

 $B_2 = (d+a)/r$

 $B_3 = (b-a)/r$

D = aquifer thickness

 $B_4 = (d-a)/r$

s = drawdown at time, t

Q = discharge rate

r = radial distance from pumping well

K = hydraulic conductivity

t = time with drawdown, s

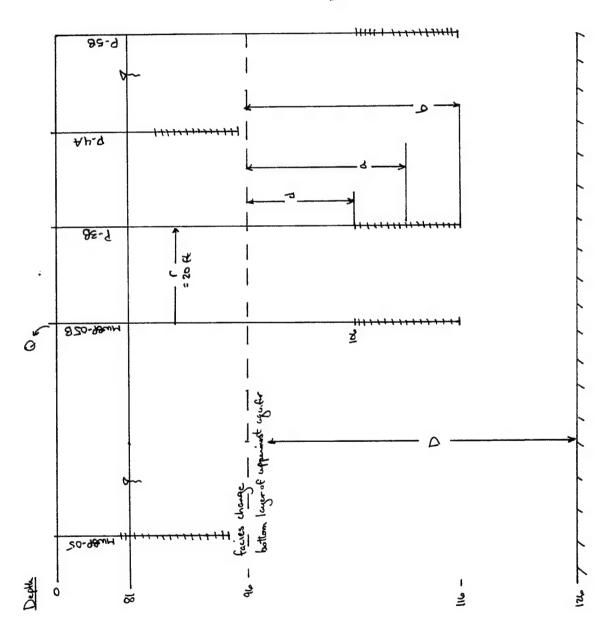


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d= 106-96= 10 ft a= 111-96= 15 ft b= 116-96= 20 ft D= 126-96= 30 ft







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Numerical values for M(u,B) are given in Kruseman and de Ridder (1991) and those which apply are included in Table 1 (see Section 5).

The following assumptions and conditions underly this method:

- 1) The aquifer is confined.
- 2) The aquifer has a seemingly infinite areal extent.
- 3) The aquifer is homogeneous, isotropic and of uniform thickness over the area influenced by the test.
- 4) Prior to pumping, the piezometric surface is nearly horizontal over the area that will be influenced by the test.
- 5) The aquifer is pumped at a constant discharge rate.
- 6) The well does not penetrate the entire thickness of the aquifer.
- 7) Flow to the well is in an unsteady state.
- 8) The time of pumping is relatively short: $t < [(2D-b-a)^2(S_s)]/20K$.

Discussion. Conditions 4) through 7) are met in this test. Given the type of alluvial aquifer system in which the wells are installed, Conditions 2) and 3) are not satisfied in their classic sense. As for condition 1), the aquifer has been assessed to be semiconfined, and portions of other tests react similar to confined aquifers. Applying a confined method is considered appropriate for the aquifer. Condition 8) will be assessed later in the calculation.

4.0 Procedure

- For one observation point, determine values for B₁, B₂, B₃ and B₄. Using these B values, find the values of M(u,B_n) for different values of 1/u. Use equation (2) to calculate values for E(u) at various values for 1/u.
- Plot values of E(u) versus 1/u on log-log paper; this gives the type curve.
- At the same scale as the type curve, plot (corrected) drawdown versus time for the observation point.
- Match the data curve to the type curve. At relatively large values of time, the data should diverge from the type curve; this is to be expected because the type curve is based on the assumption that the pumping time is short.
- Select a match point "A" on the superimposed sheets and note values of s, t, E(u) and 1/u.
- Substitute the values for s and E(u) into equation (1) and calculate K.
- Substitute values of t, 1/u and K into equation (3) and calculate S_s.
- Data should be used from piezometers at a distance, r < 2D.

5.0 Application

This method was unable to be applied to the pumping well, MWBP-05B. Piezometer P-3B showed an effect from partial penetration and this method was used for it. Data from piezometer P-5B did not follow any classic response patterns and the Hantush method could not be applied to it. Responses in observation points P-4A and MWBP-05 followed that of a confined aquifer and did not show any effects of partial penetration or delayed yield; therefore, they were not analyzed by this method. Only the data from P-3B could be used



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in this analysis.

Figure 1 shows the well geometry used in asigning values for b, d and a. These parameters were calculated not from the top of the water table, but from the contact between a coarse-grained and fine-grained material beneath the water table. This interface was used as the aquitard and is asserted to be the zone which is actually analyzed under this method. Table 1 provides the calculations for the various Bs and the function E(u). Values for M(u,B) are from Kruseman and de Ridder (1991).

Figure 2 shows the resulting type curve generated from 1/u and E(u) and Figure 3 shows the plot of drawdown data at P-3B at the same scale as Figure 2. A transparency for Figure 2 is also attached. The match point at E(u) = 1 and 1/u = 10 has values on Figure 3 of t = 0.58 minutes and s = 1.25 feet. Rearranging eq. (1) to solve for K with s = 1.25 ft, (b-d) = 10 ft (Table 1), and Q = 2.139 ft³/min gives:

$$K = \frac{2.139 ft^3/\text{min}}{8\pi (1.25 \ ft) (10 \ ft)} \times (1) = 6.81 \times 10^{-3} \ ft/\text{min} = 9.8 \ ft/day$$

Given that the thickness (D) of the aquifer is 45 feet, the transmissivity, $T_{1} = KD = 9.8 \times 45 = 441 \text{ ft}^2/\text{day}$.

Rearranging eq. (3) to solve for S_s with u = 0.1, t = 0.58 min and r = 20 ft, gives:

$$S_s = \frac{4(0.1)(6.81 \times 10^{-3} ft/min)(0.58 min)}{(20 ft)^2} = 3.95 \times 10^{-6} ft^{-1}$$

And the storativity, $S = S_sD = 3.95x10^{-6}(45) = 1.78x10^{-4}$ (dimensionless).

Assessment. The piezometer, P-3B, is located 20 feet from the pumping well. This satisfies the condition of r < 2D (60 feet). The time of pumping which appears to be applicable from Section 3.0 is $t < \{(2D-b-a)^2(S_s)\}/20K$.

 $(2D-b-a)^2 = (60-20-15 \text{ feet})^2 = 625 \text{ ft}^2$. $625 \text{ ft}^2 \times 3.95 \times 10^{-6} \text{ ft}^{-1} = 2.47 \times 10^{-3} \text{ ft}$. Now $K = 6.8 \times 10^{-3} \text{ ft/min}$ and 20K = 0.136 ft/min. $2.47 \times 10^{-3} \text{ ft/} 0.136 \text{ ft/min} = 0.018 \text{ min}$ or 1.09 seconds. This seems unreasonably low for pumping time. The chosen time of 0.58 minutes is about 35 seconds, which seems short enough to allow for the calculations to be considered valid.

6.0 Conclusion

The data set for P-3B exhibits the effects of partial penetration. Applying the Hantush method for partial penetration gives the following aquifer properties:

$$K = 9.8 \text{ ft/day}$$

 $T = 441 \text{ ft}^2/\text{day}$
 $S_s = 3.95 \times 10^{-6} \text{ ft}^{-1}$
 $S = 1.78 \times 10^{-4}$.



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7.0 References

Hantush, M.S., 1961a, Drawdown around a partially penetrating well, Journal of Hydraulics Div., Proc. American Society of Civil Engineers, Vol. 87(HY4), pp. 83-98.

Hantush, M.S., 1961b, Aquifer tests on partially penetrating wells, Journal of Hydraulics Div., Proc. American Society of Civil Engineers, Vol. 87(HY5), pp. 171-195.

Kruseman, G.P., N.A. de Ridder, 1991, Analysis and Evaluation of Pumping Test Data, 2nd ed., Publication 47, International Institute for Land Reclamation and Improvement, Wageningen, The Netherlands, 377 pp.

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TABLE 1
Calculation of Values for E(u) Based on Equation 2

Setup: $r = 20$ ft	$B_1 = (b+a)/r = 35/20 = 1.75 = 1.8$	
(see Fig 1) $b = 20 \text{ ft}$	$B_2 = (d+a)/r = 25/20 = 1.25 = 1.2$	
d = 10 ft	$B_3 = (b-a)/r = 5/20 = 0.25$	
a = 15 ft	$B_4 = (d-a)/r = -5/20 = -0.25$ (not used in calculation)	

				Values used for	or	
M(u,B)					interpolation o	f M(u,B) = 0.25.
1/u	M(u,B ₁)=1.8	$M(u,B_2)=1.2$	M(u,B ₃)=.25	E(u) ^a	$M(u,B_3)=.20$	$M(u,B_3)=.30$
1.00E+06	2.6968	2.0292	0.4938	1.1614	0.3969	0.5907
5.00E+05	2.6951	2.0281	0.4936	1.1606	0.3967	0.5904
2.50E+05	2.6927	2.0265	0.4933	1.1595	0.3965	0.59
1.66E+05	2.6909	2.0253	0.4930	1.1586	0.3963	0.5897
1.25E+05	2.6894	2.0243	0.4928	1.1579	0.3961	0.5894
1.00E+05	2.688	2.0234	0.4926	1.1572	0.3959	0.5892
5.00E+04	2.6827	2.0198	0.4919	1.1548	0.3954	0.5883
2.50E+04	2.6752	2.0148	0.4908	1.1512	0.3945	0.5871
1.66E+04	2.6694	2.011	0.4900	1.1484	0.3939	0.5861
1.25E+04	2.6645	2.0077	0.4893	1.1461	0.3933	0.5853
1.00E+04	2.6603	2.0049	0.4888	1.1442	0.3929	0.5846
5.00E+03	2.6434	1.9936	0.4864	1.1362	0.391	0.5818
2.50E+03	2.6197	1.9778	0.4831	1.1250	0.3883	0.5778
1.66E+03	2.6014	1.9656	0.4806	1.1164	0.3863	0.5748
1.25E+03	2.586	1.9554	0.4784	1.1090	0.3846	0.5722
1.00E+03	2.5725	1.9463	0.4765	1.1027	0.3831	0.5699
5.00E+02	2.5195	1.9109	0.4692	1.0778	0.3772	0.5611
2.50E+02	2.4447	1.861	0.4588	1.0425	0.3689	0.5486
1.66E+02	2.3875	1.8228	0.4508	1.0155	0.3625	0.539
1.25E+02	2.3395	1.7907	0.4441	0.9929	0.3571	0.531
1.00E+02	2.2975	1.7625	0.4382	0.9732	0.3524	0.5239
5.00E+01	2.1342	1.6527	0.4151	0.8966	0.334	0.4962
2.50E+01	1.9103	1.5008	0.3831	0.7926	0.3083	0.4578
1.66E+01	1.7454	1.3877	0.3590	0.7167	0.289	0.4289
1.25E+01	1.612	1.2951	0.3391	0.6560	0.2731	0.405
10	1.4991	1.2159	0.34185	0.6251	0.2993	0.3844
5	1.1026	0.9297	0.25825	0.4312	0.2084	0.3081
2.5	0.676	0.6015	0.18075	0.2553	0.1462	0.2153
1.66	0.4471	0.4122	0.13245	0.1674	0.1074	0.1575
1.25	0.3084	0.2913	0.09925	0.1164	0.0806	0.1179
1	0.2186	0.2101	0.07545	0.0840	0.0614	0.0895
0.5		0.0485	0.0213		0.0175	0.0251
0.25			0.0021		0.00176	2.44E-03
0.166			0.0002295		0.000195	2.64E-04
0.125			2.625E-05		2.26E-05	2.99E-05

 $a - \ \, \mathsf{E}(\mathsf{u}, \mathsf{b}/\mathsf{r}, \mathsf{d}/\mathsf{r}, \mathsf{a}/\mathsf{r}) {=} \mathsf{M}(\mathsf{u}, \mathsf{B}_1) {-} \mathsf{M}(\mathsf{u}, \mathsf{B}_2) {+} \mathsf{M}(\mathsf{u}, \mathsf{B}_3)$

